

Composite Pd and Alloy Porous Stainless Steel Membranes for Hydrogen Production and Process Intensification

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Overview

Timeline

- Start : 5/7/2007
- Finish : 5/6/2010
- 61% Complete

Budget

- Total Project Cost: \$ 1,602,922
 - DOE Share: \$ 1,256,226
 - Recipient Share: \$ 346,696
- Funding Received:
 - FY08: \$ 442,785
 - FY09: \$ 420,638
- DOE Award #: DE-FC26-07NT43058
- DOE Project Manager:
Dr. Daniel Driscoll

Subcontractor

- Adsorption Research Inc. (ARI)

Barriers

- Barriers Addressed:
 - Long-term selectivity stability
 - H₂ flux targets
 - Mixed gas & WGS reaction studies
 - CMR modeling simulations
 - Process intensification
 - Absorbent selection and testing

→ Technical Targets**

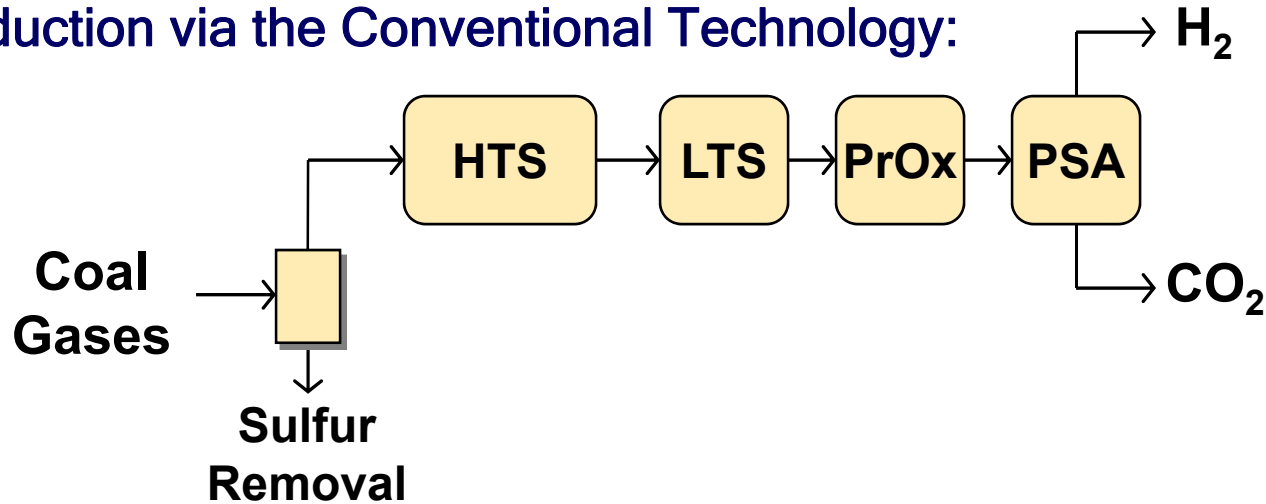
| | H ₂ Flux [scfh/ft ²] § | Temp. [°C] | ΔP max. [psi] | H ₂ Purity | Sulfur Tolerance |
|--|--|---------------|------------------|--------------------------|---------------------|
| 2010 | 200 | 300-600 | 400 | 99.5% | 20 ppm |
| 2015 | 300 | 250-500 | 800-1000 | 99.9% | >100 ppm |
| § @ 100 psi ΔP H ₂ partial pressure | | | | | |
| CO Tolerance: Yes; WGS Activity: Yes | | | | | |

Project Objectives & Relevance

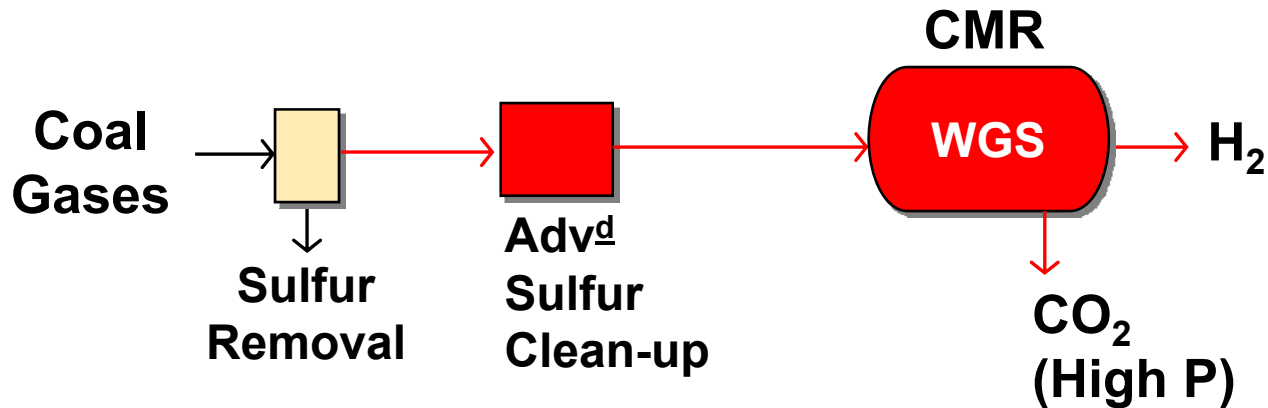
- Synthesis of composite Pd and Pd/alloy porous Inconel membranes for WGS shift reactors with long-term thermal, chemical and mechanical stability with special emphasis on the stability of hydrogen flux and selectivity
- Demonstration of the effectiveness and long-term stability of the WGS membrane shift reactor for the production of fuel-cell quality hydrogen
- Research and development of advanced gas clean-up technologies for sulfur removal to reduce the sulfur compounds to <2 ppm
- Development of a systematic framework towards process intensification to achieve higher efficiencies and enhanced performance at a lower cost
- Rigorous analysis and characterization of the behavior of the resulting overall process system, as well as the design of reliable control and supervision/monitoring systems
- Assessment of the economic viability of the proposed intensification strategy through a comprehensive calculation of the cost of energy output and its determinants (capital cost, operation cost, fuel cost, etc.), followed by comparative studies against other existing pertinent energy technologies

Approach: Coal Gasification & CMR

H₂ Production via the Conventional Technology:



Novel Catalytic Membrane Reactor (CMR):



Project Schedule & Milestones

| Tasks | Year 1 | | | | Year 2 | | | | Year 3 | | | |
|--|--------|------|------|------|--------|------|----|----|--------|----|----|----|
| | Q1 | Q2 | Q3 | Q4 | Q1 | Q2 | Q3 | Q4 | Q1 | Q2 | Q3 | Q4 |
| | Months | | | | | | | | | | | |
| | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 | 27 | 30 | 33 | 36 |
| Gas Clean-up & Fast PSA using Structured Adsorbent | | | M1 ✓ | | G1 ✓ | | | | | | | |
| | | | | | | M2 ✓ | | | | | | |
| Membrane Synthesis | | | | | | | | | | | | |
| | | M4 ✓ | | | | | | | | M3 | | |
| Membrane Characterization & Reactor Performance | | | | | | | | | | | | |
| | | | | M5 ✓ | | | | G2 | | | | |
| Membrane Reactor Modeling | | | | | | | | | | | | |
| | | | | | | M6 ✓ | | | | | | |
| Process Intensification | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Process Control System; Design & Implementation | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Process Monitoring System; Design & Implementation | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Program Management & Reporting | | | | | | | | | | | | |
| | | | | | | | | | | | | |

Membrane Properties & Permeation Test Set-up

➤ Membrane:

