## V.D Storage

# V.D. 1 Inexpensive Delivery of Compressed Hydrogen with Advanced Vessel Technology 

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## Objectives

- Evaluate high performance containers for delivery truck applications
- Evaluate high performance containers for fueling station applications
- Examine potential synergies between $\mathrm{H}_{2}$ delivery vessel conditions and refueling station requirements


## Technical Barriers

This project addresses the following technical barriers from the Hydrogen Delivery section of the Hydrogen, Fuel Cells and Infrastructure Technologies Program Multi-Year Research, Development and Demonstration Plan:

- A. Lack of Options Analysis
- F. Transport Storage Costs


## Technical Targets

Table 1. LLNL Progress Toward Meeting DOE Hydrogen Delivery Targets

| Delivery Parameter | Units | 2010 Target | LLNL advanced vessel <br> (projected) |
| :--- | :---: | :---: | :---: |
| Total cost contribution of delivering hydrogen <br> from the production site through dispensing at the <br> refueling site. | $\$ / \mathrm{kg}(\$ / \mathrm{gge})$ | 1.70 | $<0.5^{*}$ |

*Currently projected interim costs only include truck delivery. Further analysis will consider refueling station cost estimates.

## Approach

- Design conformable and cryogenic compatible pressure vessels for delivery trucks and fueling stations
- Analyze possible energy and economic savings from hydrogen delivery in advanced vessels


## Accomplishments

- Identified delivery truck operational regimes in a temperature vs. density (T- $\rho$ ) diagram.
- Estimated possible savings by delivering high density hydrogen (high pressure and possibly cooled) where potential additional capital costs of trailers are balanced by reduced operating or energy costs.
- Identified preliminary design parameters for glass fiber macrolattice conformable pressure vessels for inexpensive hydrogen delivery truck trailers ( $\sim 0.50 /$ gge $)$.


## Future Directions

- Determine favorable hydrogen storage parameters and refueling operations to minimize delivery cost from a large scale production site through dispensing at the refueling station.
- Conduct a detailed design of a truck size macrolattice pressure vessel.
- Manufacture and test small scale container components to verify performance


## Introduction

Conventional forms of truck delivery (ambient temperature compressed $\mathrm{H}_{2}$ gas at $\sim 2600$ psi or liquid hydrogen $\left(\mathrm{LH}_{2}\right)$ cooled to 20 K$)$ represent extreme regions of temperature and density within the hydrogen phase diagram (Figure 1) [1]. Hydrogen delivery in today's low density compressed $\mathrm{H}_{2}$ tube trailers is expensive (H2A based analyses suggest $\$ 1.45 / \mathrm{kg} \mathrm{H}_{2}$ for conventional steel tube trailers). Substantial cost reductions appear possible with development of advanced pressure vessels and/or a broadened range of thermodynamic conditions under which $\mathrm{H}_{2}$ is trucked and delivered.


Figure 1. Hydrogen Storage Thermodynamics [Contours of pressure and minimum storage energy as a function of temperature (horizontal axis), density (left axis) and volume (right axis). The circles indicate regions of interest for conventional hydrogen delivery approaches: cryogenic $\mathrm{LH}_{2}$ and ambient compressed $\mathrm{H}_{2}$ at 2,600 psi.]

Herein we report interim analysis results of both approaches to reduce the cost of hydrogen truck delivery to as low as $\$ 0.50 / \mathrm{kg} \mathrm{H}_{2}$ using H2A based analyses provided by DOE. These savings are based on the compounding of four factors (volumetric efficiency, lower burst pressure ratio, increased storage pressure, and reduced temperature) relative to conventional tube trailers. Based on these results, on a preliminary basis, we can recommend pressures as high as $7,000 \mathrm{psi}$ and cooling hydrogen to temperatures as low as 200 K for compressed hydrogen delivery by truck. Thermodynamic and infrastructure analyses will refine these conditions based on refueling station operation parameters and ranges of H 2 A economic assumptions.

## Approach

Our approach has been to first analyze what has been developed by H2A to estimate the costs of current hydrogen delivery by truck. We then analyzed the thermodynamic properties of hydrogen, materials and design for pressure vessels, and onboard storage implications to find favorable synergies aimed at achieving substantial rather than incremental overall cost reductions. We developed a range of hydrogen storage and vessel design parameters which formed the technical basis for our preliminary cost estimates using delivery cost models provided by DOE. Our general tactic has been to choose delivery parameters to reduce all cost components simultaneously rather than analyze potential tradeoffs between cost components, since the first is more likely to produce a robust result for a variety of delivery logistics scenarios.

