

# Materials Solutions for Hydrogen Delivery in Pipelines

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Project ID: PD18

# Overview

## Timeline

- Project start date: 05/2005
- Project end date: 09/2009
- Percent complete: 25%

## Budget

- Total project funding
  - \$1650K (DOE share)
  - \$1110K (contractor share)
- Funding for FY 07: \$200K
- Funding for FY 08: \$350K

## Barriers and Targets

### Barriers addressed

High capital cost and Hydrogen Embrittlement of Pipelines

### Technical Targets (2017):

- Capital cost (\$490K/Mile Transmission)
- Cost of delivery of hydrogen <\$1.00/gge
- High Reliability of operation with metrics to be determined

## Partners

### SECAT CONSORTIUM

- Advanced Technology Corporation
- ASME Standards and Technologies
- Chemical Composite Coatings Intl
- Columbia Gas of Kentucky
- Oregon Steel Mills
- Schott North America
- DGS Metallurgical Solutions, Inc.
- Hatch Moss MacDonald
- Oak Ridge National Laboratory
- University of Illinois

# Objective and Deliverables

## Objective:

- Develop materials technologies to minimize embrittlement of steels used for high-pressure transport of hydrogen

## Deliverables:

- Identify steel compositions/microstructures suitable for construction of new pipeline infrastructure
- Develop barrier coatings for minimizing hydrogen permeation in pipelines and associated processes – **ON HOLD per DOE**
- Understand the economics of implementing new technologies

# Known/Unknown

- **Known**

- Variability of microstructure within a grade i.e. not all X52, X70, etc. is created equal
- Disassociation of  $H_2$  to H required
- Disassociation causes – Corrosion, Partial Pressures
- Surface oxide layers can inhibit diffusion of hydrogen into the steel
- H migrates/collects in area of high residual stress (50% of residual stress due to microstructure mismatch, inclusions, thermal, mechanical)

- **Unknown**

- $H_2$  embrittlement of steels/welds in high pressure dry gaseous  $H_2$
- Effect on steel metallurgical microstructures in high pressure dry gaseous  $H_2$
- Effectiveness of non-metallic coatings in minimizing  $H_2$  issues
- Economics of technical solutions not qualified
- Is common X70 microstructure suitable in high pressure dry gaseous  $H_2$  (Volume fraction? Banding? Moisture/corrosion?)
- Suitability of alternative microstructures in high pressure dry gaseous  $H_2$  (Volume fraction? Banding? Moisture/corrosion?)

# Major Tasks

**Task 1:** Evaluate hydrogen embrittlement characteristics of existing commercial pipeline base steels/microstructures and welds under high-pressure hydrogen gas

**Task 2:** Evaluate hydrogen embrittlement characteristics of existing commercial alternative alloy/microstructure steels under high-pressure hydrogen gas

**Task 3:** Develop Alternate Alloys/microstructure and welding consumables and Evaluate Hydrogen Embrittlement

**Task 4:** Financial Analysis and Incorporation into Codes and Standards

Note – Tasks related to coatings have been placed on hold and are not represented here.

# Progress To Date

## a) **Four (4) commercial pipeline steels have been down-selected – Task 1**

- Majority of the baseline pipeline steel microstructure and mechanical property data have been characterized
- Commercial X70 pipeline welds have been secured for future work
- Two (2) traditional screening tests have been explored
- *In-situ* ABI test has been developed
- Processing techniques developed for glassy coatings
- Down-selected steel composition has been coated
  - For evaluation in high pressure hydrogen gas
  - Evaluation of coating technique effect on steel microstructure.

## b) **Two (2) commercial abrasion resistant/structural steels have been down-selected – Task 2**

- Low carbon-high alloy capable of producing 100% bainite or 100% martensite microstructures (dependant on processing) with good toughness
- Medium carbon-high alloy capable of producing 100% bainite or 100% martensite microstructures (dependant on processing) with good toughness

# Down-selected Commercial Pipeline Steel Compositions – Task 1

Grade*	Code	Carbon	Microstructure	Comment
X70 Std	A	0.08	Ferrite/Pearlite	Baseline
X70/X80	B	0.05	Ferrite/Acicular Ferrite	Potentially Good
X70/X80	C	0.04	Ferrite/Acicular Ferrite/Sm Pearlite	Potentially Good
X52/X60 HIC	D	0.03	Ferrite/Acicular Ferrite	Potentially Best

\*Note that all are commercially available pipeline base steels utilizing microalloying technology.