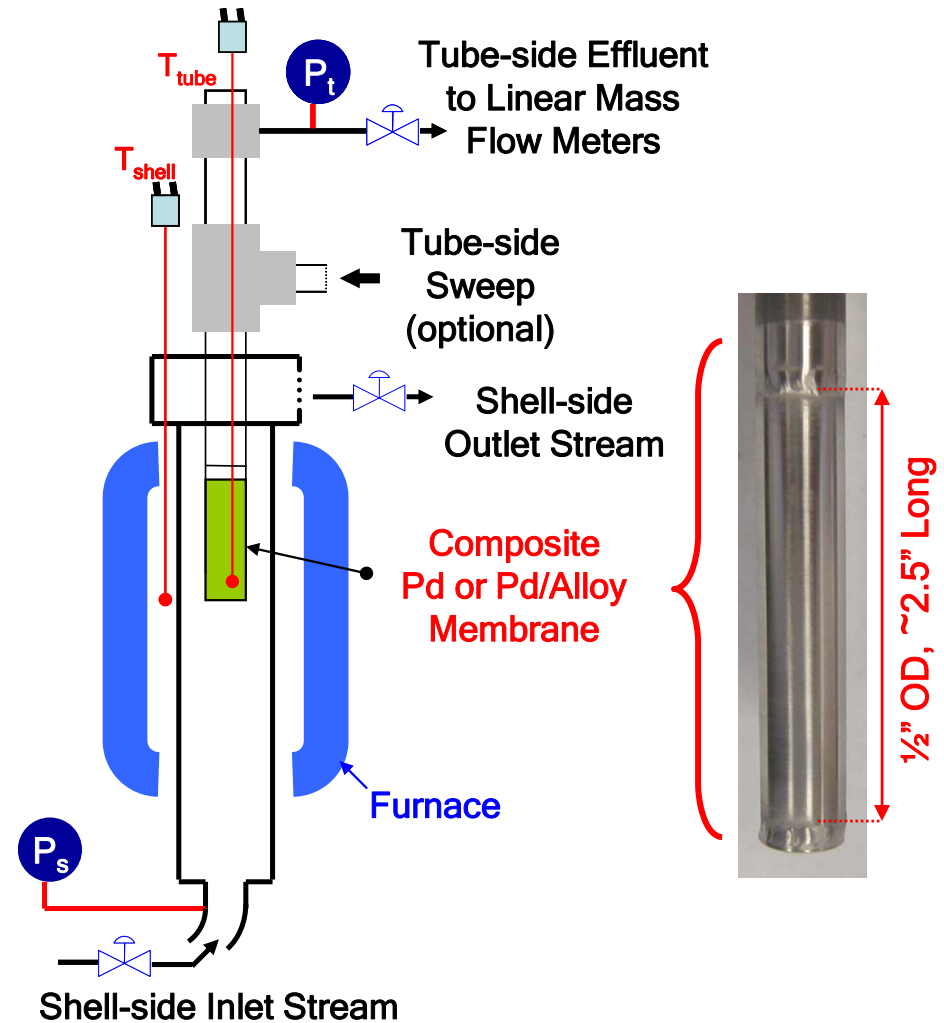
Pd supported on porous Inconel (media grade 0.1 μm)

➤ Method of Preparation: Electroless Plating

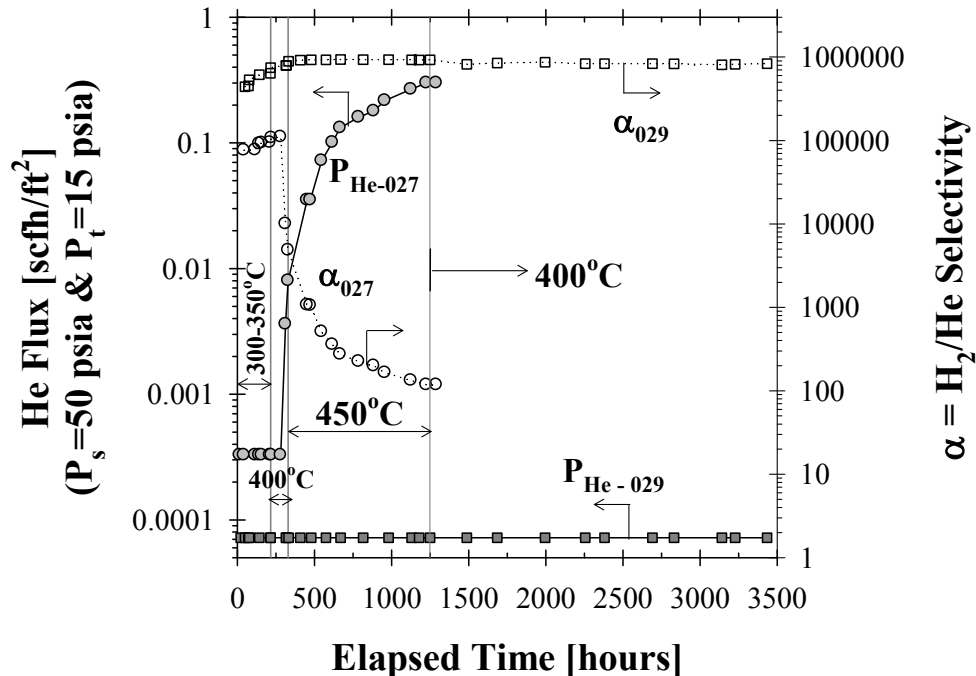
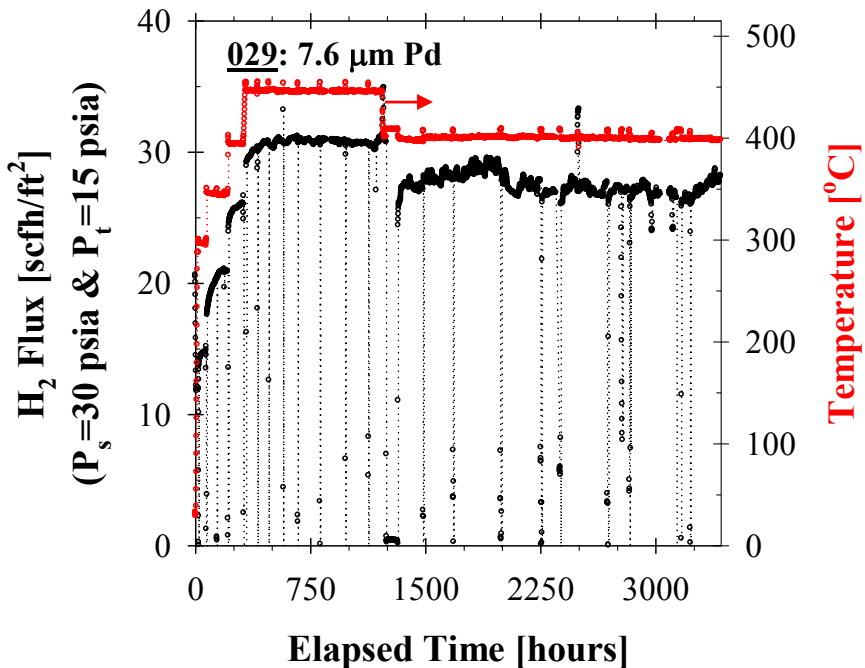
➤ Geometry:

Tubular (Plated on the outside of a tube)