## Results

## Cost breakdown of conventional tube trailers

Using H2A cost models provided by DOE, delivery of 2,640 psi hydrogen by conventional steel tube trailer is estimated to cost $\$ 1.44 / \mathrm{kg} \mathrm{H}_{2}$ for a 30 mile delivery distance. A cost structure examination reveals that labor, overhead, fuel, maintenance, and hazardous cargo insurance account for $\$ 0.51 / \mathrm{kg} \mathrm{H}_{2}$. These costs vary in direct proportion to the quantity of $\mathrm{H}_{2}$ delivered per trailer trip ( 340 kg H 2 for a tube trailer with 9 tube vessels pressurized to $2,640 \mathrm{psi}$ ). In addition, a $\$ 165,000$ truck tractor driven 4 trips daily and replaced every 5 years (i.e. 440,000 miles) accounts for another $\$ 0.12 / \mathrm{kg} \mathrm{H}_{2}$. The remaining $\$ 0.81 / \mathrm{kg} \mathrm{H}_{2}$ delivery cost is accounted for by the cost of the trailers themselves $(\$ 165,000$ for a 9 tube trailer with a total internal volume of $23.4 \mathrm{~m}^{3}$ ) including an annual property tax of $1.5 \%(\$ 0.09 / \mathrm{kg}$ $\mathrm{H}_{2}$ delivered).

This cost breakdown implies that deep reductions in hydrogen delivery cost will require not just trailers with lower costs, but also trailers with much greater storage capacity. The deviation of hydrogen room temperature pressure-volumetemperature (PVT) properties from the ideal gas law means that doubling the hydrogen capacity of a conventional tube trailer would require more than doubling the pressure ( $130 \%$ increase) to $6,200 \mathrm{psi}$. This in turn would more than double the weight of the vessels with a cost penalty of greater than $20 \%$ per kg of $\mathrm{H}_{2}$ capacity. This cost penalty would rise substantially if higher strength steels were required to meet gross vehicle weight maximums or maintain volumetric efficiency.

## Improving volumetric efficiency

A more cost-effective approach to higher trailer capacities is to improve volumetric efficiency. A tube trailer contains less than $400 \mathrm{~kg} \mathrm{H}_{2}$ within an internal volume of $23 \mathrm{~m}^{3}$. This volumetric efficiency is relatively low. Large liquid hydrogen delivery trucks, for example, have internal volumes as high as $57 \mathrm{~m}^{3}$, permitting storage of up to $4000 \mathrm{~kg} \mathrm{LH}_{2}$. Drawing on existing LLNL work for onboard hydrogen storage we have modeled and costed a conformable macrolattice pressure vessel design suitable for a

14 meter ( 45 ft .) long trailer, conservatively assuming a maximum external vessel volume of $56 \mathrm{~m}^{3}$, for a trailer in future widespread use.

Our design employs 1,400 identical $\sim 40$ liter unit cells built of lightweight high strength glass fiber composites ( $\sim 300,000$ psi tensile strength priced @ $3 \$ / l b)$. The design includes an isothermal burst pressure ratio of 1.7 , comparable to a safety factor of 2.25 with allowed transient overpressures of $30 \%$ from fast-fill thermal rises.

Projected volumetric efficiencies range from $85 \%$ to $50 \%$ for hydrogen pressures of 240-720 atm ( $3,600-11,000 \mathrm{psi}$ ). At 300 K these trailer designs store between $800-1200 \mathrm{~kg} \mathrm{H}_{2}$, a capacity 2-3 times greater than conventional tube trailers.

Vessel costs for these designs are estimated to be between $\$ 65,000-\$ 216,000\left(\$ 80-\$ 180\right.$ per $\mathrm{kg} \mathrm{H} \mathrm{H}_{2}$ capacity). A midrange vessel pressure of $7,000 \mathrm{psi}$ is projected to cost $\$ 133,000$. A $12 \%$ tax (as per H2A estimates for tube trailers) and $\$ 15,000$ for a trailer bed yields total projected trailer cost of $\$ 165,000-$ equivalent to a conventional tube trailer, but with a much larger storage capacity ( $1150 \mathrm{~kg} \mathrm{H}_{2}$ ). Lower pressures would reduce trailer cost, but also capacity, and increase the need for compression at the refueling station. A detailed optimization would likely result in a storage pressure below $7,000 \mathrm{psi}$, so delivery costs benchmarked to an $1150 \mathrm{~kg} \mathrm{H}{ }_{2}$ capacity 7,000 psi trailer are likely conservative.