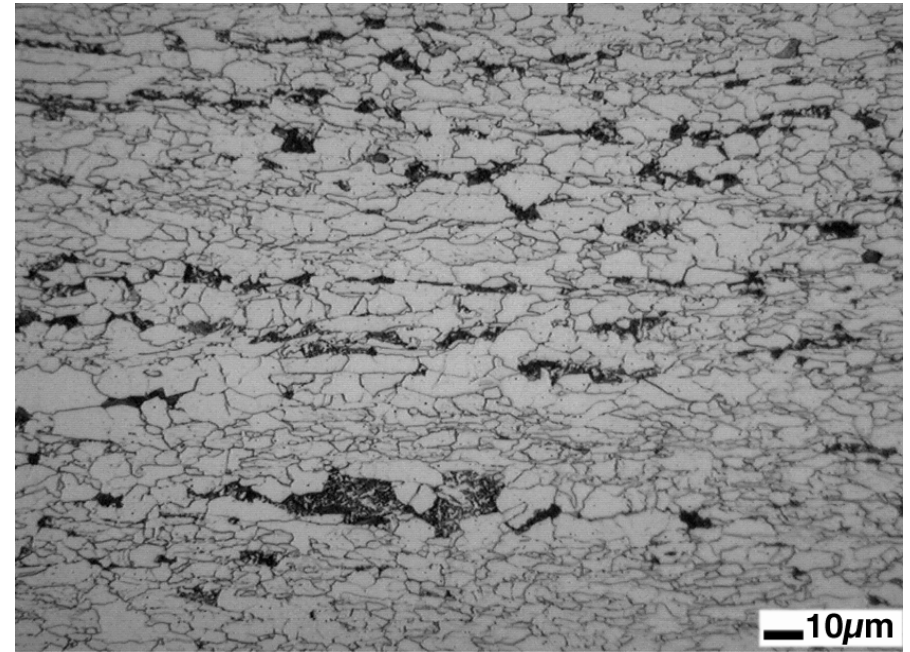
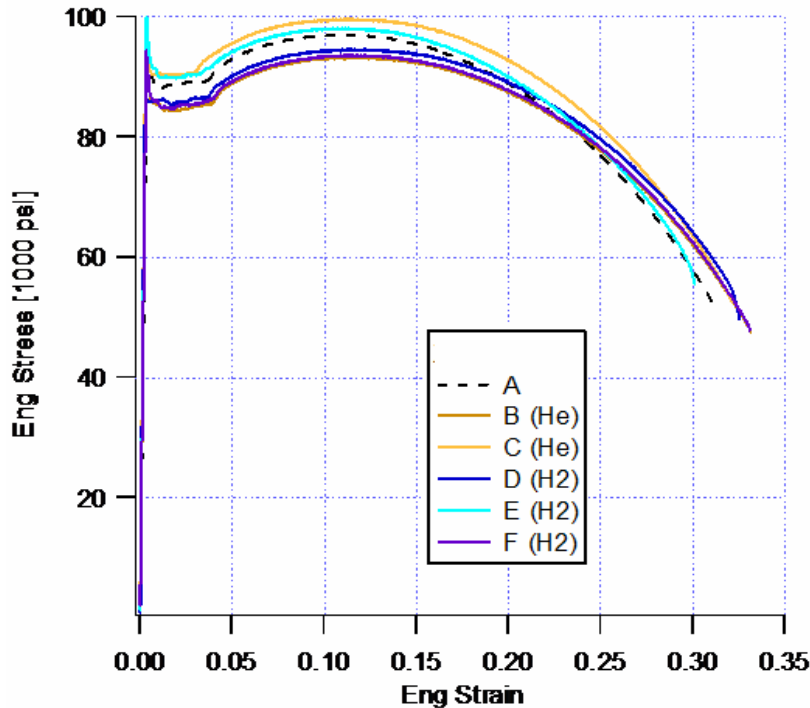
# Down-selected Commercial Abrasion Resistant/Structural Alternative Steel Compositions/Microstructures – Task 2

