

Direct Hydrogen PEMFC Manufacturing Cost Estimation for Automotive Applications

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Overview

The 2009 & 2010 PEMFC cost analyses are based on updates to the bottom-up high-volume stack and BOP cost models developed in 2008.

Timeline

- Base Period: Feb 2006-May 2008
 » 100% complete
- Option Yr 1 & 2: May 2008-Feb 2010
 - » 100% complete
- Option Yr 3: Feb 2010-Feb 2011
 - » 15% complete

| Barriers | | | | | | | |
|--|--------------------------|---|---|--|--|--|--|
| Barriers addressed | | | | | | | |
| » B. Cost | Cost Targets (\$/kW) | | | | | | |
| 2009 2010 2015 | | | | | | | |
| Fuel Cell System | uel Cell System 60 45 30 | | | | | | |
| Fuel Cell Stack 25 15 | | | | | | | |
| * Manufactured at volume of 500 | 000 per vea | r | - | | | | |

Partners

- Project lead: TIAX
- Collaborate with ANL on system configuration and modeling
- Yong Yang¹ : mfg. cost modeling
- Feedback from Fuel Cell Tech Team, Developers, Vendors

Budget

- Total project funding
 - » Base Period = \$415K
 - » No cost share
- ♦ FY08 = \$50K
- ♦ FY09 = \$51K
- ♦ FY10 = \$92K



Objectives

| | Objectives |
|---------|--|
| Overall | Bottom-up manufacturing cost assessment of 80 kW direct-H₂ PEMFC system for automotive applications |
| 2009 | High-volume (500,000 units/year) cost projection of ANL 2009 PEMFC system configuration assuming an NSTFC-based MEA and a 20 μm PFSA membrane >Bottom-up manufacturing cost analysis of <i>both</i> stack and BOP >Sensitivity analyses on stack and system parameters Independent peer review of cost analysis methodology and results Comprehensive report on the 2008 PEMFC cost analysis (high-volume, bottom-up stack and BOP cost) |
| 2010 | Preliminary high-volume (500,000 units/year) cost projection of ANL 2010 PEMFC system configuration assuming an NSTFC-based MEA and a 20 µm reinforced PFSA membrane Metal bipolar plates Stack conditioning |



BOP = Balance-of-Plant NSTFC = Nano-Structured Thin Film Catalyst PFSA = Perfluorosulfonic acid

Background

Over the past year, we updated the PEMFC cost assessment based on input from ANL on the 2009 stack performance parameters.

- In 2009, we updated the system configuration, stack performance assumptions and stack and BOP component specifications based on ANL modeling results
 - Based cost assessment on ANL 2009 PEMFC system configuration assuming an NSTFC MEA and a 20 μm PFSA membrane
 - Updated bottom-up cost assessment of stack, balance of stack and stack assembly
 - Replaced EWH by planar MH for cathode air and anode fuel humidification
 - Costed HT & LT radiators, fans, coolant pumps; air precooler; flow orifice for CEM
 - Participated in independent peer-review of our cost analysis methodology and results
 - Submitted a comprehensive report to DOE on our 2008 PEMFC cost analysis
- In 2010, we are working on changes based on ANL 2010 PEMFC system:
 - NSTFC MEA with 20 μm reinforced PFSA membrane
 - Metal bipolar plates thermal nitrided, Au-Nanoclad
 - Non-woven carbon paper GDL
 - Eliminate anode fuel humidifier, pleated planar MH for cathode air humidification
 - Other BOP updates pending ANL input
 - Stack conditioning pending funding authorization from DOE



MEA = Membrane Electrode Assembly EWH = Enthalpy Wheel Humidifier PFSA = Perfluorosulfonic acid NSTFC = Nano-Structured Thin Film Catalyst MH = Membrane Humidifier

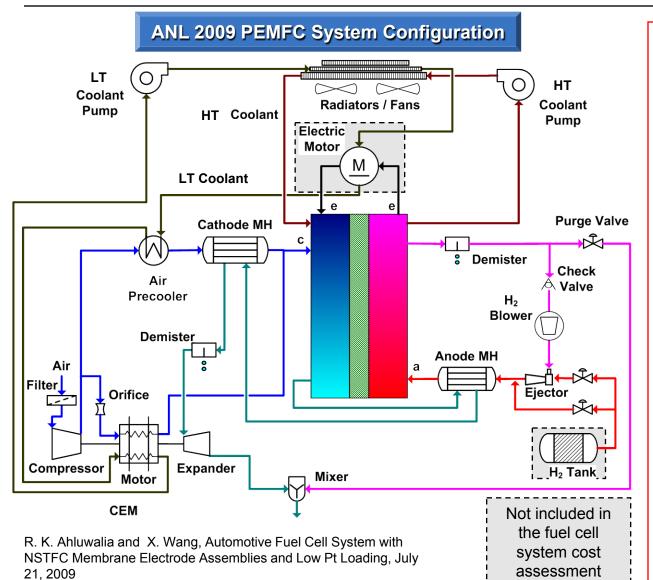
We used a bottom-up approach to determine high-volume (500,000 units/year) manufacturing cost for the major stack and BOP components.

| Stack Components | BOP Components |
|--|---|
| Catalyst Coated Membrane Electrodes Gas Diffusion Layer (GDL) Membrane Electrode Assembly (MEA) Bipolar Plates Seals | Radiators (HT, LT) Cathode Planar Membrane Humidifier (MH) Anode Planar MH Compressor-Expander-Module (CEM) H₂ Blower |
| » Develop production process flow chart for key subsystems and components » Obtain raw material prices from potential suppliers » Estimate manufacturing costs using TIAX cost models (capital equipment, raw material costs, labor rates) | Develop Bill of Materials (BOM) Obtain raw material prices from potential suppliers Develop production process flow chart for key subsystems and components Estimate manufacturing costs using TIAX cost models and Boothroyd Dewhurst Design for Manufacturing & Assembly (DFMA[®]) software |

- We used literature/experience-based estimates for stack components such as sensors, controls, control board and wire harness. We scaled quotes/catalog-based estimates for BOP components such as air precooler, flow orifice, coolant pumps, radiator fans, H₂ ejectors, valves/regulators and piping/fittings.
- We used the TIAX technology-based bottom-up cost model for the HT/LT radiators, and cathode/anode planar MH, while we used the DFMA[®] bottom-up manufacturing cost model for the CEM and H₂ blower.



Approach 2009 System Configuration



Key features

Stack

- 3M NSTFC MEA
- + 20 μm unsupported membrane
- 0.05 (a)/0.1 (c) mg/cm² Pt
- 90 °C, 2.5 atm
- Graphite bipolar plates
- Woven carbon fiber GDL

Air Management

- CEM module
- · Air-cooled motor/Air-foil bearing

• Efficiencies at rated power: 70% compressor, 73% expander, 86% motor, 87% controller

Water Management

- Cathode MH with precooler
- Anode MH w/o precooler

Thermal Management

- Advanced 24-fpi louver fins
- 55% pump + 92% motor efficiency
- 45% blower + 92% motor efficiency

Fuel Management

- Parallel ejector-pump hybrid
- 35% pump efficiency

MEA = Membrane Electrode Assembly ANL = Argonne National Laboratory



The high-volume manufactured cost of the 2009 PEMFC stack for six scenarios^{1, 2} is estimated to range between \$19/kW and \$40/kW.

| Key Cost Assumptions | | 2009 Stack Scenarios ^{1, 2} | | | | | |
|--|-----------------------|--------------------------------------|------------|------------|------------|-----------|-------|
| Key Cost Assumption | S1 | S2 | S 3 | S 4 | S 5 | S6 | |
| System net power | kW _e | | | 80 |) | | |
| Stack gross power ² | kW _e | 91.5 | 92.1 | 92.3 | 91.6 | 91.8 | 92.1 |
| Cell voltage (rated power) ² | V | 0.729 | 0.690 | 0.659 | 0.736 | 0.693 | 0.661 |
| Stack gross power density ² | mW/cm ² | 479 | 658 | 789 | 451 | 701 | 886 |
| Pt loading (total) ² | mg/cm ² | | 0.25 | | 0.15 | | |
| Stack Pt content | g/kW _{gross} | 0.52 | 0.38 | 0.32 | 0.33 | 0.21 | 0.17 |
| System Pt content | g/kW _{net} | 0.60 | 0.44 | 0.37 | 0.38 | 0.25 | 0.20 |
| Stack efficiency (rated power) ² | % LHV | 57.4 | 54.5 | 52.1 | 57.4 | 54.6 | 52.1 |
| System efficiency (rated power) ² | % LHV | 50.0 | 47.3 | 45.0 | 50.0 | 47.3 | 45.0 |
| System voltage (rated power) | V | 300 | | | | | |
| System active area | m² | 19.1 | 14.0 | 11.7 | 20.3 | 13.1 | 10.4 |
| Stack cost ³ | \$/kW _{net} | 40.2 | 30.0 | 25.9 | 33.2 | 22.3 | 18.7 |

¹ All scenarios assume a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, 20 µm PFSA membrane, and stack operating conditions of 90 °C and 2.5 atm.

² Based on stack and system modeling results by ANL for 2009 PEMFC system: R. K. Ahluwalia and X. Wang, March 6-July 21, 2009.

³ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).



