

2007 DOE Hydrogen Program Review Hydrogen Storage by Spillover

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> > **Project ID: ST3**

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Overview

Timeline

Barriers

- Project start date: FY05
- Project end date: FY10
- Percent complete: 45%

Budget

- Total project funding
 - DOE share: \$939,356
 - Contractor share: \$280,000
- Funding received in FY06: \$225,000
- Funding for FY07: \$225,000

- General
 - Weight & Volume
 - Rates (Refueling and discharge)
- Reversible Solid-State Material
 - Hydrogen Capacity & Reversibility
 - Lack of Understanding of H₂
 Spillover

Partners

- Sample/adsorbed H
 Verification, Characterization & Mechanism
 NREL, NIST, Rice U
- Plan industrial collaboration after the initial phase of study and sorbent optimization

Project Objectives

- To develop hydrogen storage materials with capacities in excess of 6 wt% (and 45 g/L) at room temperature by using the spillover mechanism
 - To develop and optimize our new Bridge-Building techniques for spillover to enhance hydrogen storage
 - To develop direct doping techniques for spillover
 - To obtain a mechanistic understanding for hydrogen spillover in nanostructured carbon-based materials for the purpose of hydrogen storage



Technical Approach

Strategy for storage by spillover: (A) Supported metal catalyst for H_2 dissociation; (B) Sorbent as receptor for H; (C) Building carbon bridges (by carbonization of a precursor) for spillover, resulting in a composite sorbent. (Yang et al., U.S. Patent application filed, 2005)



Technical Accomplishments/ Progress/Results

Isotherms measured at 298K on Pt/AC catalyst (10%) and IRMOF-8 (80 or 90%)



- Spillover can significantly enhance H_2 capacity.
- Bridge building can further increase H_2 capacity.
- MOFs are unstable as they decompose in ambient air (by hydrolysis), and are difficult to reproduce as shown by Samples 1-3 (by the same procedure).

* All H_2 uptake values in this work are excess capacities.

High-pressure Hydrogen Isotherms at 298 K on 6 wt%Pt/AX-21 by a new (direct) doping technique (error bars based on 1σ of 4 samples)



- Spillover can significantly enhance H_2 capacity on AX-21
- Unlike MOFs, AX-21 is more stable and the H_2 capacities are reproducible.
- The data on Pt/AX-21 have been validated by DOE.
- Kinetics of spillover are slow; understanding of kinetics and mechanism is crucial for further development.

Low-P H₂ Adsorption Isotherms on Bridged IRMOF-8 (with Pt/AC Catalyst)



• Hydrogen storage capacity by spillover is temperature dependent

• From the temperature dependence, **the binding energies (isosteric heats of adsorption) are in the ideal range for storage: -24.8 kJ/mol** (at 0.0078wt%), -**21.3 kJ/mol** (at 0.0108wt%) and **-20.1 kJ/mol** (at 0.0137wt%).

IRMOF-8 Model used for Molecular Orbital Computation (*left*) and Energy of Adsorption (E_{ads}) for 1 H Atom on Each Site of IRMOF (*right*)



- Spillover H can form weak bonds with all sites of MOF.
- Two H atoms could bond with each O site.
- The bond energies agree with the experimental heats of adsorption.

• The **theoretical maximum amount** for IRMOF-8 by spillover is **7wt%** (or **71.4 g/L by volume**), which are promising for meeting 2010 DOE system wt. & vol. targets of 6wt% & 45g/L.

Hydrogen Adsorption Kinetics on Bridged IRMOF-8 (Q_w= Equilibrium Amount)



- Spillover is very fast at low pressures
- The <u>activation energy for surface diffusion</u> is 9.3 kJ/mol for H on bridged IRMOF-8, ~ 1/2 to 1/3 of the binding energies
- <u>Surface diffusion time constant</u>, <u>D/R</u>², can be calculated from the uptake rate. But what is R?