Grade*	Code	Carbon	Alloy	Microstructure	Comment
100 KSI Yield Strength	E	0.08	Mn, Ni, Nb, B, Ti	100% Bainite or Martensite dependent on processing	Potentially Good
Abrasion Resistant 400 BHN	F	0.15	Mn, Si, Cr, Mo, Nb, B, Ti	100% Bainite or Martensite dependent on processing	Potentially Good

\*Note that all are commercially available structural/abrasion resistant base steels utilizing solute solution strengthening and boron/microalloying technology



# Effect of Hydrogen on the Mechanical Properties of Steel A – Ex-situ Testing



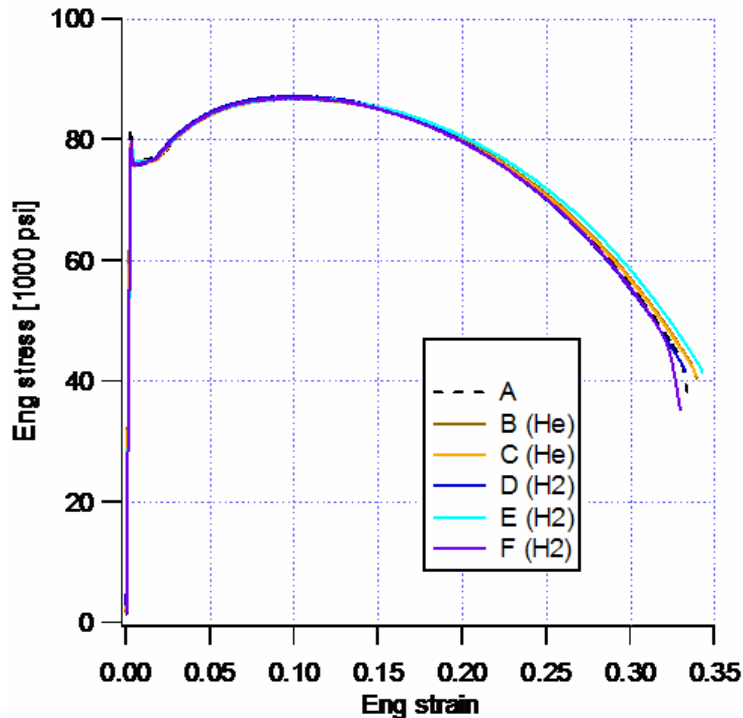
20 KSI H<sub>2</sub> @ 100 °C for 8 days  
5 KSI He @ 100 °C for 8 days  
Strain rate 10<sup>-4</sup> in/in/sec

## Ferrite + Pearlite

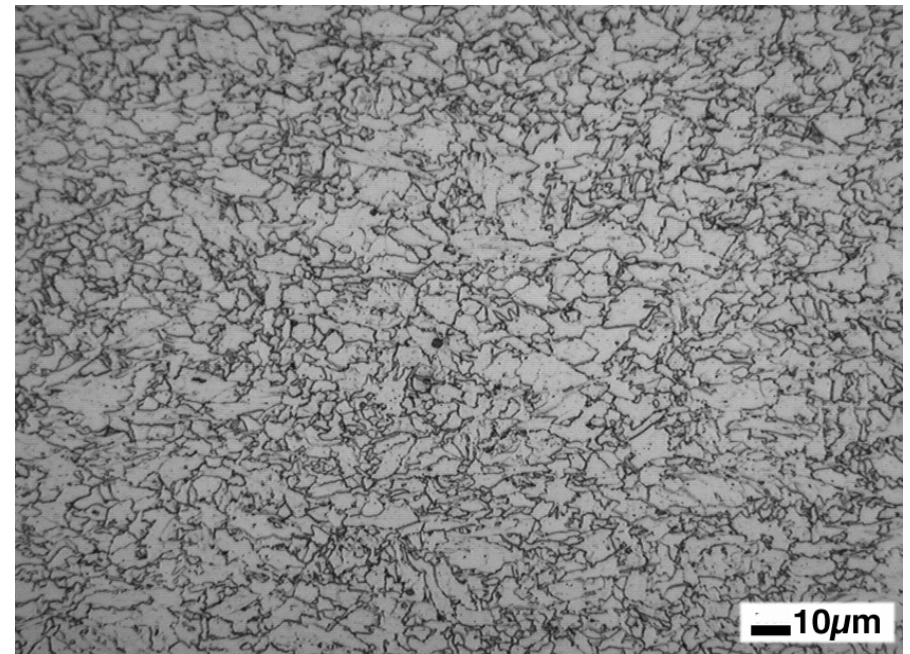
Surface to ¼ thick – 4.13% volume fraction pearlite  
¼ thick to centerline – 8.40% volume fraction pearlite  
Centerline – 6.90% volume fraction pearlite