➤ Membrane Area $\approx 25 \text{ cm}^2$

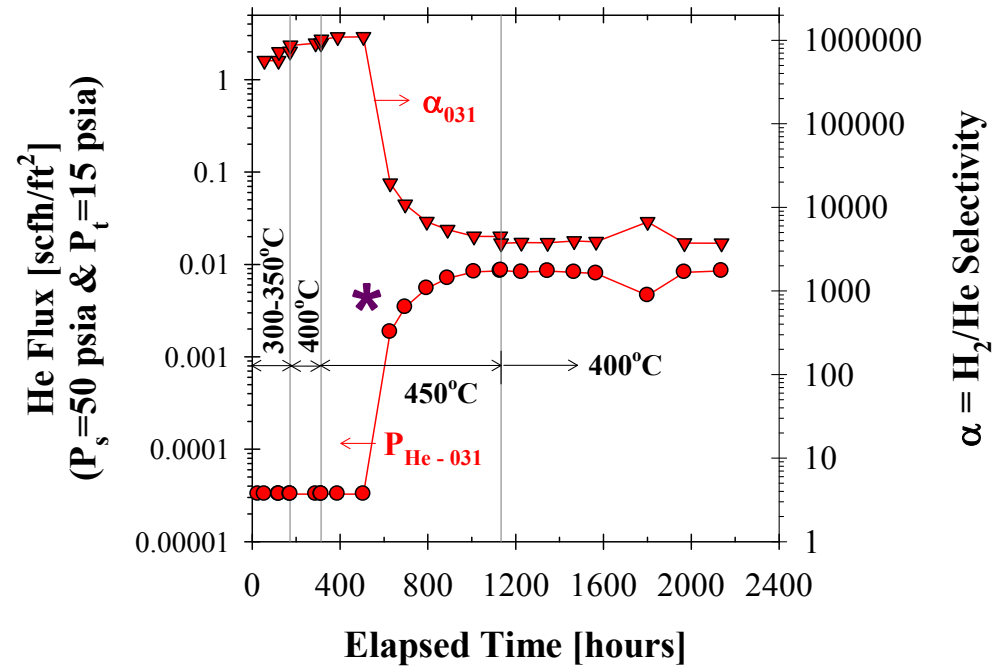
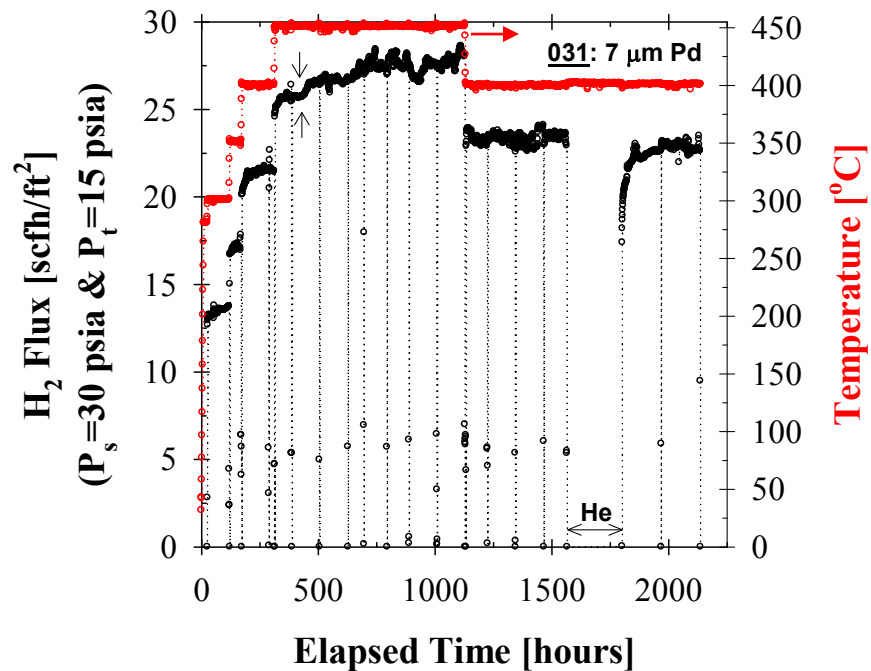


Long-Term Selectivity Stability



- Excellent long-term H₂/He selectivity stability was achieved over a total testing period of ~3550 hours (>147 days).
- High pressure flux measurements of the membrane 029 (7.6 μm thick pure-Pd/Inconel) at ~400 & 450°C and at a ΔP of ~100 psi ($P_{\text{High}}=115$ psia & $P_{\text{Low}}=15$ psia), led to a H₂ flux of ~150 & 166 scfh/ft², respectively, with essentially infinite ideal H₂/He selectivity.

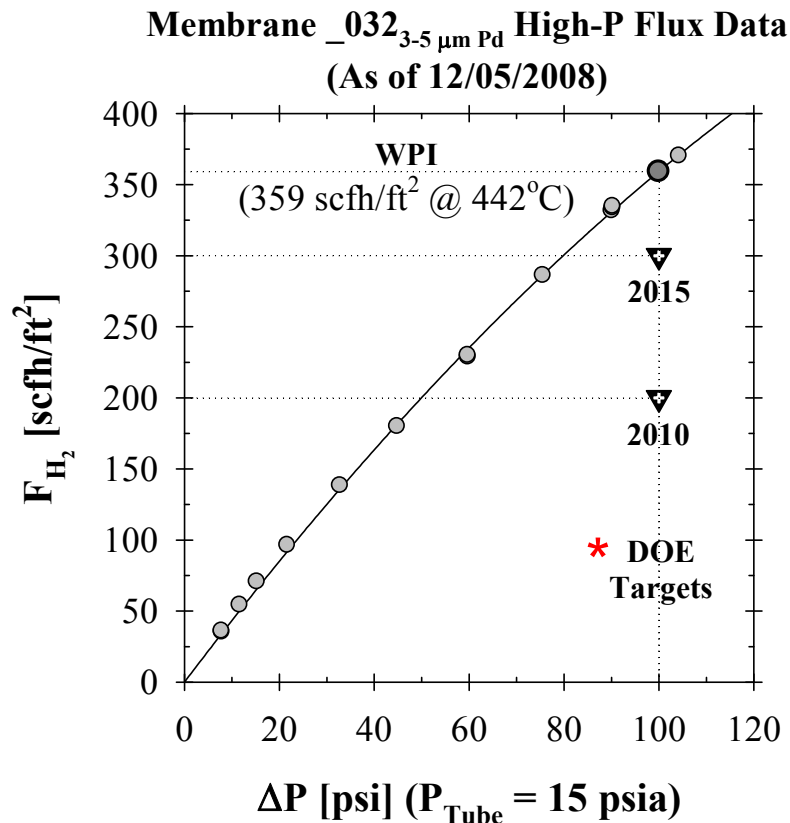
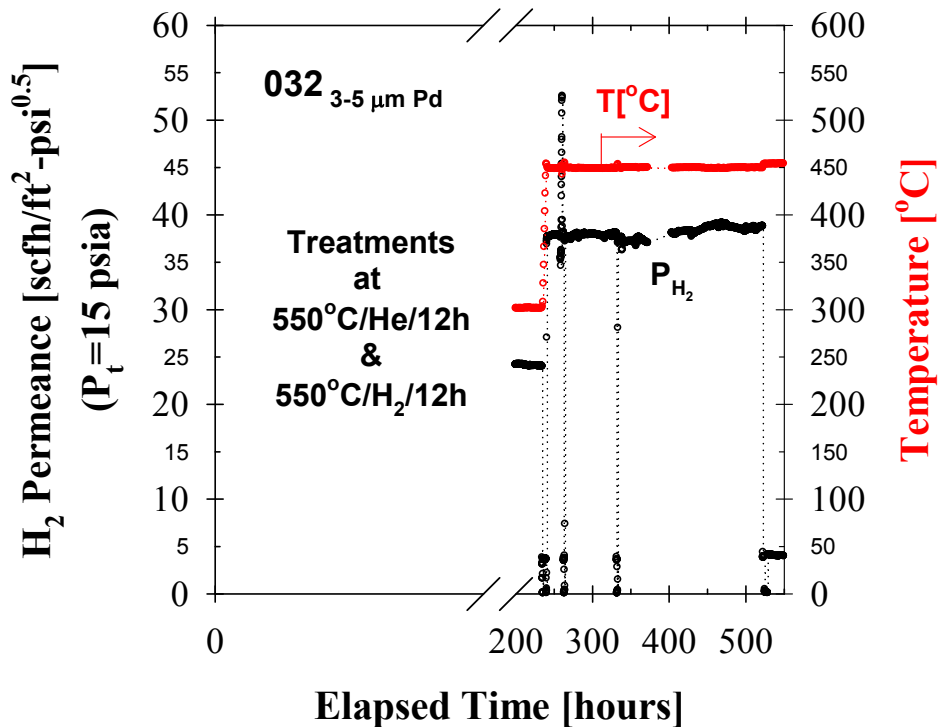
Reproducibility of the Long-Term Selectivity Stability



- The excellent H₂/He selectivity stability of the membrane 029 over the temperature range of 300-450°C, was successfully re-produced with the membrane 031 (7 μm thick pure-Pd/Inconel).
- At ~450°C and at a ΔP of 15 psi (P_{High}=30 psia & P_{Low}=15 psia), the H₂ flux and the final H₂/He selectivity were ~26.6 scfh/ft² & ~4500, respectively, after a total testing period of ~2200 hours (>90 days).