We developed stack specifications for the 2009 baseline scenario S5, consistent with the performance predicted by ANL's stack and system modeling.

| TIAX Assumptions | Units | 2005 ¹ | 2007 ^{2,3} | 2008 ⁴ | 2009 ⁵ |
|------------------------------|--------------------------|-------------------|----------------------------|--------------------------|-------------------|
| Number of stacks per system | # | 2 | 2 | 2 | 2 |
| Number of cells per stack | # | 231 | 221 | 219 | 217 |
| Active area to Total area | % | 85 | 85 | 85 | 85 |
| Active area per cell | cm ² | 323 | 260 | 277 | 304 |
| Cell pitch | cells/inch (cells/cm) | 9.55 (3.76) | 9.75 (3.84) | 9.75 (3.84) | 10.57 (4.16) |
| System voltage (rated power) | V | 300 | 300 | 300 | 300 |

¹ E.J. Carlson et al., Cost Analysis of PEM Fuel Cell Systems for Transportation, NREL/SR-560-39104, Sep 30, 2005

² R.K. Ahluwalia and X. Wang, Reference Fuel Cell System Configurations for 2007: Interim Results, ANL, Feb. 6, 2007

³ R.K. Ahluwalia, X. Wang and R. Kumar, Fuel Cell Systems Analysis, DOE Hydrogen Program Review, May 15-18, 2007

⁴ R. K. Ahluwalia, X. Wang and R. Kumar, Fuel Cell Systems Analysis, 2008 USDOE Hydrogen Program Review, Arlington, VA, June 9-13, 2008

⁵ R. K. Ahluwalia and X. Wang, Automotive Fuel Cell System with NSTFC Membrane Electrode Assemblies and Low Pt Loading, July 21, 2009



Using S5 as the 2009 baseline scenario, we estimated that the MEA and seal together cost ~\$101/m², of which material costs represent ~81%.

| Manufactured Cost ¹ | MEA (\$/m²) | Frame Seal (\$/m²) | | |
|--|--------------------------------------|--------------------|--|--|
| Material - Membrane - Electrode - GDL | 76.70 - 9.77 - 58.69 - 8.23 | 4.78 | | |
| Capital Cost | 6.18 | 1.14 | | |
| Labor | 3.85 | 0.81 | | |
| Tooling & Equipment | 4.21 | 0.95 | | |
| Other ² | 2.03 | 0.45 | | |
| Subtotal | 92.97 | 8.13 | | |
| Total | 101.11 | | | |

¹ Manufactured cost on an active area basis

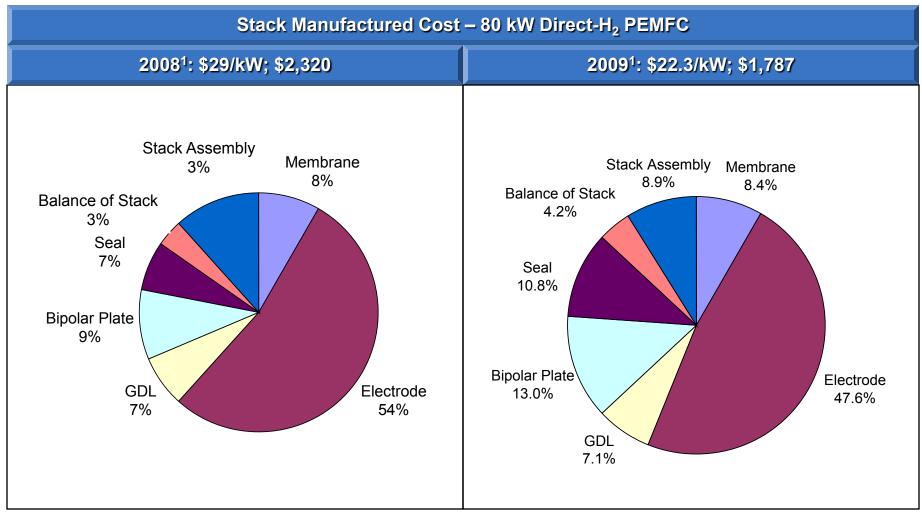
² Other costs include utilities, maintenance, and building



In 2008, the MEA and seal cost was \$140/m² due to higher material costs for the membrane (30 μ m), electrodes (Pt loading = 0.25 mg/cm²) and GDL (275 μ m).



The electrodes represent approximately 48% of the ~\$22/kW fuel cell stack manufactured cost in 2009.

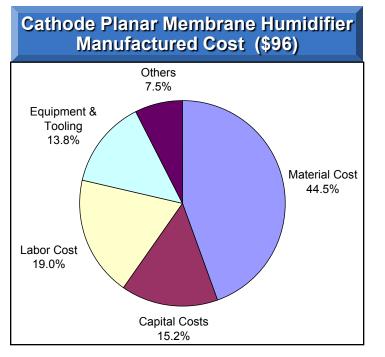


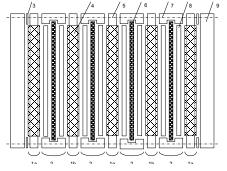
¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).



Progress 2009 PEMFC System Cathode Planar MH Cost

We developed bottom-up manufacturing costs for the cathode and anode planar MH based on ANL specifications¹ and other patents².





| Cathode Planar Membrane Humidifier Manufactured Cost (\$) | | | | | | | |
|---|----|----------|---------|--|--|--|--|
| Process | # | Material | Process | | | | |
| Die Cut GDL | 1 | 2.49 | 2.02 | | | | |
| Die Cut Membrane | 2 | 7.03 | 2.14 | | | | |
| Hot Press Lamination | 3 | 0.01 | 6.06 | | | | |
| Injection Molding Frame Seal | 4 | 0.00 | 4.20 | | | | |
| Laser Cut Nickel Foam | 5 | 15.44 | 17.16 | | | | |
| Injection Molding Foam Frame | 6 | 4.39 | 4.34 | | | | |
| Injection Molding End Plate Gasket | 7 | 0.11 | 0.45 | | | | |
| Die Casting End Plate | 8 | 9.50 | 1.32 | | | | |
| Component Assembly | 9 | 0.00 | 6.90 | | | | |
| QC & Testing | 10 | 0.00 | 6.80 | | | | |
| Packaging | 11 | 0.00 | 2.03 | | | | |
| Fastener Cost | - | 3.91 | 0.00 | | | | |
| Total | - | 96 | | | | | |

¹ R. K. Ahluwalia and X. Wang, Automotive Fuel Cell System with NSTFC Membrane Electrode Assemblies and Low Pt Loading, July 21, 2009 ² U.S. Patents 6,737,183; 6,835,477; 6,864,005; 7,078,117



MH = Membrane Humidifier

The water management system OEM cost^{1,2} is projected to be \$170.

| Water Management System Cost (\$) | | | | | | | |
|------------------------------------|---------------------------|-------------------------|-------------------|--|--|--|--|
| Component | Factory Cost ¹ | OEM Cost ^{1,2} | Comments | | | | |
| Cathode Planar Membrane Humidifier | 96 | 111 | Bottom-up costing | | | | |
| Anode Planar Membrane Humidifier | 52 | 59 | Bottom-up costing | | | | |
| Total | 148 | 170 | | | | | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Assumes 15% markup to the automotive OEM for BOP components

The cathode and anode planar membrane humidifier costs are both estimated using bottom-up costing tools.



The thermal management system OEM cost^{1,2} is projected to be \$413.

| Thermal Management System Cost (\$) | | | | | | |
|-------------------------------------|---------------------------|-------------------------|---|--|--|--|
| Component | Factory Cost ¹ | OEM Cost ^{1,2} | Comments | | | |
| HT Radiator | 83 | 95 | Bottom-up costing | | | |
| LT Radiator | 12.6 | 14.5 | Bottom-up factory cost = \$56; Scaling by LTR heat duty, 2.9/12.9*56=\$12.6 | | | |
| Air Precooler | - | 43.2 | Bell Intercooler \$108/unit Assuming 60% discount | | | |
| HT/LT Radiator Fan | - | 75 | McMaster-Carr 5990K48, Base-mount single- | | | |
| - Motor | - | - 60 | phase AC motor, 0.75 HP, 3450 rpm, \$152/unit Assuming 60% discount, motor costs \$60/unit | | | |
| - Fan | - | - 15 | Aluminum fan costs ~\$15/unit | | | |
| HT Coolant Pump | - | 150 | McMaster-Carr 5990K53, Base-mount single- | | | |
| - Motor | - | - 95 | phase AC motor, 1.5 HP, 3450 rpm, \$238/unit Assuming 60% discount, motor costs \$95/unit | | | |
| - Pump | - | - 55 | Aluminum pump costs ~\$55/unit | | | |
| LT/Air Precooler Coolant Pump | - | 30 | AWECO pump, high-volume quote | | | |
| Other | - | 5 | Two temperature sensors | | | |
| Total | 399 | 413 | | | | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Assumes 15% markup to the automotive OEM for BOP components

The air precooler, radiator fan, coolant pumps, and their motors are assumed to be purchased components; hence their price includes a markup.



The fuel management system OEM cost^{1,2} is projected to be \$425.

| | Fuel Management System Cost (\$) | | | | | | |
|-------------------------|----------------------------------|----------------------------|--|--|--|--|--|
| Component | Factory Cost ¹ | OEM Cost ^{1,2} | Comments | | | | |
| H ₂ Blower | 219.5 | 252 | Bottom-up costing using DFMA® | | | | |
| H ₂ Ejectors | - | 40 | 2 ejectors assumed @ \$20/unit | | | | |
| H ₂ Demister | - | 61 | Parker Hannifin MN1S-6CN, 28 SCFM, ∆P=1.25 psid, rated for H ₂ to 175 F, \$152.50/unit Assuming 60% discount, H ₂ demister costs ~\$61/unit (Note: Parker Hannifin MN4S-6CN, rated for H ₂ to 200+ F, ∆P=0.35 psid, \$600/unit) | | | | |
| Solenoid Valves | - | 46 | 2 solenoid flow control valves w/ built-in ports, McMaster-Carr 61245K1, \$57.96/unit, Assuming 60% discount, solenoid valves cost ~\$23/unit | | | | |
| Purge Valve | 13 | 15 | DFMA [®] bottom-up costing; DOE Chemical Hydride Storage presentation, Sept. 2005 | | | | |
| Check valve | 9 | 10 | DFMA® bottom-up costing; DOE Chemical Hydride Storage presentation, Sept. 2005 | | | | |
| Total | 389 | 425 | | | | | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Assumes 15% markup to the automotive OEM for BOP components

The H₂ ejectors, H₂ demister, and solenoid valves are assumed to be purchased components; hence their price includes a markup.