Note the relatively large variability of stress-strain curves

# Effect of Hydrogen on the Mechanical Properties of Steel B – Ex-situ Testing



20 KSI H<sub>2</sub> @ 100 °C for 8 days  
5 KSI He @ 100 °C for 8 days  
Strain rate 10<sup>-4</sup> in/in/sec

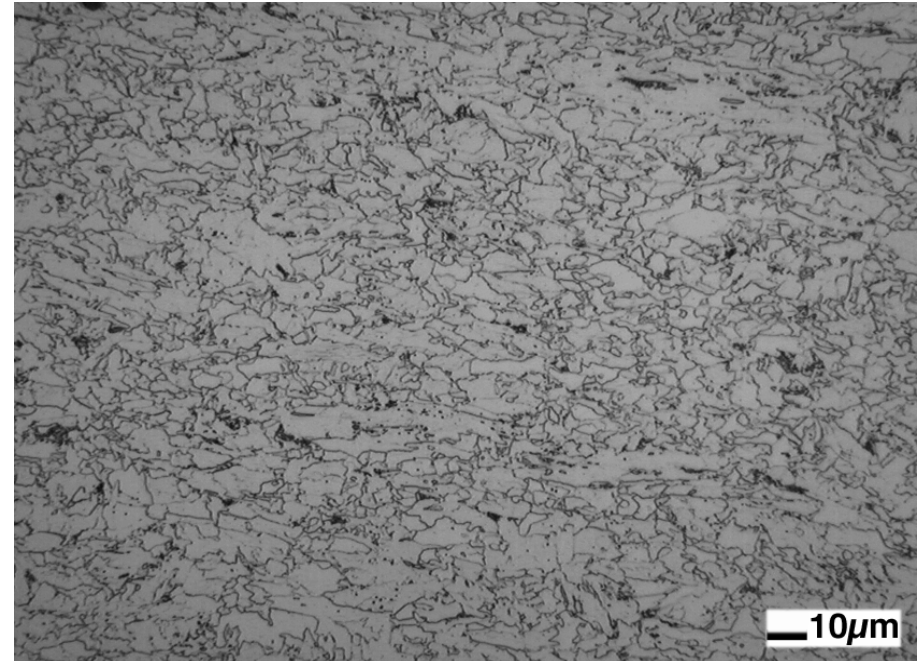
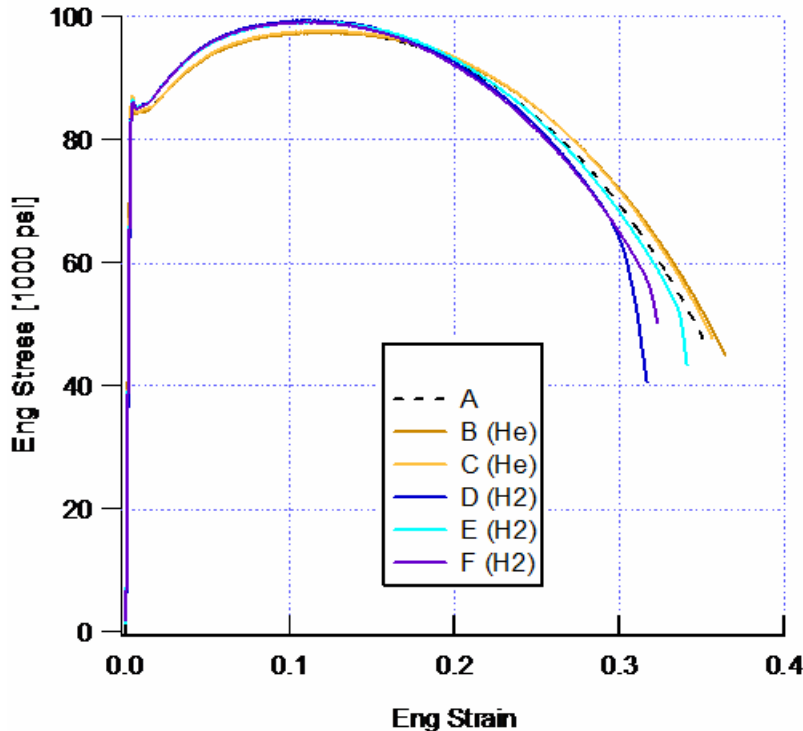