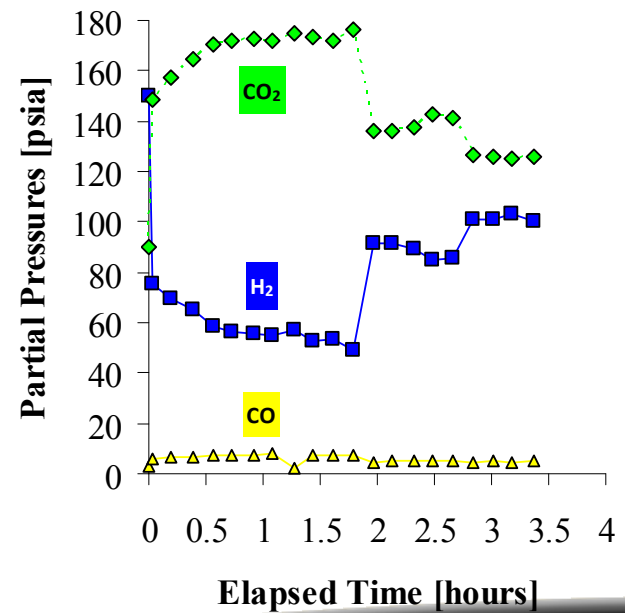
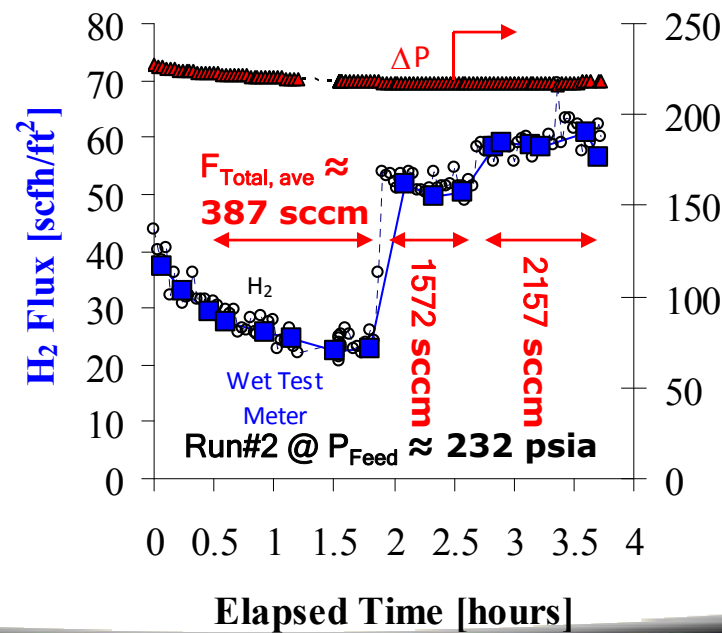
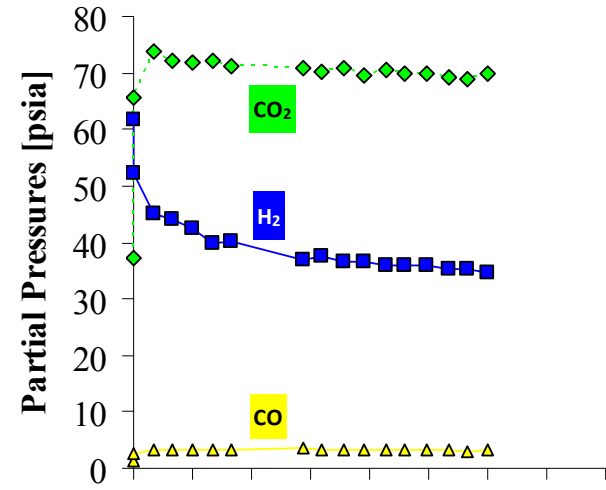
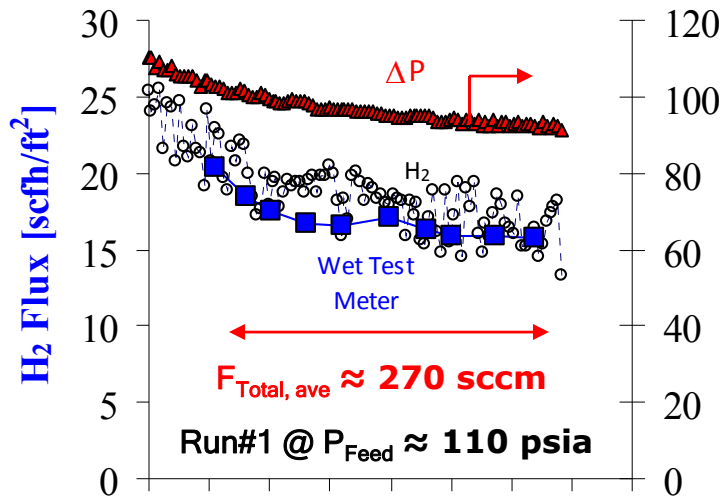
* At ~500 hours (450 °C) the sudden change in the leak profile was due to a defect formed and/or present during the synthesis, which was not cured completely and did not contribute to any further leak growth.

Progress Towards DOE H₂ Flux Targets



➤ At 442°C & at a ΔP of 100 psi (P_{High}=115 psia & P_{Low}=15 psia), the H₂ flux of the 3-5 μm thick Pd/Inconel membrane 032 was as high as ~359 scfh/ft² at the end of ~285 hours of testing with H₂/He selectivity of ~450, which exceeded the DOE's 2010 and 2015 H₂ flux targets.

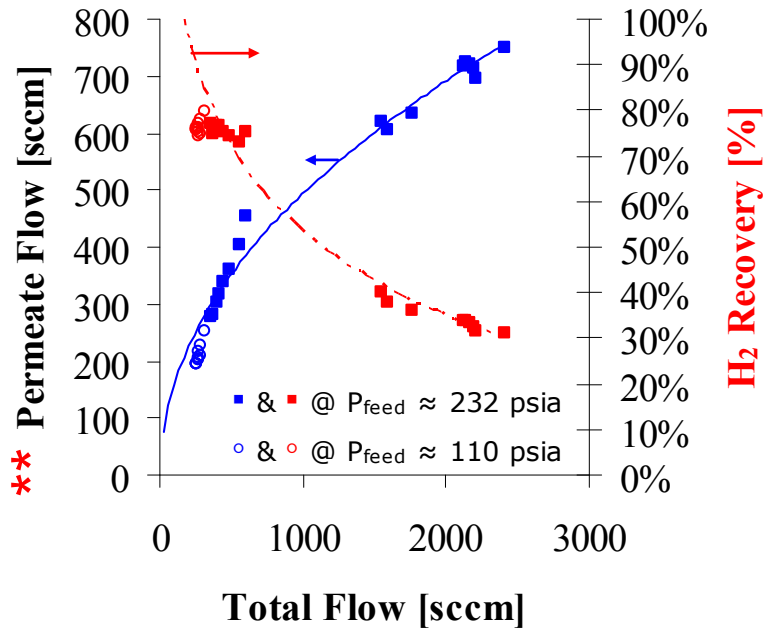
Mixed Gas Testing* of Membrane 029_{7.6 μm Pd}