Delivery cost estimates (Table 1) based on this 7,000 psi spreadsheet design using H2A truck delivery models are $\$ 0.92 / \mathrm{kg} \mathrm{H}_{2}$ for a $100 \mathrm{~kg} \mathrm{H}_{2} /$ day station and $\$ 0.43 / \mathrm{kg} \mathrm{H}_{2}$ for a $340 \mathrm{~kg} \mathrm{H}_{2} /$ day station (scaling station demand to account for the increased capacity of the macrolattice vessel trailer relative to conventional steel tube trailer capacities). Even if our trailer cost estimates prove optimistic by a factor of 2 (i.e. up to $\$ 330,000$ for an $1150 \mathrm{~kg} \mathrm{H}_{2}$ trailer) macrolattice hydrogen truck delivery costs would only increase from $\$ 0.43 / \mathrm{kg} \mathrm{H}_{2}$ to $\$ 0.66 / \mathrm{kg} \mathrm{H}_{2}$ at a refueling station with $340 \mathrm{~kg} \mathrm{H}_{2}$ day demand.

## Potential advantages of delivering hydrogen at reduced temperatures

Delivering hydrogen in a cooled state has multiple advantages:

- hydrogen density increases for a given pressure ( $35 \%$ for $7,000 \mathrm{psi} \mathrm{H}_{2}$ cooled to 200 K )
- colder hydrogen can reduce fast-fill onboard hydrogen vessel temperatures, improving range and/or easing vessel requirements and associated capital costs.
- colder hydrogen rises to higher pressure when warmed, potentially reducing refueling station mechanical compression requirements.
- cooling hydrogen gas reduces its mechanical stored energy substantially, improving safety. This could potentially justify lower burst pressure ratios, with further reductions in vessel material costs and improved volumetric efficiency.
- lower temperatures substantially improve the fatigue strength of glass fibers by reducing or eliminating stress corrosion from water vapor.

These advantages merit analyzing the potential of delivering cooled compressed hydrogen by truck. It is often considered that hydrogen cooling is too expensive and energy intensive for practical applications. However, Figure 1 indicates that this is not necessarily the case. Figure 1 shows that the theoretical energy requirements to achieve a given hydrogen density does not increase considerably as the hydrogen is cooled from 300 K to 200 K . This is true over a wide range of densities. Consequently we have calculated the effect of storing hydrogen at 200 K on the macrolattice trailer designs outlined earlier and found substantial potential advantages.

At 200 K the strength of S-glass fibers increases approximately $50 \%$ from room temperature. This advantage, compounded with the approximate $35 \%$ increase in hydrogen density for cooling to 200 K at 7,000 psi yields very lightweight vessels using substantially less material, yet storing substantially more hydrogen. Modifying our spreadsheet model incorporating these improved parameters results in macrolattice vessel designs for trailers storing between 1200-2000 $\mathrm{kg} \mathrm{H}_{2}$ with estimated vessel costs of $\$ 45,000-145,000$ for pressures of $3,600-$ $11,000 \mathrm{psi}$ and a temperature of 200 K . A $7,000 \mathrm{psi}$ 200 K trailer would have an $1,800 \mathrm{~kg} \mathrm{H}_{2}$ capacity and an estimated vessel cost of $\$ 90,000$. Allowing $\$ 15,000$ for a trailer bed, and $\$ 45,000$ for a thin wall vacuum jacket to maintain temperature would yield a
$\$ 165,000$ cooled macrolattice trailer (including a $12 \%$ tax noted in H2A models), corresponding to a capital cost below $\$ 100 / \mathrm{kg} \mathrm{H}_{2}$ capacity.

Using H2A cost models, 30 mile hydrogen delivery costs with such a trailer are estimated to be $\$ 0.83 / \mathrm{kg} \mathrm{H}_{2}$ for a $100 \mathrm{~kg} \mathrm{H}_{2} /$ day station, falling substantially to $\$ 0.27 / \mathrm{kg} \mathrm{H}_{2}$ for a $530 \mathrm{~kg} \mathrm{H}_{2} /$ day station (again scaled to account for the larger capacity of the macrolattice trailer relative to a conventional hydrogen tube trailer). A doubling of trailer cost to $\$ 330,000$ (roughly half the cost of an $\mathrm{LH}_{2}$ trailer) would only raise estimated delivery costs to $\$ 0.42 / \mathrm{kg} \mathrm{H}_{2}$ (Table 2).