The air management system OEM cost^{1,2} is projected to be \$982.

| | Air Management System Cost (\$) | | | | |
|---|---------------------------------|----------------------------|--|--|--|
| Component | Factory Cost ¹ | OEM Cost ^{1,2} | Comments | | |
| CEM (Compressor, Expander, Motor, Motor Controller | 687 | 790 | Bottom-up costing using DFMA [®] ; motor controller input power updated to 9.3 kWe | | |
| | | | Parker Hannifin HN4S-10CG, 226 SCFM, ∆P=2 psid, 1-¼ " NPT, 95% coalescing efficiency, \$390.60/unit, Assuming 60% discount, demister costs ~\$156/unit | | |
| Air demister | - | 156 | (Note: Parker Hannifin HN4L-8CG, 98.5% coalescing eff., ΔP =2 psid, \$534/unit; Parker Hannifin HN5S-7CVPG, 99.5% coalescing eff., ΔP =0.5 psid, \$680/unit; Parker Hannifin HN6S-7CVPG, 99.5% coalescing eff., ΔP =0.35 psid, \$805/unit; Parker Hannifin HN8S-MEG, 99.95% coalescing eff., ΔP =0.35 psid, \$1,235/unit; Parker Hannifin FF4-1201-6QU, 99.97% coalescing eff., ΔP =0.35 psid, \$3,689/unit) | | |
| Air/H ₂ mixer | - | 27 | Gas mixer, McMaster-Carr 3322K18, 1" pipe, \$68.42, Assuming 60% discount, air/H ₂ mixer costs ~\$27/unit | | |
| Flow orifice | - | 5 | Acetal instant tube-fitting orifice, McMaster-Carr 6349T17, ½" tube, \$11.29, Assuming 60% discount, flow orifice costs ~\$4.5/unit | | |
| Air filter | - | 4 | | | |
| Total | 879 | 982 | | | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Assumes 15% markup to the automotive OEM for BOP components

The air demister, air/H₂ mixer, flow orifice, and air filter are assumed to be purchased components; hence their price includes a markup.



The high-volume OEM cost^{1,2} for the 2009 BOP subsystems is projected to be \$1,991.

| BOP Subsystem | Component | Technology / Cost Basis | Factory Cost ¹ , \$ | OEM Cost ^{1,2} , \$ |
|-----------------------|---|-------------------------|--------------------------------|------------------------------|
| Water | Cathode planar membrane humidifier (for air) | ANL | 96 | 111 |
| Management | Anode planar membrane humidifier (for H_2) | ANL | 52 | 59 |
| | HT automotive tube-fin radiator | Modine | 83 | 95 |
| | LT automotive tube-fin radiator | Modine | 13 | 15 |
| | Air precooler | Bell Intercooler | - | 43 |
| Thermal Management | HT/LT radiator fan | McMaster-Carr | - | 75 |
| | HT coolant pump | McMaster-Carr | - | 150 |
| | LT/Air precooler coolant pump | Aweco | - | 30 |
| | Other (2 Temperature sensors) | - | - | 5 |
| | H ₂ blower | Parker Hannifin | 219 | 252 |
| | H ₂ ejectors | - | - | 40 |
| Fuel | H ₂ demister | Parker Hannifin | - | 61 |
| Management | Solenoid valves | McMaster-Carr | - | 46 |
| | Purge valve | DFMA [®] | 13 | 15 |
| | Check valve | DFMA [®] | 9 | 10 |
| | Compressor Expander Motor (CEM) | Honeywell | 687 | 790 |
| | Air demister | Parker Hannifin | - | 156 |
| Air Management | Air/H ₂ mixer | McMaster-Carr | - | 27 |
| | Flow orifice | McMaster-Carr | - | 5 |
| | Air filter | - | - | 4 |
| TOTAL | | - | 1,815 | 1,991 |



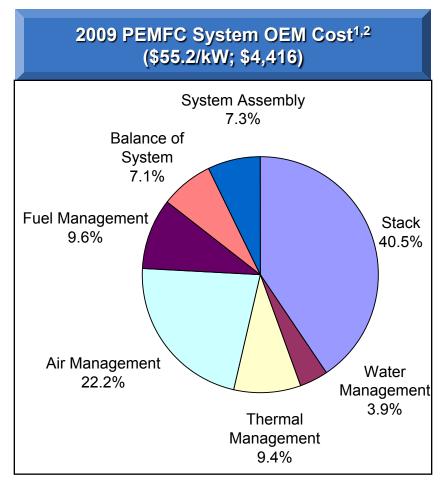
¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). ² Assumes 15% markup to the automotive OEM for BOP components

Progress 2009 PEMFC System System Cost Breakout

The 2009 PEMFC stack cost is lower than the DOE 2010 target of \$25/kW, while the system cost is higher than the DOE 2010 target of \$45/kW.

| PEMFC System Cost ¹ (\$/kW) | 2008 OEM Cost ^{1,2} | 2009 OEM Cost ^{1,2} |
|---|------------------------------------|------------------------------------|
| Stack | 29.0 | 22.3 |
| Water Management | 3.3 | 2.1 |
| Thermal Management | 2.8 | 5.2 |
| Fuel Management | 3.8 | 5.3 |
| Air Management | 8.9 | 12.3 |
| Balance of System | 3.1 | 4.0 |
| System Assembly | 5.5 | 4.0 |
| Total | 57.0 | 55.2 |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).
 ² Assumes 15% markup to the automotive OEM for BOP components

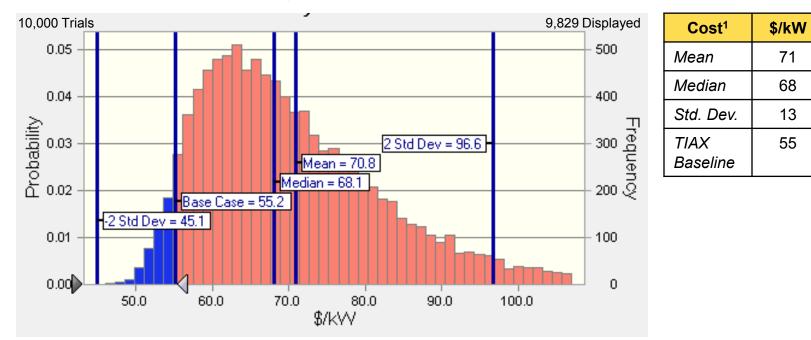


BOP, balance of system and system assembly costs together represent ~60% of the PEMFC system cost in 2009, compared to ~38% in 2005.



Progress 2009 PEMFC System *Multi-Variable Sensitivity*

Monte Carlo analysis shows that the high-volume 2009 PEMFC system OEM cost¹ ranges between \$45/kW and \$97/kW (2σ), with a mean cost of \$71/kW.

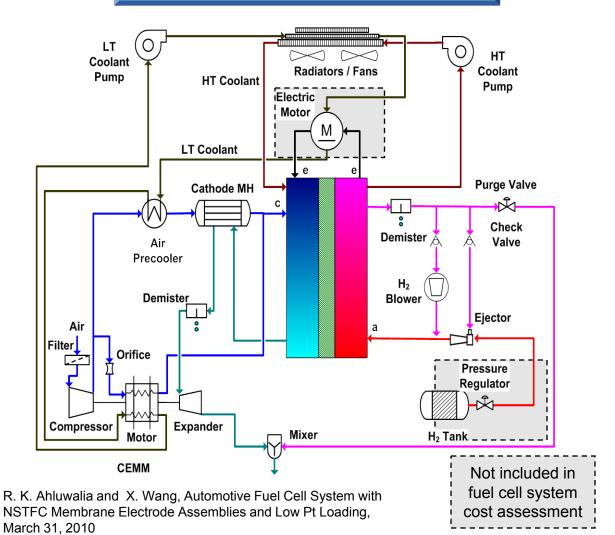


2009 PEMFC System OEM Cost¹ (\$/kW)

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Assumes a % markup to automotive OEM for BOP components.