* 61.7% H₂, 37.1% CO₂ & 1.2% CO

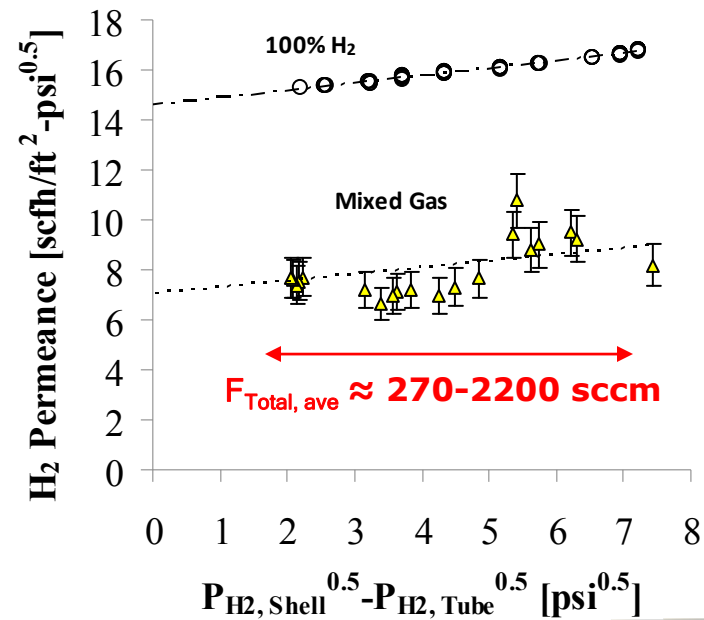
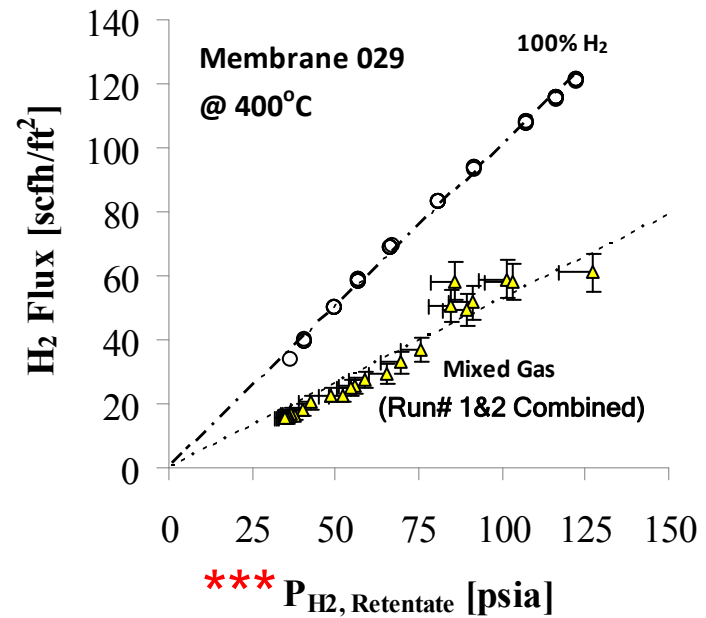


Mixed Gas Testing* of Membrane 029_{7.6 μm Pd}



➤ Compared to the pure H₂ flux, the lowering of the H₂ flux for the mixed gas testing was primarily due to the changes in the H₂ partial pressure along the length of the reactor caused by the removal of H₂ at a high permeation rate.

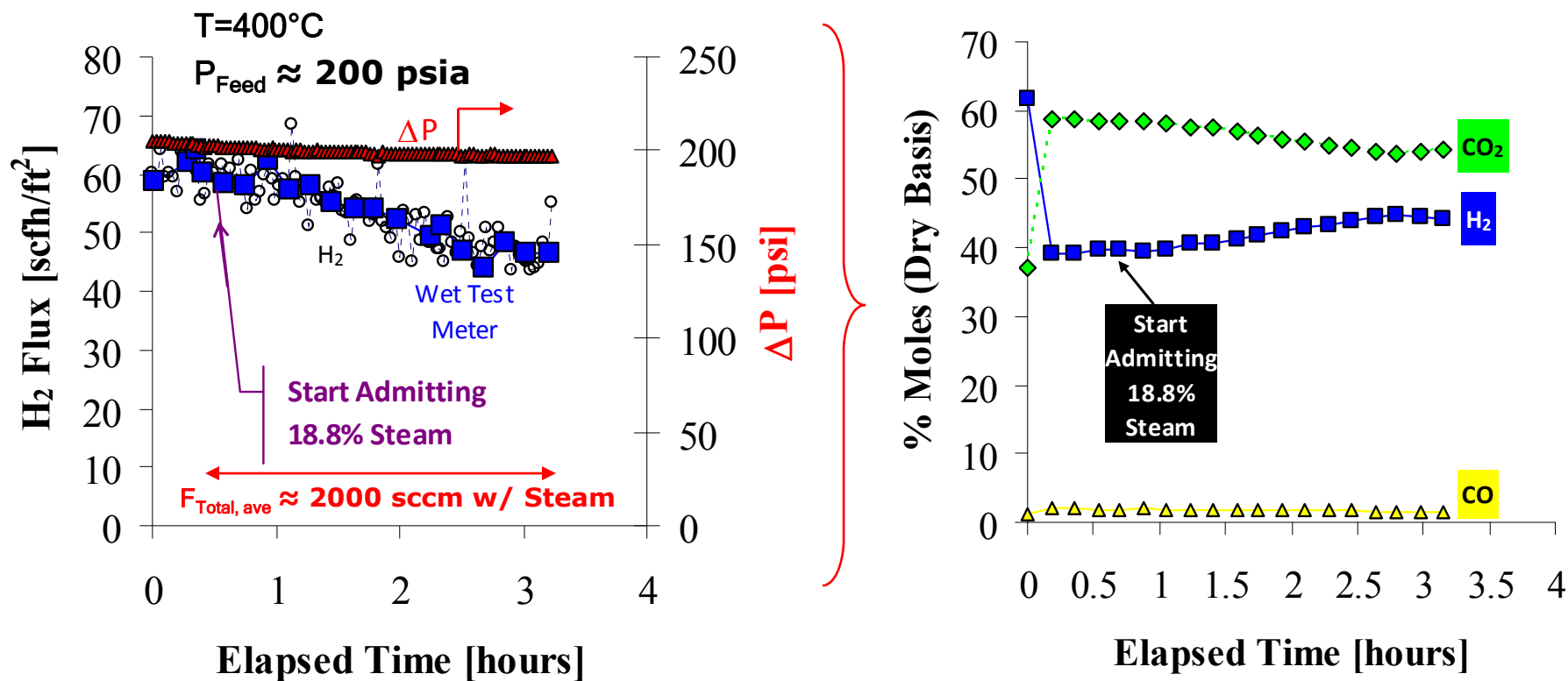
- * 61.7% H₂, 37.1% CO₂ & 1.2% CO
- ** H₂ only, no other gases detected in the permeate



