II.C.1 High Efficiency Solar Thermochemical Reactor for Hydrogen Production

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Overall Objectives

• Verify the potential for solar thermochemical cycles for hydrogen production to be competitive in the long term and by 2020, develop this technology to produce hydrogen with a projected cost of $3/gge at the plant gate.

• Develop a high-efficiency particle bed reactor for producing hydrogen via a thermochemical water-splitting (WS) cycle, and demonstrate continuous operation on a solar simulator producing greater than 3 L of $H_2$.

Fiscal Year (FY) 2017 Objectives

• Discover and characterize suitable materials for two-step, non-volatile metal oxide thermochemical water-splitting cycles. (Barriers S and T)

• Construct and demonstrate a particle receiver-reactor capable of continuous operation at greater than 3 kW thermal input. (Barrier T)

Technical Barriers

This project addresses the following technical barriers from the Hydrogen Production section of the Fuel Cell Technologies Program Multi-Year Research, Development and Demonstration Plan.

(S) High-Temperature Robust Materials

(T) Coupling Concentrated Solar Energy and Thermochemical Cycles

(X) Chemical Reactor Development and Capital Costs

Technical Targets

This project is conducting fundamental studies on materials for use in concentrated solar power applications and designing reactor concepts that, when combined, will produce hydrogen from thermochemical WS cycles. Insights gained from these studies will be applied toward the design and optimization of a large scale solar receiver and reactor that meets the following ultimate DOE hydrogen production targets.

• Hydrogen cost: <$2/kg $H_2$

• Material of reaction cost: ≤$11,000/yr tonne per day $H_2$

• Solar-to-hydrogen conversion ratio: ≥26%

• One-sun hydrogen production rate: ≥2.1 x 10^-6 kg/s $m^2$

FY 2017 Accomplishments

• Discovered a novel perovskite material for solar thermochemical $H_2$ production. It exhibits thermodynamic cycle behavior intermediate to $SrLa_xMn_{1-x}Al_{y}O_3$ perovskite compositions (SLMA) and $CeO_2$. This is desirable because a reasonable compromise between a large reduction in temperature (like SLMA), and high WS favorability in the presence of steam and hydrogen (like $CeO_2$), will be required for commercial viability.

• Demonstrated $H_2$ production through solar thermochemical water splitting in Sandia’s cascading pressure receiver-reactor (CPR²) prototype. This was accomplished at a scale of ~3.5 kWth while achieving a peak rate of 0.2 SLPM $H_2$. The prototype validated key design objectives important to advancing the technology readiness level of this renewable WS pathway.

INTRODUCTION

This research and development project is focused on the advancement of a technology that produces hydrogen at a cost that is competitive with fossil-based fuels for transportation. A two-step, solar-driven WS thermochemical
cycle is theoretically capable of achieving a solar-to-hydrogen conversion ratio that exceeds the DOE target of 26% at a scale large enough to support an industrialized economy [1]. The challenge is to transition this technology from the laboratory to the marketplace and produce hydrogen at a cost that meets or exceeds DOE targets.

Conceptually, heat derived from concentrated solar energy can be used to reduce a metal oxide at high temperature producing oxygen (Step 1). The reduced metal oxide is then taken “off sun” and re-oxidized at lower temperature by exposure to water, thus producing hydrogen (Step 2) and completing the cycle. Commercial success of solar thermochemical hydrogen production is contingent upon developing suitable redox active materials and incorporating them into an efficient reactor. There are numerous material chemistries that have attributes suitable for inclusion in a thermochemical hydrogen production system [2-4]. The challenge is to identify an optimally performing material. In addition, the development of redox material and reactor are not mutually exclusive, but must be conducted in parallel [5]. To maximize the probability of success, this project also addresses the reactor- and system-level challenges related to the design of an efficient particle-based reactor concept [6].

**APPROACH**

Thermochemical WS reactors are heat engines that convert concentrated solar energy (heat) to chemical work. Our approach is to discover materials to accomplish the WS chemistry and pair these with a novel CPR that, when combined, can achieve an unprecedented solar-to-hydrogen conversion ratio. The material discovery work involves expanding our understanding of the underlying thermodynamics and kinetics in order to make performance improvements and/or formulate new, more redox-active compositions. Sandia’s patented CPR technology is based on a moving bed of packed particles that embodies key design attributes essential for achieving high efficiency operation: (1) sensible heat recovery; (2) spatial separation of pressure, temperature, and reaction products; (3) continuous on-sun operation; and (4) direct absorption of solar radiation by the redox-active material. Research efforts are focused on demonstrating this technology in a ~3 kW-scale prototype.