Key features

Stack

- 3M NSTFC MEA
- 20 μm reinforced membrane
- 0.05 (a)/0.1 (c) mg/cm² Pt
- Metal bipolar plates
- Non-woven carbon paper GDL

Air Management

- CEM module
- Air-cooled motor/Air-foil bearing

Water Management

Cathode MH with precooler

Thermal Management

Advanced 40-fpi microchannel fins

Fuel Management

• Parallel ejector-pump hybrid



NSTFC = Nano-Structured Thin Film Catalyst CEM = Compressor Expander Motor MH = Membrane Humidifier

MEA = Membrane Electrode Assembly ANL = Argonne National Laboratory

To be consistent with ANL's stack performance model, we made the following material assumptions for the 2010 cost projection.

| Component | Parameter | Selection |
|--------------------------------|-------------------|---|
| Membrane | Material | 20 μm 3M PFSA |
| Memprane | Supported | Mechanically reinforced |
| | Catalyst | Ternary PtCo _x Mn _y alloy |
| Electrodes (Cathode and Anode) | Туре | Nano-Structured Thin Film |
| | Support | PR-149 Organic whiskers |
| Gas Diffusion Layer (GDL) | Material | 225 μm non-woven carbon paper ¹ |
| Gas Dillusion Layer (GDL) | Porosity | 80% |
| Bipolar Plate | Type ³ | Metal w/ Nitridation surface treatment ² |
| Seal | Material | Viton® |

¹ Ref: Ballard Material Products GDL with PTFE+MPL, AvCarb® GDS3250 @ 50 kPa

² Ref: ORNL Fe-20Cr-4V alloy with nitridation surface treatment

³ We will evaluate Au-Nanoclad SS316 plates as an alternate scenario for metal bipolar plates in 2010

We used a Pt price of \$1,100/tr.oz. for the baseline analysis and captured the impact of variation in Pt price through sensitivity analyses.



PR = Perylene Red

The **preliminary** high-volume cost of the 2010 PEMFC stack for six scenarios^{1, 2, 3} is estimated to range between \$17/kW and \$33/kW.

| Key Cost Assumptions | | | 2010 | Stack So | enarios | 1, 2, 3 | |
|--|-----------------------|---------------------------|-------|----------|---------|---------|-------|
| Key Cost Assumption | S1-1 | S1-2 | S1-3 | S2-1 | S2-2 | S2-3 | |
| System net power | kW _e | 80 | | | | | |
| Stack gross power ³ | kW _e | 90 | 91 | 92 | 86 | 87 | 88 |
| Cell voltage (rated power) ³ | V | 0.721 | 0.650 | 0.590 | 0.685 | 0.622 | 0.563 |
| Stack gross power density ³ | mW/cm ² | 573 | 1059 | 1411 | 561 | 930 | 1201 |
| Pt loading (total) ³ | mg/cm ² | | | 0.1 | 5 | | |
| Stack Pt content | g/kW _{gross} | 0.26 | 0.14 | 0.11 | 0.27 | 0.16 | 0.12 |
| System Pt content | g/kW _{net} | 0.29 | 0.16 | 0.12 | 0.29 | 0.18 | 0.14 |
| Stack efficiency (rated power) ³ | % LHV | 57 | 52 | 47 | 54 | 49 | 45 |
| System efficiency (rated power) ³ | % LHV | 50 | 45 | 40 | 50 | 45 | 40 |
| System voltage (rated power) | V | 300 | | | | | |
| System active area | m² | 15.7 8.6 6.5 15.3 9.4 7.3 | | | | 7.3 | |
| Stack cost ⁴ | \$/kW _{net} | 33.0 | 20.7 | 17.4 | 32.4 | 22.3 | 19.0 |

¹ All scenarios assume a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, and 20 μ m reinforced PFSA membrane.

² S1: 2.5 atm, 85 C; S2: 1.5 atm, 75 C

³ Based on stack and system modeling results by ANL for 2010 PEMFC system: R. K. Ahluwalia and X. Wang, March 31, 2010.

⁴ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).



We developed specifications for the 2010 PEMFC stack scenarios consistent with the performance predicted by ANL modeling^{1, 2, 3}.

| TIAX Assumptions | | 2010 Stack Scenarios ^{1, 2, 3} | | | | | |
|--|--------------------------|---|---------------|---------------|---------------|---------------|---------------|
| TIAN Assumptions | S1-1 | S1-2 | S1-3 | S2-1 | S2-2 | S2-3 | |
| Number of stacks per system | # | 1 | | | | | |
| Number of cells per stack | # | 417 | 462 | 509 | 438 | 483 | 533 |
| Active area to Total area ⁴ | % | | • | 75% | 6 | - | |
| Active area per cell | cm ² | 377 | 186 | 128 | 349 | 195 | 137 |
| Cell pitch | cells/inch (cells/cm) | 19.7 (7.8) | 19.7 (7.8) | 19.7 (7.8) | 19.7 (7.8) | 19.7 (7.8) | 19.7 (7.8) |
| System voltage (rated power) | V | | | 300 |) | • | - |

 1 All scenarios assume a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, and 20 μm reinforced PFSA membrane.

 2 S1: 2.5 atm, 85 C; S2: 1.5 atm, 75 C

³ Based on stack and system modeling results by ANL for 2010 PEMFC system: R. K. Ahluwalia and X. Wang, March 31, 2010.

⁴ Active area to Total area ratio reduced from 85% in 2009 to 75% in 2010, based on feedback from OEMs and FCTT



The reinforced 20 μ m PFSA membrane is estimated to cost ~\$19/m² on an active area basis, with materials representing ~85% of the cost.

| Membrane Manufactured Cost ¹ | | | | | | | |
|---|----------------------|---------|------------------|---------|--|--|--|
| Component | Mat | erial | Process | | | | |
| | (\$/m²) | (\$/kg) | (\$/m²) | (\$/kg) | | | |
| Film Handling | 6.33 | 107.64 | 0.33 | 5.67 | | | |
| Coating | 9.64 | 163.83 | 0.42 | 7.10 | | | |
| Drying & Cooling | 0.00 | 0.00 | 1.87 | 31.84 | | | |
| Quality Control | 0.00 | 0.00 | 0.03 | 0.57 | | | |
| Laminating | 0.00 | 0.00 | 0.05 | 0.89 | | | |
| Packaging | 0.03 | 0.43 | 0.03 | 0.44 | | | |
| Subtotal | 15.99 2.74 2.74 46.5 | | | | | | |
| Total | 18.73 (\$/m²) | | | | | | |
| | | 318.42 | 2 (\$/kg) | | | | |

¹ Manufactured cost on an active area basis or per kg of finished membrane basis (accounts for scrap and yield)

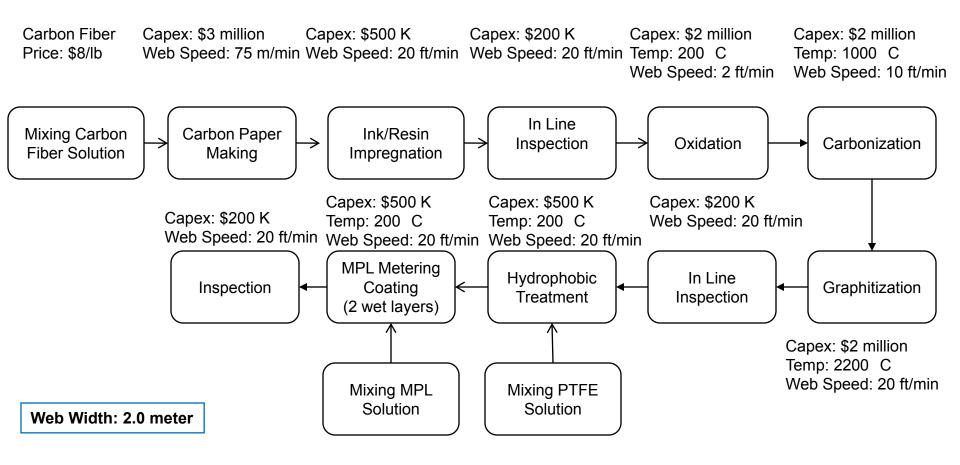
² 3M PFSA ionomer cost preliminarily increased by factor of 20% over 2009 Nafion[®] baseline cost of \$80/lb due to higher cost risk for shorter side chain PFSA ionomer: to be verified by industry feedback in 2010

³ ePTFE cost preliminarily assumed to be \$5/m²: to be verified by industry feedback in 2010

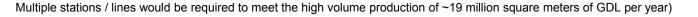
Membrane Manufactured Cost (\$19/m²) Equipment & Tooling Others Labor 4.6% 2.3% 0.9% Capital Cost 6.9% Material 85.3%

The **preliminary** 2010 membrane cost estimate is higher due to increased ionomer² and ePTFE³ costs for the reinforced membrane.

In 2010, we costed a non-woven carbon paper GDL with PTFE+MPL.



The 2010 GDL cost is based on discussions with Ballard Material Products on their AvCarb® GDS3250, suitable for automotive applications.

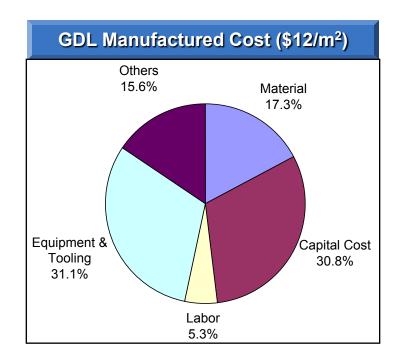


The preliminary cost of the 2010 non-woven carbon paper GDL (for both anode and cathode), is \sim \$12/m², on an active area basis.

| Manufactured Cost ¹ | GDL (\$/m²) | GDL (Anode + Cathode) (\$/m²) |
|-----------------------------------|----------------|-------------------------------------|
| Material | 1.02 | 2.05 |
| Capital Cost | 1.83 | 3.66 |
| Labor | 0.31 | 0.63 |
| Tooling | 1.85 | 3.69 |
| Other ² | 0.92 | 1.84 |
| Total | 5.94 | 11.87 |

¹ Manufactured cost on an active area basis

² Other costs include utilities, maintenance, and building



The GDL costing is changed from "buy untreated woven carbon cloth" in 2009 to "fabricate non-woven carbon paper + PTFE + MPL" in 2010.