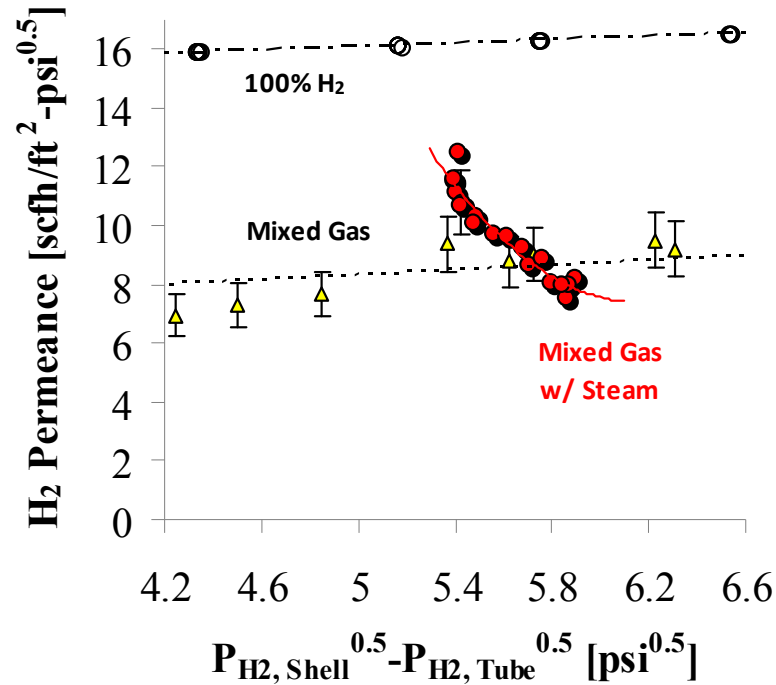
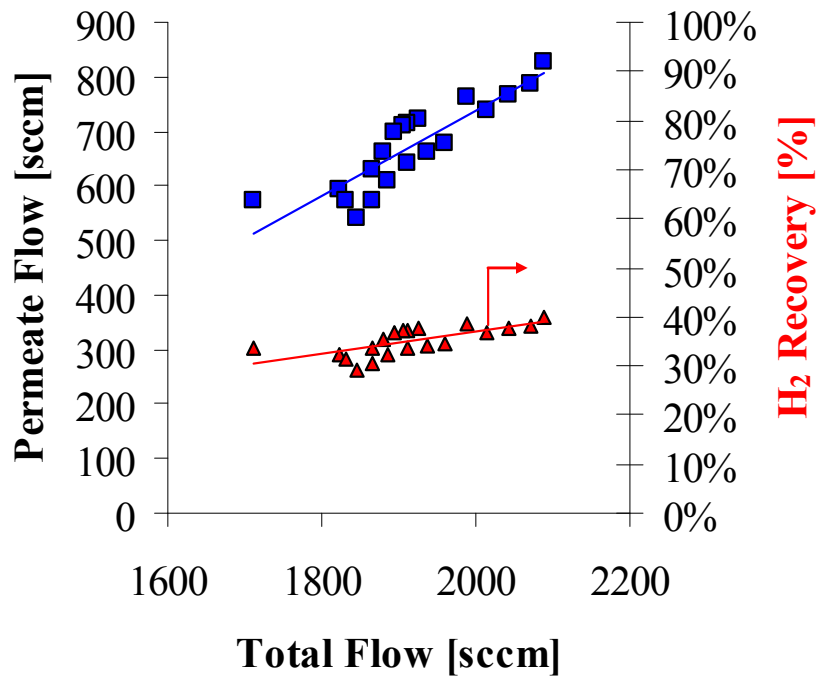
*** H₂ partial pressure at the retentate exit is based on the GC analysis



Mixed Gas Testing** of Membrane 029_{7.6 μm Pd} with Steam



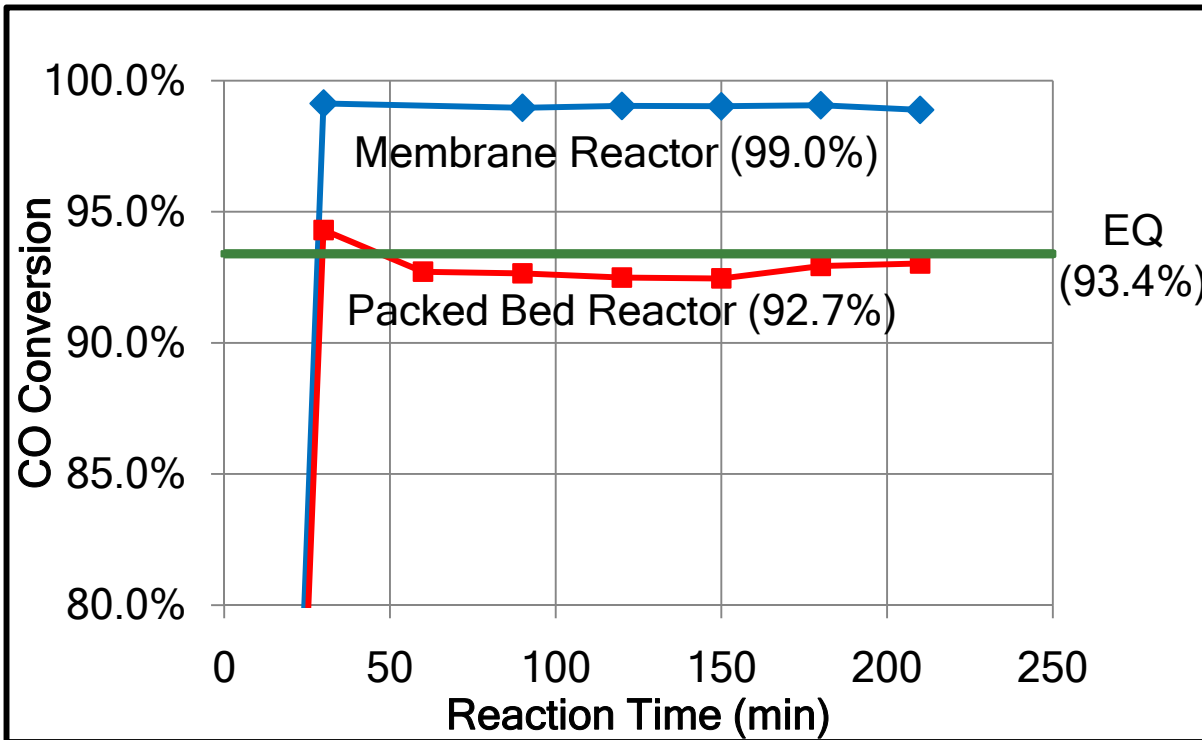
Mixed Gas Testing** of Membrane 029_{7.6 μm Pd} with Steam



Factors affecting hydrogen flux under mixed-gas testing conditions:

- Dilution of H₂ concentration on the feed side due to the presence of other gases
- The change of H₂ partial pressure due to the in-situ removal of H₂ along the length of the membrane module
- Gas phase mass transfer limitations due to the formation of a concentration boundary layer (Concentration polarization)
- Competitive adsorption of other gas components on the membrane surface

WGS Reaction in a Pd-based* CMR



➤ CO conversion vs. time is shown for both a membrane reactor (red) (*Membrane 0.1-AA-2: 12.5 m Pd) and a packed bed reactor (blue) fed with the conditions listed in the table