## Ferrite + Acicular Ferrite

Surface to ¼ thick – Acicular ferrite TBD by TEM  
¼ thick to centerline – Acicular ferrite TBD by TEM  
Centerline – Acicular ferrite TBD by TEM

Note the relatively small variation in the stress-strain curves

# Effect of Hydrogen on the Mechanical Properties of Steel C – Ex-situ Testing



**Ferrite/acicular ferrite + sm pearlite**

20 KSI H<sub>2</sub> @ 100 °C for 8 days  
5 KSI He @ 100 °C for 8 days  
Strain rate 10<sup>-4</sup> in/in/sec

Surface to ¼ thick – AF TBD by TEM, pearlite TBD  
¼ thick to centerline – AF TBD by TEM, pearlite TBD  
Centerline – AF TBD by TEM, pearlite ≈ 3%

Note intermediate variability in the stress-strain curves

# NACE Hydrogen Induced Cracking (HIC) Test

- Evaluates resistance of pipeline and pressure vessel plate steels to Hydrogen Induced Cracking (HIC) caused by hydrogen adsorption through a corrosive mechanism
- Cracks that develop in the microstructure are evaluated transverse to the rolling direction
- UNSTRESSED test specimens are immersed in one of two H<sub>2</sub>S containing solutions for 96 hours – Solution A (Low pH – more severe), Solution B (High pH – less severe)
- Test provides reproducible environments for distinguishing RELATIVE susceptibility to HIC in a relatively SHORT TIME

# NACE HIC Testing of Selected Pipeline Steels

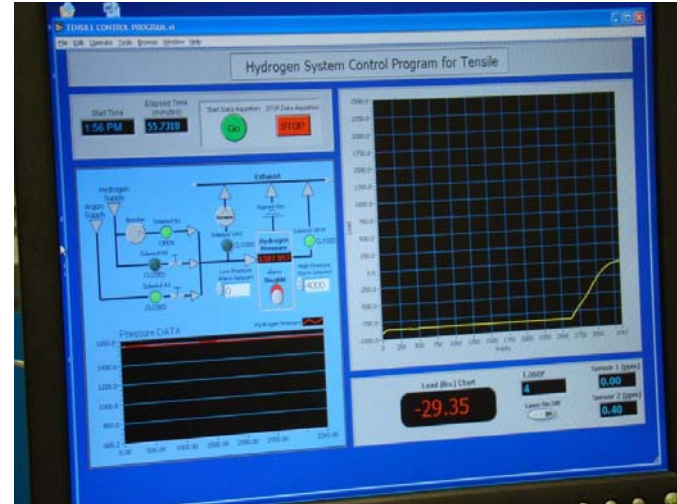
<b>Alloy</b>	<b>Crack Length Ratio (%)</b>	<b>Crack Sensitivity Ratio (%)</b>	<b>Crack Thickness Ratio (%)</b>
<b>A</b>	<b>11.8<sup>a</sup></b>	<b>0</b>	<b>0.1</b>
<b>B</b>	<b>0.4<sup>b</sup></b>	<b>0</b>	<b>0</b>
<b>C</b>	<b>0</b>	<b>0</b>	<b>0</b>
<b>D</b>	<b>0</b>	<b>0</b>	<b>0</b>

a) Cracks located at the ferrite/pearlite interface

b) Cracks located between surface and  $\frac{1}{4}$  thickness and associated with cluster of non-metallic inclusions (related to  $\frac{1}{4}$  thickness casting inclusion issue)