Simple 2-D Model for Hydrogen Spillover on Bridged IRMOF-8 including Pt/AC Catalyst (AC: Activated Carbon)



- Spillover is rate-limited by surface diffusion of H on receptor (not H_2 dissociation on Pt)
- R_2 is the radius of diffusion for D/R²
- R depends on connectivity between receptor particles, and is increased by bridge building

Rates of Adsorption (*l*), and Desorption (*r*) at Different Pressures on Bridged IRMOF-8 (T = 298 K). Q_{∞} = Equilibrium Adsorption (a) or Desorption (b) Amount at Each Pressure



- Rates for both adsorption and desorption are fast at low loadings but become slower at higher loadings
- Desorption is faster than adsorption
- Desorption (or discharge) rate is fast enough for powering vehicle at 60 or 70 miles/hour

D/R² as Function of H₂ Loading at 298 K for Bridged IRMOF-8



- Diffusion time constant (D/R^2) declines with loading
- Diffusivity (D) does not decline with loading; thus, R increases with loading
- This result is strong evidence that the spiltover H also serves as bridges

Concentration Dependence of R (in D/R²)



- The diffusion distance for spillover (R) increases with loading (q)
- The dependence can be expressed as $R = kq^{1/3}$

Model for Adsorption on Spillover Systems:

Equilibrium constant K₁ that relates the surface concentration (C) of H on activated carbon support to that on Pt:

$$K_1 = \frac{C_{AC}}{C_{Pt}}$$

Likewise, K₂ is the equilibrium constant between MOF and Pt:

$$K_2 = \frac{C_{MOF}}{C_{Pt}}$$

At equilibrium, the total amount adsorbed (on AC and MOF):

$$q = K_1 q_{Pt} + \left(\frac{R_2}{R_1}\right)^3 K_2 q_{Pt}$$

where the isotherm on Pt is given by Langmuir (1918):

$$q_{Pt} = \frac{k_1 \sqrt{P_{H_2}}}{1 + k_2 \sqrt{P_{H_2}}}$$
 and $R_2 = k' q^{1/3}$

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Substituting q_{Pt} and R_2 into the isotherm, one gets:

$$q = \frac{K_1 k_1 \sqrt{P_{H_2}}}{1 + k_2 \sqrt{P_{H_2}} - K' k_1 \sqrt{P_{H_2}}}$$

where
$$K' = \left(\frac{k'}{R_1}\right)^3 K_2$$

This is the equilibrium isotherm for the spillover system. It's shape can be concave, convex or linear.....

At the limit of very high pressures:

$$q \cong \frac{K_1 k_1}{k_2 - K' k_1}$$

 The first model for equilibrium isotherm for spillover is developed and verified.

Future work plan/Objectives

- Storage by spillover with bridge-building on other high surface area MOFs: MIL-101, COF-1 (Covalent organic framework), and MOF-177
- New direct doping techniques on AX-21 and other ultra-highsurface-area carbons
- Test other promising receptors (sorbents) (for sorbent candidates, see R. T. Yang, *Adsorbents: Fundamentals and Applications,* Wiley, New York, 2003)
- Test different catalysts and bridge-building precursors, as well as techniques for bridge building
- Obtain basic understanding of the spillover process including equilibrium and kinetics, using deuterium isotope
- To achieve the 4.5 wt% (36 g/L) DOE (interim) system target at 298K in FY2007
- To address issues on fueling rates and other DOE targets

Summary

- H₂ dissociation and spillover can significantly increase the H₂ storage capacity at ambient temperature.
- Bridge building facilitates spillover thereby enhances storage.
- The binding energies of the spiltover hydrogen are in the ideal range of 20-25 kJ/mol for storage applications.
- The discharge rates of the spiltover hydrogen at ambient. temperature are fast enough for automotive applications, but the charging rates at ambient temperature are slow.
- The model developed in this work is useful to those performing atomistic calculations (e.g., Boris Yakobson)
- Further understanding for the mechanism of spillover/storage is needed.
- Further development for different sorbent/catalyst/bridges is needed.

Summary Table

All data are @ 298K (Room Temperature)

On-Board Hydrogen Storage System Targets

(*Data based on material only, not system value) (** Based on a bulk density of 1.02 g/cm³ for MOF-8)

Sorbent	Storage Parameter	Units	2010 System Target	FY06 Result*	FY07 Result*	Notes
Bridged IRMOF-8	Wt. Storage Capacity	wt % H ₂	6 wt%	4 wt%	2.2-4 wt%	Highly unstable; low reproducibility
	Vol. Storage Capacity	Kg H ₂ /L	45 g/L	40.8 g/L**		
	Desorption Temperature			298K	298K	
Metal/Carbon (Pt/AX-21)	Wt. Storage Capacity				1.2 wt%	More stable; Reproducible; Validated by NREL
	Vol. Storage Capacity					
	Desorption Temperature				298K	