➤ Estimated equilibrium conversion for the conditions listed is shown in green

➤ The feed consisted of CO and H₂O

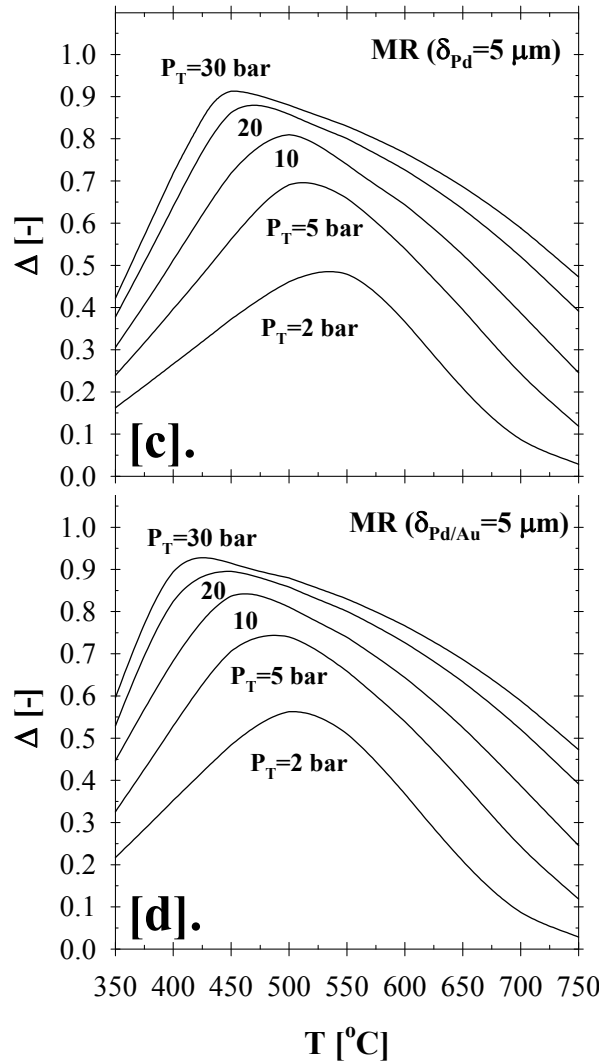
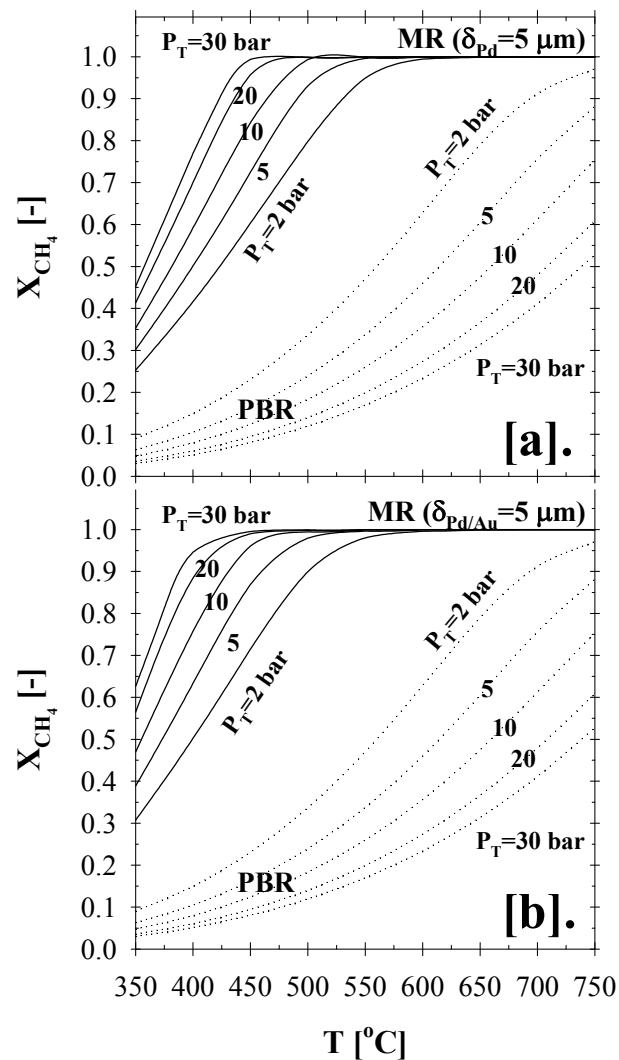
➤ The membrane reactor had a tube-side pressure of 14.5 psia, H₂ recovery was 89.9%

➤ The packed bed reactor contained a stainless steel tube with the same dimensions as the membrane

| | Packed Bed Reactor | Membrane Reactor |
|---|--------------------|------------------|
| T (°C) | 346 | 349 |
| H ₂ O/CO | 1.55 | 1.44 |
| P (psig) | 200 | 200 |
| GHSV** _{STP} (hr ⁻¹) | 151 | 149 |

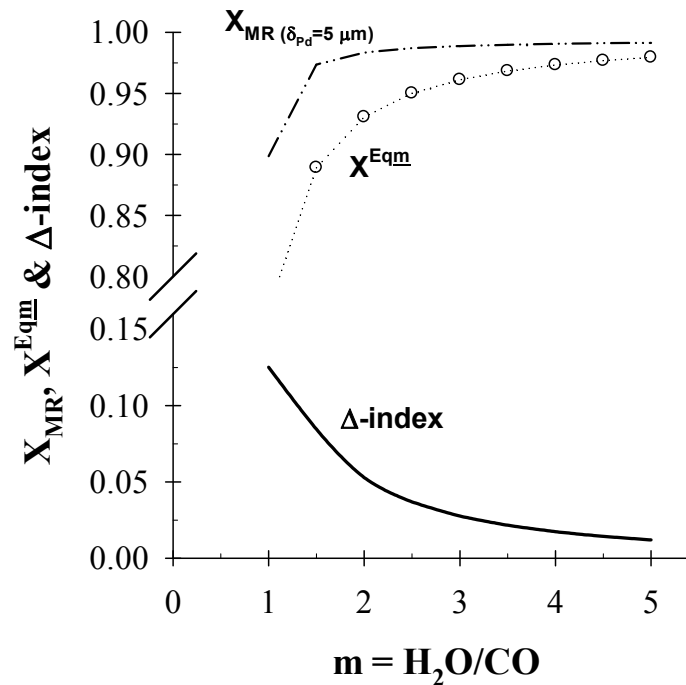
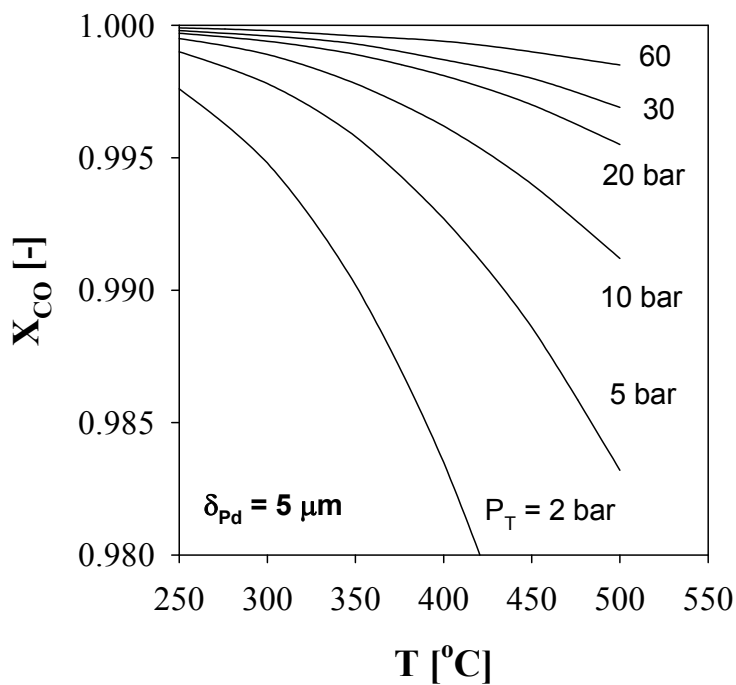
** GHSV=Total Feed Flowrate/Volume of the Reactor

CMR Modeling of the MSR* Reaction w/ Process Intensification Analysis



- The superior performance of the CMRs over that of conventional PBRs was amply demonstrated over a wide range of operating conditions.
- Impact of operating conditions on the CMR performance was successfully simulated & targeting analysis was utilized to optimize and evaluate the best performance range via the proposed process intensification indicator Δ -index. ($\Delta = X_{CH_4,MR} - X_{CH_4,PBR}$)

CMR Modeling of the WGS* Reaction w/ Process Intensification Analysis



- At 400°C and 60 bar the total CO conversion, X_{CO} , simulated for the CMR and the PBR were 99.9 and 88.9%, respectively. As the driving force for the H_2 permeation increased with the higher pressure on the reaction side, the in-situ removal of the high partial pressure H_2 resulted in an enhancement of the X_{CO} in the case of Pd-based CMR over the entire temperature range.
- In contrast to conventional reactors operated under excess steam-to-CO ratios, the Δ -index analysis showed that the CMR operation below $m < 2$, can further improve the CO conversion of the WGS reaction by $\sim 13\%$, provided that the coke formation was avoided by utilizing a highly active & selective catalyst for WGS reaction.