Table 2. Preliminary Projected 30 Mile $(50 \mathrm{~km}) \mathrm{H}_{2}$ Trailer Delivery Costs

| Trailer Technology Capacity and Cost | $\$ / \mathrm{kg} \mathrm{H}_{2}$ delivered @100 kg $\mathrm{H}_{2}$ /day | $\$ / \mathrm{kg} \mathrm{H}_{2}$ delivered @ 340 kg $\mathrm{H}_{2}$ /day | $\$ / \mathrm{kg} \mathrm{H}_{2}$ delivered @ 530 kg $\mathrm{H}_{2}$ /day |
| :---: | :---: | :---: | :---: |
| 2,640 psi steel trailer $340 \mathrm{~kg} \mathrm{H}_{2}$, \$165k | \$1.44 | \$0.99 | \$0.89 |
| $7,000 \mathrm{psi}$ fiberglass $1150 \mathrm{~kg} \mathrm{H}_{2}$, $\$ 165 \mathrm{k}$ | \$0.92 | \$0.43 | \$0.35 |
| $7,000 \mathrm{psi}, 200 \mathrm{~K}$ 1800 kg H2, \$165k | \$0.83 | \$0.34 | \$0.27 |
| $7,000 \mathrm{psi}$ fiberglass $1150 \mathrm{~kg} \mathrm{H}_{2}$, \$330k | \$1.65 | \$0.66 | \$0.52 |
| $7,000 \mathrm{psi} 200 \mathrm{~K}$ 1800 kg H2, \$330k | \$1.54 | \$0.58 | \$0.42 |

Cooling and compression costs for hydrogen
All of the costs mentioned above do not include the energy and other costs of compressing and cooling hydrogen. We will examine these costs in further detail later in the year, but at present note that the theoretical minimum energy requirements to densify hydrogen at 300 K and 200 K (from atmospheric pressure at room temperature as shown in Figure 1) are small. Electricity costs of $\$ 0.05-\$ 0.08 / \mathrm{kWh}$ could imply approximately $\$ 0.10-0.20 / \mathrm{kg} \mathrm{H}_{2}$ in cooling and compression costs above room temperature cost of compression to $2,600 \mathrm{psi}$. On the other hand, the energy spent in cooling may be recoverable down stream in reduced costs or improved operations at the refueling station. In general, it is likely to be more cost effective to
cool and compress hydrogen at a large scale central plant than a smaller scale refueling station.

## Conclusions

To date we can conclude that delivery of hydrogen by more volumetrically efficient and higher storage capacity trucks can reduce the cost of hydrogen substantially, especially at station scales larger than $100 \mathrm{~kg} \mathrm{H}_{2} /$ day (up to $500 \mathrm{~kg} \mathrm{H}_{2} /$ day). A macrolattice based glass fiber composite vessel for a delivery trailer operating between $3,600-7,000 \mathrm{psi}$ will likely represent a broad optimum across the spectrum of hydrogen delivery parameters. Trailers storing 2-3 times more hydrogen ( $800-1200 \mathrm{~kg} \mathrm{H}_{2}$ ) than conventional tube trailers appear very attractive, even with somewhat conservative material cost estimates.

H2A based cost models suggest delivery costs below $\$ 0.50 / \mathrm{kg} \mathrm{H}_{2}$ appear feasible if such high capacity trailers can be developed. In addition these costs are determined chiefly by increased performance (storage capacity) than by low materials costs, lending great robustness to their relative
advantages. For example a zero cost tube trailer still has a hydrogen delivery cost of $\$ 0.63 / \mathrm{kg} \mathrm{H}_{2}$ using H 2 A models, this cost is comparable to the delivery cost estimate for an $1150 \mathrm{~kg} \mathrm{H}_{2}$ capacity $7,000 \mathrm{psi}$ macrolattice trailer costing up to $\$ 330,000$ (more than twice our actual cost estimate).

Cooling hydrogen to 200 K offers even greater delivery cost savings potential, and reduced dependence on glass fiber material costs, by increasing hydrogen storage capacities to between $1100-2000 \mathrm{~kg} \mathrm{H}$ 2 due to compounding advantages from increased hydrogen density and strength increases of glass fibers under reduced temperatures. The additional costs of cooling and counterbalancing advantages of cold hydrogen at the refueling station need to be evaluated.

## Reference

1. Gene Berry, Joel Martinez-Frias, Francisco EspinozaLoza, Salvador Aceves, "Hydrogen Storage and Transportation," Encyclopedia of Energy, Volume 3, pp. 267-281, Elsevier Academic Press, New York, 2004.