**RESULTS**

**Materials Research and Development Thrust.** Over the course of this project, Sandia and collaborators have synthesized and screened a large number of compounds looking for redox and WS activity. A general rule has emerged where materials that exhibit a large extent of reduction (δ > 0.2) generally do not split water under commercially viable oxidation conditions [7]. Moreover, we have learned that compounds with thermodynamic redox properties that are intermediate between the SLMA perovskite and CeO₂ are desirable because they represent a reasonable compromise between a large reduction extent at relatively low-temperature (like SLMA) and high WS favorability in the presence of steam and hydrogen (like CeO₂).

Recently our group found a complex perovskite (AB₇/₂₅B’₇/₇₅O₂, where A = alkaline earth metal, B’ = rare earth metal, and B’ = transition metal) that not only exhibits thermodynamic behavior between SLMA and CeO₂, but also undergoes a very interesting reversible phase transition during redox cycling that has not been reported for perovskites capable of thermochemical water splitting. Firstly, in the course of investigating a family of compounds with AB₂₅B’₇₅O₂ (0 < x < 1) stoichiometry, we found that only the AB₂₅B’₇₅O₂ (B₂₅B’₇₅) formulation was active for WS. Evidence for this is presented in Figure 1, where the plot on the left shows a strong correlation between the amount of B₂₅B’₇₅ phase present in an as-synthesized sample to the total hydrogen produced during WS experiments. Samples were prepared using the sol-gel method. Various compound stoichiometries were targeted by adjusting the mass fraction of B relative to B’ in the sol-gel liquid precursors. X-ray diffraction confirmed that targeted stoichiometries (x ≠ 0.25) having excess B or B’ were comprised of various WS inactive secondary oxide phases, mainly AB₂O₃ and AB₂O₅, along with B₂₅B’₇₅ suggesting that AB₂₅B’₇₅O₂ is a line compound.

Secondly, during an investigation of the B₂₅B’₇₅ oxygen redox cycle using thermogravimetric analysis, anomalies in the reduction behavior were discovered that were dependent upon the temperature profile and the oxygen partial pressure used in the experiment (data not shown). This prompted a more thorough look into the crystallography of B₂₅B’₇₅ during reduction using in situ high temperature X-ray diffraction; the results of which are also presented in Figure 1. The image on the right in this figure is comprised of X-ray diffraction line scans (between 23 and 32 deg. 2θ) stacked atop another with each pixel row representing a different sample temperature (298 K→1,623 K→298 K) recorded in a low O₂-partial pressure helium atmosphere (i.e., during thermal reduction). It is clear by the manner in which the colored vertical bars at various 2θ scattering angles bend (indicating changes in lattice d-spacing due to thermal and chemical effects), disappear (crystal phases reacting away), and appear (new crystal phases forming) that there is complex solid state chemistry occurring in B₂₅B’₇₅ at a temperature of 1,573 K. As mentioned previously, this chemistry does not conform to that commonly observed in other solar thermochemical hydrogen perovskite materials, and could impart high reduction entropy to B₂₅B’₇₅ that maintains WS favorability in the presence of both steam and hydrogen (data not shown).

**CPR Fabrication and Demonstration Thrust.** Sandia completed an intensive staged buildout and test campaign...
of the CPR\(^2\) that commenced in July 2016 and concluded in May 2017. The goal was to complete construction of Sandia’s moving particle bed reactor, support structure, solar simulator, and balance of plant, and then test the complete system. The assembled CPR\(^2\), which stands ~6 m tall, is pictured in Figure 2 and consists of several main components shown in a solid rendering on right, and in the photograph on left, in Figure 2. Key components of the CPR\(^2\) are a particle source chamber for pre-heating and storing ~70 kg CeO\(_2\) particles, a four-lamp, 20 kW\(_{th}\) solar simulator array for radiant heating of particles, a receiver/reactor or thermal reduction (TR) chamber to reduce particles and produce O\(_2\),

**FIGURE 1.** (Left) fractional amount of AB\(_{0.25}\)B\(_{0.75}\)O\(_y\) perovskite line compound contained in an as-prepared powder sample as a function of the target compound stoichiometry (x). The observed \(\text{H}_2\) production capacity of a powder sample tested in the stagnation flow reactor is also displayed and clearly shows a strong positive correlation between AB\(_{0.25}\)B\(_{0.75}\)O\(_y\) phase fraction and total amount of \(\text{H}_2\) produced. (Right) In situ high-temperature X-ray diffraction lines scans between 23 and 32 deg. 2\(\theta\) as a function of sample temperature measured for the AB\(_{0.25}\)B\(_{0.75}\)O\(_y\) perovskite line compound during thermal reduction. Line scan intensity reveals several diffraction peaks associated with AB\(_{0.25}\)B\(_{0.75}\)O\(_y\) polymorphs of this perovskite, and decomposition products like AB\(_x\)O\(_y\) and AB\(_x\)O\(_y\). The abrupt phase transition at ~1,573 K is reversible, and may be responsible for maintaining WS favorability at moderate \(\text{H}_2\)O:\(\text{H}_2\) ratios during re-oxidation.