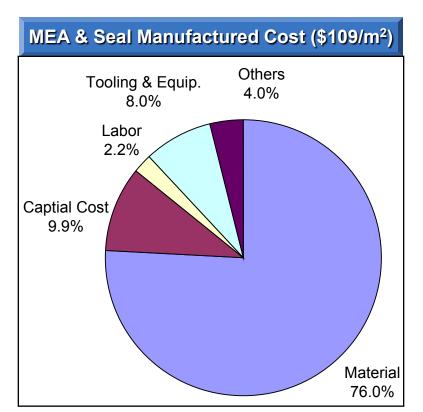
Using S2-2 as an example scenario, the 2010 MEA and seal together are estimated to cost ~\$109/m².

| Manufactured Cost ¹ | MEA (\$/m²) | Frame Seal (\$/m²) | | |
|--|---------------------------------------|--------------------|--|--|
| Material - Membrane - Electrode - GDL | 77.19 - 15.99 - 59.14 - 2.05 | 5.99 | | |
| Capital Cost | 9.09 | 1.75 | | |
| Labor | 1.15 | 1.27 | | |
| Tooling & Equipment | 7.32 | 1.50 | | |
| Other ² | 3.51 | 0.71 | | |
| Subtotal | 98.26 | 11.22 | | |
| Total | 109.49 | | | |

¹ Manufactured cost on a per m² of active area basis

² Other costs include utilities, maintenance, and building

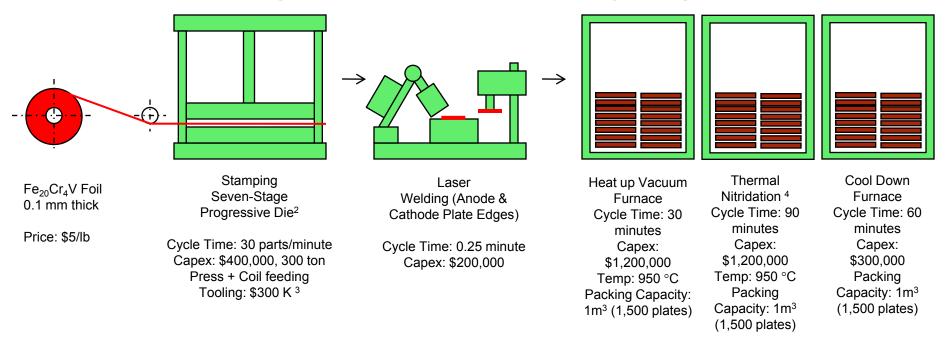
 3 Active area to Total area ratio reduced from 85% in 2009 to 75% in 2010, based on feedback from OEMs and FCTT



The preliminary estimate for the 2010 MEA & seal cost is higher due to increased ionomer and ePTFE costs for the reinforced membrane, the reduction in active area ratio³ from 85% to 75%, reduction in MEA utilization from 100% to 95%, and refinement of GDL costing.



The metal bipolar plate cost is based on discussions with ORNL on their thermal nitriding process¹ for specific alloys, e.g. Fe-20Cr-4V.



- Stamping: The anode side plate and the cathode side plate are stamp pressed by a seven stage progressive die which forms the micro flow channels, punches the main flow channels, bolt holes, and trims the edges.
- Welding: The anode and cathode side plate edges are welded together using laser welding.
- Thermal Nitridation: The bipolar plate is heated for 1.5 hours at 950 °C degree in a vacuum nitridation furnace. It takes 0.5 hour to heat up and 1 hour to cool down.
- 1. Nitrided metallic bipolar plates, M.P. Brady, et al., ORNL, DOE Merit Review presentation, May 2009
- 2. US 20090081520 (Hitachi)
- 3. Discussion with Minster Press Inc., April 2010
- 4. Preferential thermal nitridation to form pin-hole free Cr-nitrides to protect proton exchange membrane fuel cell metallic bipolar plates, M.P. Brady, et al., Scripta Materialia 50 (2004) 1017-1022

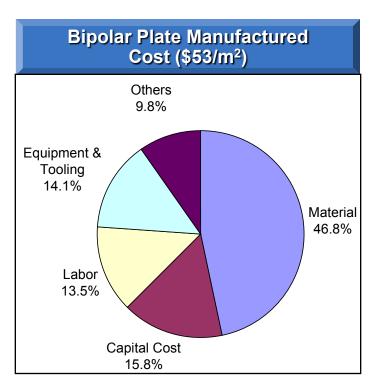


The **preliminary** cost of the nitrided Fe-20Cr-4V metal bipolar plates is estimated to be ~\$53/m² or ~\$6/kW in 2010.

| | Manufactu | r Plate ured Cost¹ m²) | Manufact | ar Plate ured Cost² kW) |
|---------------|------------------|------------------------------|----------|-------------------------------|
| Component | Material Process | | Material | Process |
| Stamping | 24.75 | 10.70 | 2.91 | 1.26 |
| Laser Welding | 0.00 | 7.05 | 0.00 | 0.83 |
| Nitridation | 0.00 | 10.40 | 0.00 | 1.22 |
| Subtotal | 24.75 28.14 | | 2.91 | 3.31 |
| Total | 52 | .89 | 6 | .22 |

¹ Manufactured cost on an active area basis

² Manufactured cost on a kW_{net} basis



The base metal foil thickness¹ is 0.1 mm and the overall bipolar plate thickness is 0.9 mm. We will also evaluate Au-Nanoclad SS316 bipolar plates in 2010.



Preliminary 2010 stack (S2-2) manufactured costs on an active area basis are higher than the 2009 stack costs, due to the reduction in active area ratio from 85% (in 2009) to 75% (in 2010).

| Stack Manufactured Cost ¹ , \$/m ² | 2009 | 2010 S2-2 ^{2, 3, 4} | ∆% | Comments |
|---|------|---------------------------------|-------|--|
| Membrane | 11 | 19 | +70% | 3M PFSA ionomer (1.2*\$80/lb) & ePTFE (\$5/m²) included in 2010 |
| Electrodes | 65 | 68 | +4% | MEA utilization rate decreased from |
| GDL | 10 | 12 | +8% | 100% in 2009 to 95% in 2010 |
| Seals | 15 | 18 | +22% | Active area decreased from 13.1 m ² in 2009 to 9.4 m ² in 2010 |
| Bipolar plates | 18 | 53 | +194% | Nitrided metallic plate in 2010 |
| Balance of Stack (Stack manifold, tie bolts, end plates, current collectors, electrical insulators) | 6 | 5 | -20% | 1 stack per system in 2010 vs. 2 stacks per system in 2009 |
| Stack Assembly ^{5, 6} | 12 | 15 | +25% | Active area decreased from 13.1 m ² in 2009 to 9.4 m ² in 2010 |
| Total Stack ⁷ | 136 | 189 | +39% | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Based on stack and system modeling results by ANL for 2010 PEMFC system: R. K. Ahluwalia and X. Wang, March 31, 2010.

 3 Assumes a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, and 20 μm reinforced PFSA membrane.

⁴ S2: stack inlet pressure @ rated power = 1.5 atm, stack temperature = 75 °C

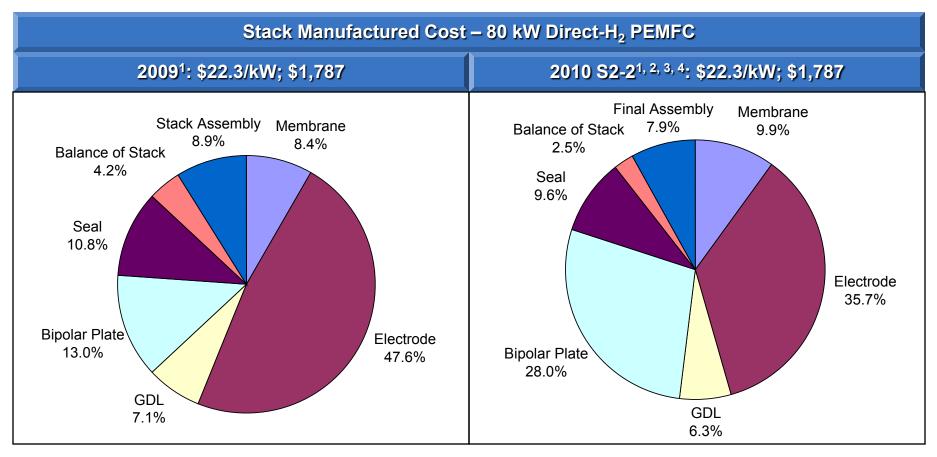
⁵ Stack Assembly cost includes QC but not Stack Conditioning; QC includes visual inspection, and leak tests for fuel loop, air loop and coolant loop

⁶ Task to "Estimate High-Volume Costs of Stack Conditioning" is planned to be completed in 2010, pending funding authorization from DOE

⁷ Results may not appear to calculate due to rounding of the component cost results.



The preliminary cost estimate for the 2010 stack (S2-2) is ~\$22/kW, which is similar to the 2009 stack cost.



¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

- ² Based on stack and system modeling results by ANL for 2010 PEMFC system: R. K. Ahluwalia and X. Wang, March 31, 2010.
- 3 Assumes a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, and 20 μm reinforced PFSA membrane.