**Lower numbers are desirable**

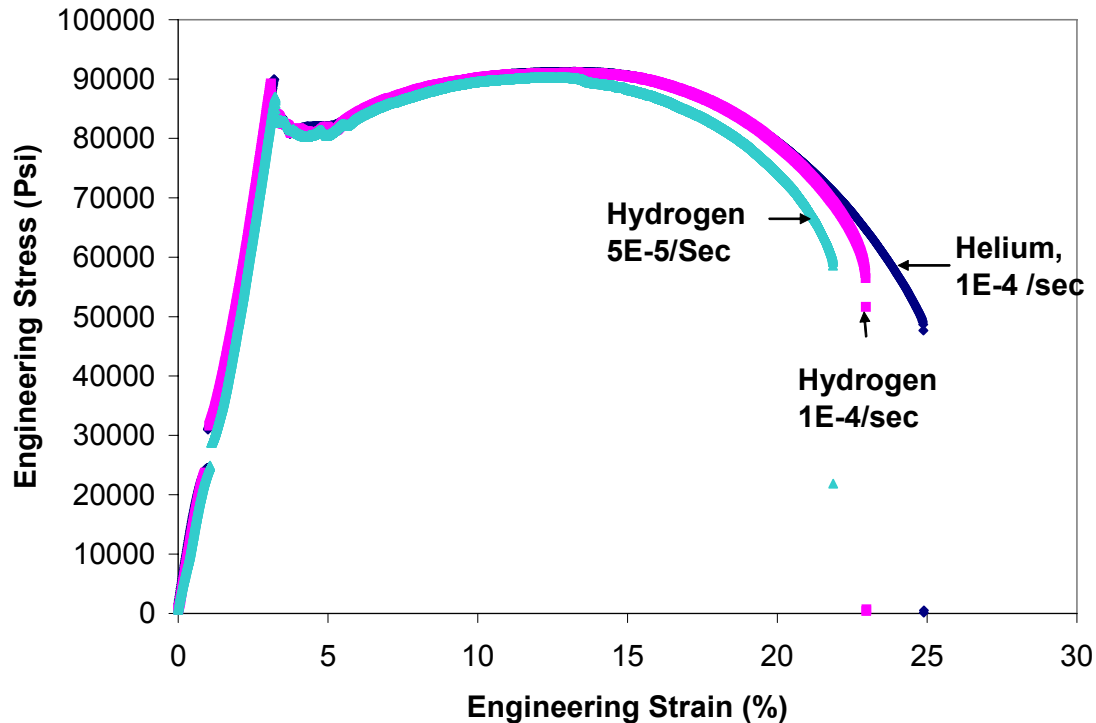
# System for *in-situ* Testing in High Pressure Hydrogen is Now Fully Functional at ORNL



## Key features

- Room temperature gas pressures up to 4800 psi
- Strain rates down to  $1\text{E-}6/\text{sec}$
- Test loads up to 4000 lbs
- Flexible specimen geometry
- Computer-controlled valves and data acquisition

# Effect of Strain Rates on Stress-Strain Curves in Hydrogen Atmosphere for Alloy A



Note: Friction correction has NOT been applied

- Gas compositions used: UHP hydrogen (99.9999%), UHP Helium (99.9999%)
- Gas pressure: 1580 psi
- Presence of hydrogen decreases total strain to failure
- The decrease in total strain is a function of the strain rate used for testing