**FIGURE 2.** Image and schematic of Sandia’s fully assembled and operational CPR\(^2\). PS = particle source chamber, SSIM = 4-lamp, 20 kW\(_{th}\) solar simulator, TR = thermal reduction chamber, WS = water splitting chamber, and PD = particle drain (see text for details).
a pressure separation segment, a WS reactor to oxidize particles and produce \( \text{H}_2 \), and a particle drain chamber for collecting oxidized particles. In addition, a comprehensive balance of plant subsystem inclusive of steam generator, vacuum pumps, mass flow controllers, engineered safety components, sensors, transducers, and data acquisition and control system was assembled and integrated into the CPR\(^2\) for the supply and control of gases and particles, power to lamp array, and signal inputs and outputs to the reactor. The fully functional CPR\(^2\) resides at the National Solar Thermal Test Facility in Albuquerque, New Mexico.

Figure 3 consists of selected photographs and data plots that document a successful demonstration of Sandia’s moving particle bed solar-driven thermochemical WS reactor technology. The demonstration was conducted in a single pass, once-through mode using CeO\(_2\) as the redox active material. A maximum thermal reduction temperature of 1,700 K was achieved in the radiant cavity receiver, and water splitting occurred at ~970 K (see data plots of temperature and instantaneous \( \text{H}_2 \) flowrate in Figure 3). The topmost image shows the receiver cavity looking through the aperture during simulator illumination. Owing to the high-temperature incandescence and reflection from the quartz dome covering the aperture, it is difficult to observe particle flow in the receiver itself. However, the diffuse glow of incandescent particles falling from the receiver through a translucent alumina tube, and a small windowed chamber positioned beneath it, attest to hot particles falling into the WS. Two different techniques were used to measure \( \text{H}_2 \) production rate, a standard heat capacity-based mass flow meter and a Sandia patented solid state sensing device.

In summary, Sandia and collaborators designed, fabricated, and demonstrated \( \text{H}_2 \) production through thermochemical water splitting in the CPR\(^2\) prototype. This was accomplished at a scale of ~3.5 kW\(\text{th} \) (20 kW\(\text{e} \)) while achieving a peak rate of 0.2 SLPM \( \text{H}_2 \). In so doing, our prototype validated the following design objectives: (1) continuous and direct irradiation of redox material without particle shading, (2) precise control of particle flow rate and residence time in the TR, (3) pressure separation without internal mechanical components like valves, and (4) counter-flow mass exchange between steam and particles in WS (i.e., no mixing or fluidization during re-oxidation). Successful validation of these design objectives builds on knowledge needed to verify the potential for this hydrogen production technology to be cost competitive in the future, and critical to

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{figure3.png}
\caption{(Left) images of the CPR\(^2\) during operation. Starting from top to bottom, CeO\(_2\) particles are heated by simulated solar radiation (~3.5 kW\(\text{th} \) at the aperture) to ~1,700 K where \( \text{O}_2 \) is removed from the solid by vacuum pumping the TR. The radiant cavity through which CeO\(_2\) particles flow is seen looking through the quartz dome in topmost picture. Particles then move by gravity through connecting chambers and collect in the WS. Incandescence from falling particles is clearly visible through viewports on the connecting chambers. Once a sufficient amount of reduced CeO\(_2\) accumulates in the WS, steam is introduced causing the spontaneous re-oxidation of CeO\(_2\) and production of \( \text{H}_2 \). (Right) selected excerpts of data streams from the CPR\(^2\) data acquisition and control system showing temperature readings from various locations within the system and instantaneous \( \text{H}_2 \) flowrate as a function of run time during a test.}
\end{figure}
advancing the technology readiness of Sandia’s concept for implementing a high-temperature, two-step thermochemical water splitting cycle.

**CONCLUSIONS AND UPCOMING ACTIVITIES**

- Discovering a redox material that will meet or exceed DOE cost and performance targets. We anticipate that investments made by DOE’s Hydrogen Advanced Water Splitting Materials Consortium (found at http://h2awsm.org) will focus on advancing the material discovery effort.
- Establishing the CPR as a “routine-use” R&D tool to support seedling projects in Hydrogen Advanced Water Splitting Materials Consortium as well as engage commercial interest and investment.
- Publish all project results in peer-reviewed journals.

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**FY 2017 SELECTED PUBLICATIONS/PRESENTATIONS**


**REFERENCES**