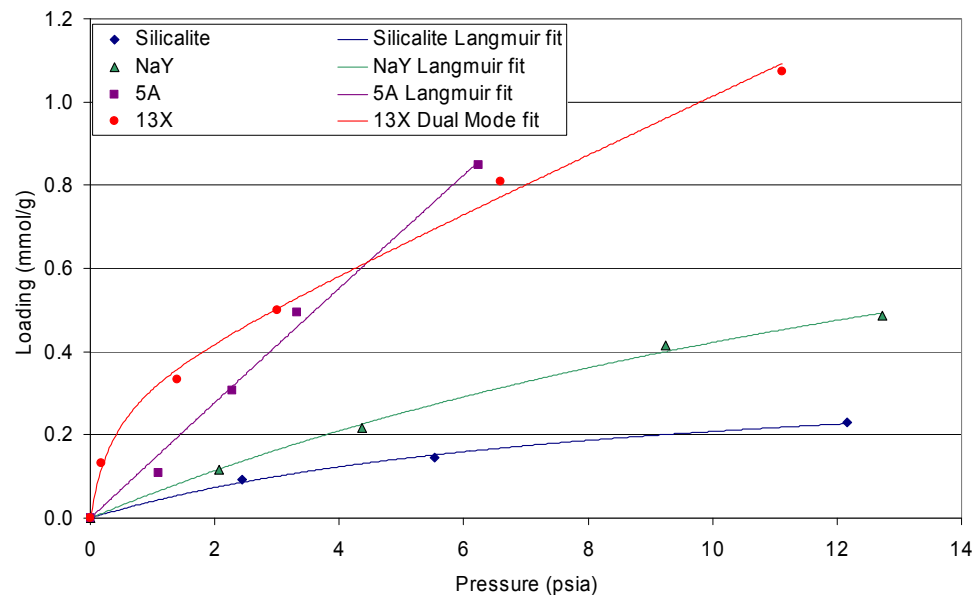
Collaborations

Adsorption Research Inc. (ARI); sub

(Through telephone conversations and quarterly report to the prime)

- ARI completed adsorption selection & property measurement for Zeolite 5A, Zeolite 13X, NaY and Hisiv3000
- The equilibrium isotherms of the adsorbents 5A, 13X, NaY and Hisiv3000 were measured at 200 and 230°C for CO₂, COS and H₂S and the equilibrium data were fitted using the Langmuir equation. The eq^m isotherms at 200 and 230°C were also measured for the water vapor.
- To evaluate both short-time and long-time diffusion behavior of the adsorbents 5A, 13X, NaY and Hisiv 3000, transient uptake tests for CO₂, COS and H₂S were conducted at 200 & 230°C.

Adsorption Results @ 200°C H₂S Isotherms



- The development of the pressure swing adsorption (PSA) system and the demonstration of a suitable adsorbent in cyclic operation at 200°C & 200 psia is underway.

Proposed Future Work (FY09 & FY10)

- Continue WGS reaction and mixed gas testing studies
- Complete 2010 technical target screening and qualification tests* phase 1 and phase 2
- Synthesis of thin separation layers to achieve higher H₂ flux using support with minimum mass transfer resistance
- Continue Pd/Au alloying studies to improve H₂ flux
- Conduct long-term sulfur poisoning & recovery experiments
- Further refinement & improvement of the CMR model (i.e., 2-D non-isothermal finite element modeling via the Comsol Multiphysics)
- Continue process intensification & performance assessment analyses coupled with process control strategies
- Initiate economical analysis for the proposed process intensification framework
- Complete building & testing of a Pressure Swing Adsorption (PSA) system (sub: ARI)

Project Summary

- Achieved excellent long-term H₂/He selectivity stability of essentially infinite over a total testing period of ~3550 hours (>147 days) at 300-450°C & at a ΔP of 15-100 psi (P_{Low}=15 psia), with membrane 029_{7.6 μm Pd/Inconel}
- Achieved re-producible long-term H₂/He selectivity stability (~2200 hours, >90 days) with membrane 031_{7 μm Pd/Inconel} at T = 300-450°C.
- Flux of ~359 scfh/ft², which exceeded the DOE's 2010 and 2015 H₂ flux targets [Membrane 032_{3-5 μm Pd/Inconel} @ T=442°C & ΔP of 100 psi (with P_{Low}=15 psia)].
- Initiated mixed gas experiments (61.7% H₂, 37.1% CO₂ & 1.2% CO w/ or w/o 19% Steam) using membrane 029_{7.6 μm Pd} at 400°C & ΔP=100-200 psi (with P_{Low}=15 psia).
- Achieved 99% total CO conversion and 89.9% H₂ recovery in a 12.5 μm thick Pd-based CMR operated at ~350°C, ΔP=200 psi (P_{Low}=15 psia) H₂O/CO=1.44 and GHSV_{stp}=150 h⁻¹. Under similar conditions, X_{CO,PBR} & X_{CO,Eqm} were 92.7% & 93.4%, respectively.
- Successfully completed MSR & WGS reaction modeling studies and initiated process intensification analysis.
- Completed property & isotherm measurements for the selected adsorbents and initiated PSA system construction.

Project Summary Table

| | DOE Targets§ | | Current WPI Membranes | | | | |
|---|--------------|----------|-----------------------|----------------------------|------------|------------|------------|
| | 2010 | 2015 | #025R | #027 | #029 | #031 | #032 |
| Flux [scfh/ft ²] | 200 | 300 | 65.9 | 36.1 | 166 | 26.6 | 359 |
| ΔP (psi) H ₂ partial pressure (P _{Low} =15 psia) | 100* | 100* | 15 | 15 | 100 | 15 | 100 |
| Temperature [°C] | 300-600 | 250-500 | 400 | 400 | 450 | 450 | 442 |
| H ₂ /He Selectivity | n/a | n/a | ~220 | ~120 | ∞ | ~4500 | ~450 |
| Total Test Duration [hours] | n/a | n/a | 1015 | ~1250 | ~4500 | ~2200 | ~523 |
| Thickness [μ m] | n/a | n/a | 4.2 Pd | 6.2 Pd/Au _{5 wt%} | 7.6 Pd | 7.0 Pd | 3-5 Pd |
| WGS Activity | Yes | Yes | Not tested | Not tested | Not tested | Not tested | Not tested |
| CO Tolerance | Yes | Yes | Not tested | Not tested | Yes | Not tested | Not tested |
| S Tolerance [ppm] | 20 | >100 | Not tested | Not tested | Not tested | Not tested | Not tested |
| H ₂ Purity | 99.5% | 99.99% | 99.0% | 99.5% | ≥99.999% | 99.98% | 99.8% |
| ΔP Operating Capability (Max. System Pressure, psi) | 400 | 800-1000 | 15** | 15** | 225** | 15** | 100** |

§ DOE-NETL Test Protocol v7 - 05/10/2008

* Standard conditions are 150 psia hydrogen feed pressure and 50 psia hydrogen sweep pressure;

** Maximum pressure tested, however, the ΔP can be higher since previous WPI membranes were tested up to 600 psi under MSR reaction conditions