 4 S2: stack inlet pressure @ rated power = 1.5 atm, stack temperature = 75 $^\circ\text{C}$



Preliminary 2010 stack (S2-2) manufactured costs on a net kW basis are similar to the 2009 stack costs.

| Stack Manufactured Cost ¹ , \$/kW | 2009 | 2010 S2-2 ^{2, 3, 4} | Δ% | Comments | 2010 DOE Target | |
|---|------|---------------------------------|-------|---|--------------------|--|
| Membrane | 1.9 | 2.2 | +18% | 3M PFSA ionomer (1.2*\$80/lb) & ePTFE (\$5/m²) included in 2010 | | |
| Electrodes | 10.6 | 8.0 | -25% | Power density is higher for same | | |
| GDL | 1.6 | 1.4 | -12% | Pt loading in 2010^2 ; | 10 | |
| Seals | 2.4 | 2.1 | -11% | 2010: 930 mW/cm ² , 2009: 701 mW/cm ² | | |
| Bipolar plates | 2.9 | 6.2 | +115% | Nitrided metallic plate in 2010 | 5 | |
| Balance of Stack (Stack manifold, tie bolts, end plates, current collectors, electrical insulators) | 0.9 | 0.6 | -39% | Power density is higher for same Pt loading in 2010 ² ; 2010: 930 mW/cm ² , 2009: 701 mW/cm ² | | |
| Stack Assembly ^{5, 6} | 1.8 | 1.8 | -11% | | | |
| Total Stack ⁷ | 22.3 | 22.3 | 0% | | 25 | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Based on stack and system modeling results by ANL for 2010 PEMFC system: R. K. Ahluwalia and X. Wang, March 31, 2010.

 3 Assumes a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, and 20 μm reinforced PFSA membrane.

⁴ S2: stack inlet pressure @ rated power = 1.5 atm, stack temperature = 75 °C

⁵ Stack Assembly cost includes QC but not Stack Conditioning; QC includes visual inspection, and leak tests for fuel loop, air loop and coolant loop

⁶ Task to "Estimate High-Volume Costs of Stack Conditioning" is planned to be completed in 2010, pending funding authorization from DOE

⁷ Results may not appear to calculate due to rounding of the component cost results.



The preliminary high-volume OEM cost of the 2010 PEMFC system for six scenarios^{1, 2, 3} is estimated to range between \$49/kW and \$65/kW.

| PEMFC System Cost ¹ | | | | | | | |
|-------------------------------------|----------------------|------|------|------|------|------|------|
| (\$ľkW) | Cost ^{4, 5} | S1-1 | S1-2 | S1-3 | S2-1 | S2-2 | S2-3 |
| Stack ⁴ | 22.3 | 33.0 | 20.7 | 17.4 | 32.4 | 22.3 | 19.0 |
| Water Management ^{5, 6, 7} | 2.1 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| Thermal Management ^{5, 7} | 5.2 | 5.2 | 5.2 | 5.2 | 5.2 | 5.2 | 5.2 |
| Fuel Management ^{5, 7} | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 |
| Air Management ^{5, 7, 8} | 12.3 | 12.2 | 12.4 | 12.9 | 9.9 | 10.4 | 10.6 |
| Balance of System ^{5, 7} | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| System Assembly | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Total System ^{4, 5, 6, 7} | 52.4 | 65.0 | 52.9 | 50.0 | 62.2 | 52.4 | 49.4 |

 1 All scenarios assume a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, and 20 μm reinforced PFSA membrane.

 2 S1: 2.5 atm, 85 C; S2: 1.5 atm, 75 C

³ Based on stack and system modeling results by ANL for 2010 PEMFC system: R. K. Ahluwalia and X. Wang, March 31, 2010.

⁴ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

⁵ Assumes 15% markup to the automotive OEM for BOP components

⁶ Water Management in 2010 preliminarily assumes cathode planar membrane humidifier and no anode humidifier

⁷ Using 2009 cost numbers for BOP subsystems' preliminary cost; all BOP costs pending ANL input, are planned to be updated in 2010

⁸ CEM motor controller cost varies based on preliminary modeling by ANL, of CEM parasitic power, for different scenarios



Summary

The key conclusions, accomplishments and next steps for our project are summarized below.

- Key conclusions and accomplishments:
 - The 2009 PEMFC stack cost¹ was estimated to range between \$19/kW and \$40/kW over six different scenarios.
 - The PEMFC stack and system costs^{1, 2} were estimated to be \$22/kW and \$55/kW respectively, for the 2009 baseline scenario.
 - BOP, balance-of-system and system assembly costs together represented ~60% of the projected PEMFC system cost, for the 2009 baseline scenario.
 - Monte Carlo analysis shows that the 2009 PEMFC system OEM cost^{1, 2} ranges between \$45/kW and \$97/kW (2σ), with a mean cost of \$71/kW.
 - We participated in an independent peer-review of our cost analysis, and submitted a comprehensive report to DOE on our 2008 PEMFC cost analysis
 - Preliminary estimates for the manufactured cost¹ of the 2010 PEMFC stack, ranged between \$17/kW and \$33/kW over six different scenarios.
 - Preliminary estimates for the OEM cost^{1, 2} of the 2010 PEMFC system, ranged between \$49/kW and \$65/kW over six different scenarios.
- Next steps:
 - Finalize baseline scenario for 2010 PEMFC system, and develop BOP cost estimates
 - Finalize reinforced membrane, non-woven GDL and metal bipolar plate (thermal nitrided and Au-Nanoclad) cost estimates for baseline scenario for 2010 PEMFC stack
 - Develop bottom-up cost projection for stack conditioning³
 - Perform single-variable and Monte Carlo sensitivity analyses on stack and system costs

¹ High-volume manufactured cost based on a 80 kW net power PEMFC net power system.

² High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Assumes a % markup to automotive OEM for BOP components.



Acknowledgement

We would like to thank the DOE for supporting this project over the past five years, and acknowledge valuable discussions with OEMs, FCTT, developers, national labs, and equipment manufacturers.

- Key discussions this year to date include:
 - Ballard Material Products
 - Ford Motor Co.
 - Oak Ridge National Laboratory
 - Argonne National Laboratory
 - Several equipment manufacturers
 - Independent Peer Review Panel





Supplemental Slides



We coordinated with DOE, ANL, developers, and stakeholders so far this year, with additional meetings to follow.

| Audience/ Reviewer | Date | Location |
|---|------------------|---------------|
| Fuel Cell Tech Team Mtg. | May 08 | Detroit MI |
| Several Work-in-Progress Mtgs. with DOE and ANL | June – Sep 08 | Telecon |
| DOE Annual Merit Review | June 08 | Arlington VA |
| DOE HFCIT Review | Sep 08 | Washington DC |
| Fuel Cell Tech Team Review | Sep 08 | Telecon |
| Several Work-in-Progress Mtgs. with the Independent Peer Review Panel | Dec 08 – Mar 09 | Telecon |
| Several Work-in-Progress Mtgs. with DOE and ANL | Feb 09 – Sep 09 | Telecon |
| DOE Annual Merit Review | May 09 | Arlington VA |
| Fuel Cell Tech Team Review | Aug 09 | Telecon |
| Several Telecons & Mtgs. with Ford, Ballard Material Products, ORNL, ANL, and others | Feb 10 – present | Telecon |
| DOE Annual Merit Review | June 10 | Washington DC |



For Reviewers Only

Progress 2010 Stack S2-2 *Membrane Configuration*

ANL modeled a 3M PFSA membrane, with a Gore-Select[®] type of support, and total thickness of 20 microns.

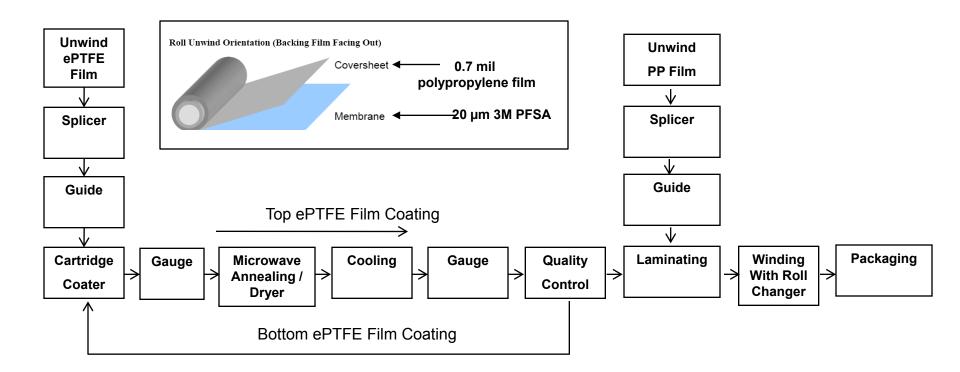
| | ePTFE | 3M PFSA ionomer Supported Membrane |
|--------------------------------------|-------|---------------------------------------|
| Thickness (µm) | 20 | 20 |
| Porosity (%) | 95% | - |
| Bulk Density (g/cm ³) | 0.098 | 1.97 |

- Impregnation of ePTFE layer with liquid ionomer solution is not suitable for a high-volume manufacturing process because both the ePTFE and ionomer film are hydrophobic. Impregnation times can be unacceptably long and repeated impregnations are needed.
 - US 6156451 (Dupont)
 - S. Ahn, Y. Lee, H. Ha, S. Hong, I. Oh, Properties of the reinforced composite membranes formed by melt-soluble ion-conducting polymer resins for PEMFCs, Electrochim. Acta 50 (2004) 571–575.
 - T.Yu,H. Lin, K. Shen, L. Huang,Y. Chang, G. Jung, J. Huang, Nafion/PTFE composite membranes for fuel cell applications, J. Polym. Res. 11 (2004)
- A double-side dispersion coating process is used in our analysis
 - US 2008/0269409 (Dupont)

We assumed a double-side dispersion coating process for membrane fabrication.



We used US 2008/0269409 to adapt our existing 3M PFSA membrane fabrication process to an ePTFE-supported membrane process.



We assumed a double-side dispersion coating process for membrane fabrication.