# Fracture Mode of Steel A Changes in the Presence of Hydrogen



**Helium**

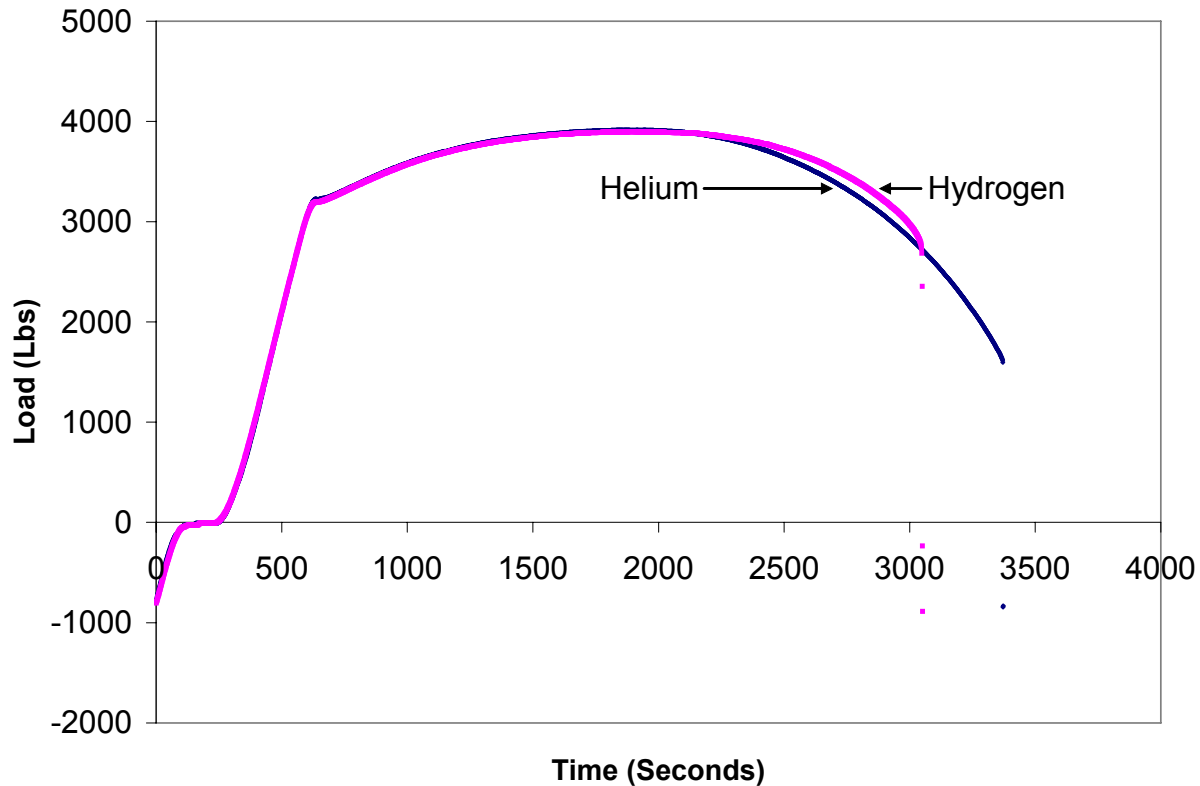
Ductile cup and cone fracture

**Hydrogen**

Faceted fracture surface with evidence for multiple secondary cracking



# Effect of Hydrogen on Deformation Characteristics of Alloy C



- Pressure: 1580 psi, Strain rate: 1E-4 /sec
- Total elongation decreases in a hydrogen atmosphere

# Fracture Mode of Steel C Also Changes in the Presence of Hydrogen



**Helium**

Ductile cup and cone fracture



**Hydrogen**

Faceted fracture surface with visible secondary cracking

# Future Work

- **Steels**
  - Complete measurement of mechanical properties *in-situ* high pressure hydrogen testing of commercial pipeline steels and commercial alternative microstructures
  - Evaluate effect of different strain rates for *in-situ* testing
  - Complete microstructural characterization of down-selected steels before and after exposure to hydrogen to understand the effect of microstructure on embrittlement
  - Evaluate *in-situ* fatigue testing of commercial pipeline steels and alternative microstructures
  - Perform and evaluate baseline fracture mechanics characteristics
- **Economic Analysis**
  - Recommend steel and coating systems for implementation
  - Evaluate economic impact of suggested materials systems

# Contacts

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