In 2010, we costed a non-woven carbon paper GDL with PTFE+MPL.

| Bill of Materials | Process |
|---|---|
| 2009 GDL : Woven carbon cloth MPL: 47% PTFE, 53% Carbon black | 2009 GDL: Purchase untreated woven carbon cloth Coat hydrophobic PTFE and MPL together |
| 2010 GDL : We developed a separate BOM for bare GDL+ PTFE+MPL GDL: non-woven carbon fiber paper, 10 wt% PTFE MPL: 50% PTFE, 50% Carbon black | 2010 GDL : Fabricate non-woven carbon paper Hydrophobic treatment MPL coating |

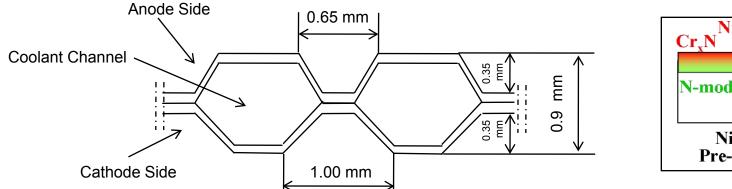
| Material | Pressure (kPa) | Bare GDL | GDL with PTFE Treatment | GDL with PTFE Treatment + MPL |
|----------------------------------|-------------------|---|---|--|
| Thickness (µm) | 50 | 185 | | 225 |
| Porosity (%) | 250 | 90% | 88% | 80% |
| Areal Weight (g/m ²) | | 40 | 44 | 75 |
| Materials | | Carbon Fiber loading: 15 g/m ² Ink/Resin loading: 25 g/m ² | 10 wt% PTFE treatment PTFE loading: 4 g/m ² | PTFE loading: 15 g/m ² Carbon black loading: 16 g/m ² |
| Comments | | AvCarb® EP40 Assume that process starts with PAN-precursor commercial-grade carbon fiber Carbon fiber price: \$8/lb | PTFE Cost: \$9.41/lb | AvCarb® GDS3250 Carbon Black Cost: \$1.52/lb |

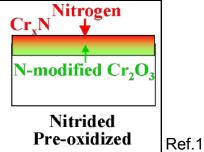
In 2009 and previous years, we combined the GDL hydrophobic coating and MPL coating together and treated them as a single process step.



Progress 2010 Stack S2-2 Metal Bipolar Plate: ORNL

Fe-20Cr-4V was picked as the base metal alloy, with nitridation surface treatment.





| Parameter | Specifications |
|---|-----------------------------|
| Bipolar Plate Area (cm ²) | 260 |
| Base Material Thickness ³ (mm) | 0.1 |
| Base Material | Fe-20Cr-4V |
| Base Material Surface Treatment | Pre-oxidation + Nitridation |
| # of Tiles in a Bipolar Plate | 2 |
| Cooling Channels? | Yes |
| Joint Method | Laser Welding Edge |

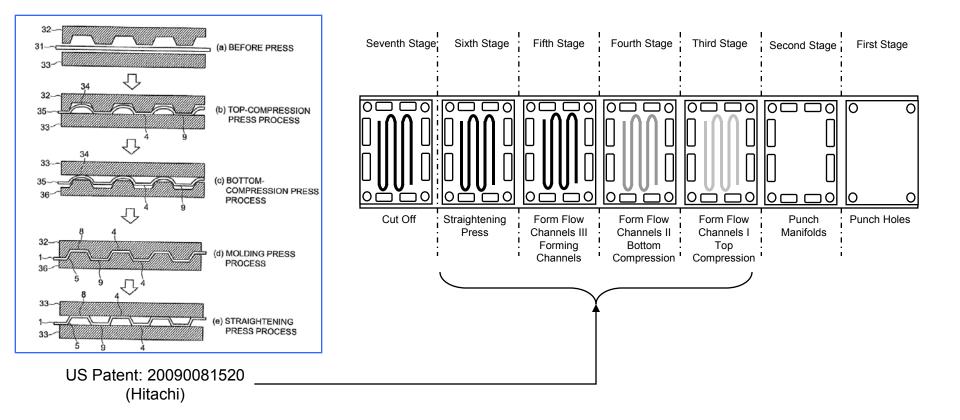
| Parameter | Dimensions |
|--|------------|
| Anode Side Channel Width ² (mm) | 0.65 |
| Anode Side Channel Depth ² (mm) | 0.35 |
| Anode Side Flow Channel Area as % of Active Area | 50% |
| Cathode Side Channel Width ² (mm) | 1.00 |
| Cathode Side Channel Depth ² (mm) | 0.35 |
| Total Thickness (mm) | 1.10 |
| Cathode Side Flow Channel Area as % of Active Area | 75% |
| Overall Active Area | 75% |
| Cavity as % of Active Area | 73% |
| Cavity as % of non Active Area | 87% |

The base metal foil thickness is 0.1 mm and the overall bipolar plate thickness is 0.9 mm.



- 1. Nitrided metallic bipolar plates, M.P. Brady, et al., ORNL, DOE Merit Review presentation, May 2009
- 2. GM patents: US 20070082252; US 7,291,414; US 20090186253
- 3. Discussion with ORNL, April 2010

A seven-stage progressive die is assumed, in order to prevent cracks during the thin metal forming process. The tooling cost is \sim \$300,000¹.



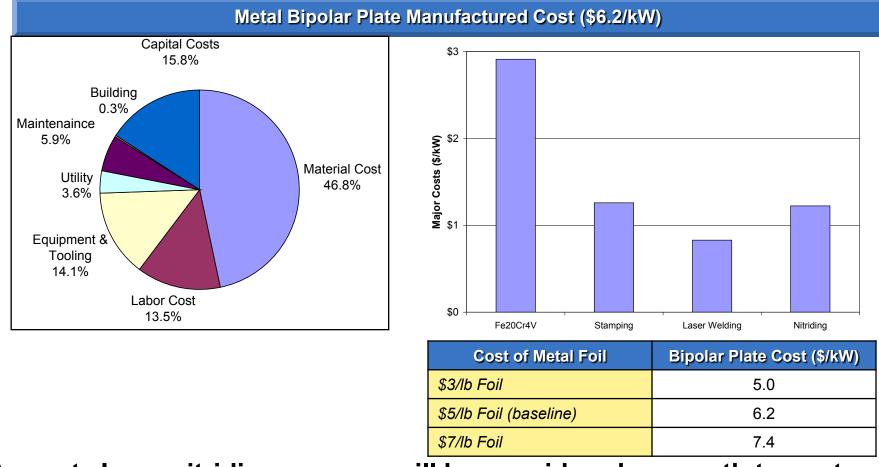
A 300 ton press with a coil feed line are assumed, with a production rate of 30 parts per minute¹.



1. Discussion with Minster Press Inc., April 2010

For Reviewers Only **Progress** 2010 Stack S2-2 *Metal Bipolar Plate: ORNL* Preliminary 2010 Results

The **preliminary** cost of the 2010 nitrided metal bipolar plates is estimated to be ~\$6/kW. The substrate alloy, stamping process, and nitriding process are the major cost drivers.

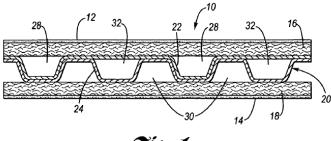


A quartz lamp nitriding process will be considered as a path to cost reduction, due to much reduced cycle time of ~10 minutes.

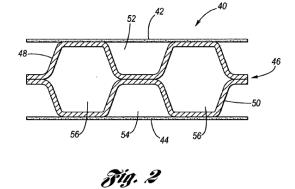
Progress 2010 Stack S2-2 Metal Bipolar Plate

Preliminary 2010 Results

US 20070082252; US 7,291,414 (GM)





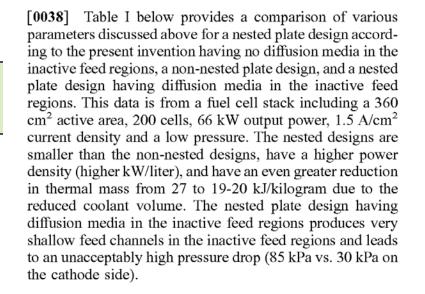


| | TABLE I | | |
|---|-----------------------------|-----------------------------|------------------------------|
| Parameter | Nested ¹ | Non-Nested ² | Nested ³ |
| Cathode channel depth (mm) Anode channel depth (mm) Feed channel depth (mm) Repeat distance (mm) | 0.34 — 0.17 0.97 | 0.35 0.31 — 1.29 | 0.34 |
| Anode ΔP (kPa) Cathode ΔP (kPa) Coolant ΔP (kPa) Power density (kW/l) Thermal mass (kJ/K) | 13 30 57 6.0 20 | 13 30 22 4.8 27 | 30 85 106 6.3 19 |

¹Nested in active feed region, non-nested in inactive feed regions, and with no diffusion media in the inactive feed regions.

²Non-nested, and no inactive feed regions.

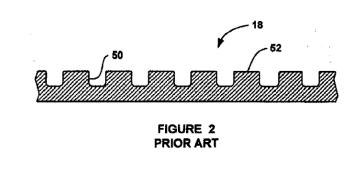
³Nested in active feed region, and non-nested in inactive feed regions, with diffusion media in the inactive feed regions.





Progress 2010 Stack S2-2 Metal Bipolar Plate

US 20090186253 (GM): 0.55 mm wide, 0.29 mm deep channels



[0012] Current fuel cell stack designs typically focus on achieving high volumetric power density by reducing the active area of the fuel cell and increasing the current density. The key enabling design features of the bipolar plate 18 for this purpose include elimination of serpentine flow channels on the cathode side 12 to avoid accumulation of liquid water in the U-bends of the channels 50, and the reduction of the channel-to-channel pitch to maximize the utilization of the catalyst layer 22 under the lands 52 in the absence of a significant channel-to-channel pressure gradient. In this design, the cathode side bipolar plate 18 includes 108 nearly rectangular channels 50 with a width of 0.55 mm and a depth of 0.29 mm and a land width of 0.65 mm. These flow field plates provide operation above 600 mV at 1.5 A/cm². One example of such a flow field plate is disclosed in U.S. patent application Ser. No. 10/669,479, titled Flow Field Plate Arrangement For A Fuel Cell, filed Sep. 24, 2003.



Using S2-2 as an example scenario, we determined the cost breakout for the MEA; materials represent ~79% of the \$98/m² MEA cost in 2010.

| Manufactured Cost | 2009 MEA ¹ | 2010 MEA ¹ | 2010 MEA Cost (\$98/m²) |
|--|--------------------------------------|---------------------------------------|---------------------------------------|
| | (\$/m ²) | (\$/m ²) | Tooling & Equip. Others 7.4% 3.6% |
| <i>Material - Membrane - Electrode - GDL</i> | 76.70 - 9.77 - 58.69 - 8.23 | 77.19 - 15.99 - 59.14 - 2.05 | Labor 1.2% Captial Cost 9.3% |
| Capital Cost | 6.18 | 9.09 | |
| Labor | 3.85 | 1.15 | |
| Tooling & Equipment | 4.21 | 7.32 | |
| Other ² | 2.03 | 3.51 | |
| Total | 93 | 98 | Material 78.6% |

The preliminary estimate for the 2010 MEA cost is higher due to increased ionomer and ePTFE costs for the reinforced membrane, the reduction in active area ratio³ from 85% to 75%, reduction in MEA utilization from 100% to 95%, and refinement of GDL costing.

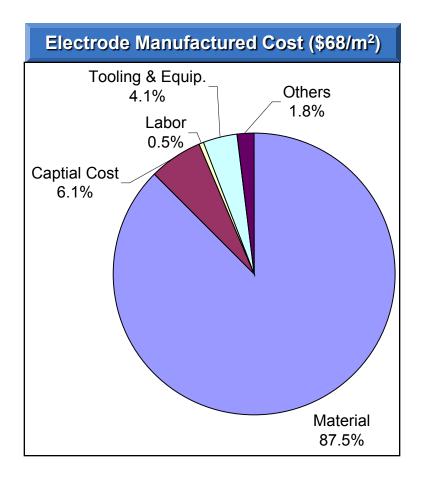


Platinum price dominates the preliminary 2010 electrode cost estimate of \$68/m². We have assumed Pt price to be \$1,100/tr.oz. or \$35.4/g.

| Manufactured Cost | Anode ¹ (\$/m²) | Cathode ¹ (\$/m ²) | Total ¹ (\$/m²) |
|----------------------|-------------------------------|--|-------------------------------|
| Material | 20.25 | 38.89 | 59.14 |
| Capital Cost | 1.58 | 2.56 | 4.14 |
| Labor | 0.16 | 0.19 | 0.35 |
| Tooling | 1.12 | 1.65 | 2.77 |
| Other ² | 0.50 | 0.72 | 1.22 |
| Total | 23.61 | 44.02 | 67.63 |

¹ m² of active area

² Other costs include utilities, maintenance, and building



Platinum at \$1,100/tr.oz. is close to the average price (\$1,096/tr.oz.) over the last year.

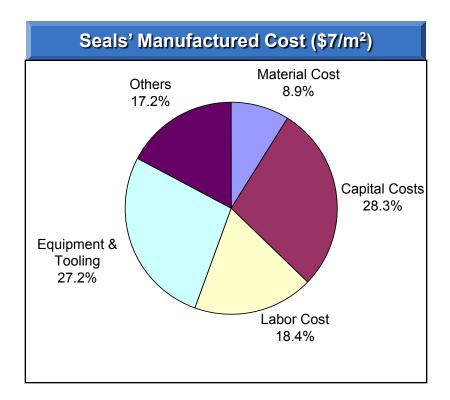


The preliminary cost of the 2010 seals is estimated to be ~\$7/m².

| Manufactured Cost ¹ | Seals (\$/m²) |
|-----------------------------------|------------------|
| Material | 0.63 |
| Capital Cost | 1.99 |
| Labor | 1.30 |
| Tooling | 1.92 |
| Other ² | 1.22 |
| Total | 7.05 |

¹ Manufactured cost on an active area basis

² Other costs include utilities, maintenance, and building



Transfer molding is used to fabricate the seals between the MEA and bipolar/cooling plate. The seal material is Viton[®] which costs ~\$20/lb.



Preliminary results of 2010 PEM fuel cell stack (S2-2) cost breakdown.

| | | | Active A | rea Basis ¹ | | | | | | |
|-----|----------------------------------|---------------------|--------------------------------------|------------------------------------|-------------------------------------|--|--|--|--|---|
| | Stack Costs | Mtl Cost (\$/m²) | Process Cost (\$/m ²) | Total Cost (\$/m ²) | Unit Cell Weight/Area (g/cm²) | Total Fuel Cell Module Weight | Total Fuel Cell Module Mtl Cost (\$) | Total Fuel Cell Module Process Cost (\$) | Total Fuel Cell Module Cost (\$) | Total Fuel Cell Module Cost (\$/kW) |
| | Anode GDL | \$1.0 | \$4.9 | \$5.9 | \$0.0 | \$1.8 | \$9.7 | \$46.3 | \$56.0 | \$0.7 |
| | Anode Active Layer | \$20.2 | \$3.4 | \$23.6 | \$0.0 | \$0.0 | \$190.6 | \$31.6 | \$222.2 | \$2.8 |
| MEA | Electrolyte | \$16.0 | \$2.7 | \$18.7 | \$0.0 | \$0.3 | \$150.6 | \$25.8 | \$176.3 | \$2.2 |
| | Cathode Active Layer | \$38.9 | \$5.1 | \$44.0 | \$0.0 | \$0.0 | \$366.1 | \$48.3 | \$414.4 | \$5.2 |
| | Cathode GDL | \$1.0 | \$4.9 | \$5.9 | \$0.0 | \$1.8 | \$9.7 | \$46.3 | \$56.0 | \$0.7 |
| | MEA Total | \$77.2 | \$21.1 | \$98.3 | 0.04 | 4 | \$727 | \$198 | \$925 | \$12 |
| Bi | ipolar Coolant Plate | \$24.8 | \$28.1 | \$52.9 | \$0.1 | \$20.1 | \$233.0 | \$264.9 | \$497.9 | \$6.2 |
| Bi | ipolar Interconnect ² | \$0.0 | \$0.0 | \$0.0 | \$0.0 | \$0.0 | \$0.0 | \$0.0 | \$0.0 | \$0.0 |
| | Gaskets | | | | | \$1.2 | \$59.3 | \$112.6 | \$171.9 | \$2.1 |
| | End Plates | | | | | \$0.7 | \$2.9 | \$1.2 | \$4.1 | \$0.1 |
| | Current Collector | | | | | \$0.4 | \$1.0 | \$0.5 | \$1.6 | \$0.0 |
| | Insulator | | | | | \$0.3 | \$6.3 | \$0.4 | \$6.8 | \$0.1 |
| | Outer Wrap | | | | | \$1.8 | \$5.5 | \$2.4 | \$7.9 | \$0.1 |
| | Tie Bolts | | | | | \$2.9 | \$23.3 | \$1.8 | \$25.1 | \$0.3 |
| | Final Assy | | | | | | | \$141.3 | \$141.3 | \$1.8 |
| | Total Unit Cell | \$101.9 | \$49.2 | \$151.2 | 0.11 | 31 | \$1,058 | \$724 | \$1,781 | \$22.3 |

¹ High-volume manufactured cost on an active area basis, for a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). ² Based on stack and system modeling results by ANL for 2010 PEMFC system: R. K. Ahluwalia and X. Wang, March 31, 2010.

 3 Assumes a Pt cost of \$1,100/tr.oz., NSTFC-based MEA, and 20 μm reinforced PFSA membrane.

⁴ S2: stack inlet pressure @ rated power = 1.5 atm, stack temperature = 75 °C

⁵ Stack Assembly cost includes QC but not Stack Conditioning ; QC includes visual inspection, and leak tests for fuel loop, air loop and coolant loop

⁶ Task to "Estimate High-Volume Costs of Stack Conditioning" is planned to be completed in 2010, pending funding authorization from DOE



Stack performance assumptions were updated by ANL based on their modeling of an NSTFC-based MEA and a 20 μm PFSA membrane.

| Key Stack Performance | 2005 ¹ | 2007 ^{2,3} | 2008 ⁴ | 2009 ⁵ | |
|----------------------------|--------------------|----------------------------|--------------------------|-------------------|-------|
| Net power | kW _e | 80 | 80 | 80 | 80 |
| Gross power | kW _e | 89.5 | 86.4 | 86.9 | 92.1 |
| Gross power density | mW/cm ² | 600 | 753 | 716 | 701 |
| Cell voltage (rated power) | V | 0.65 | 0.68 | 0.685 | 0.693 |
| Pt loading (total) | mg/cm ² | 0.75 | 0.30 | 0.25 | 0.15 |
| Membrane thickness | μm | 50 | 30 | 30 | 20 |
| Stack temperature | °C | 80 | 90 | 90 | 90 |
| Pressure (rated power) | atm | 2.5 | 2.5 | 2.5 | 2.5 |
| Stack eff. (rated power) | % LHV | 52 | 54 | 54 | 55 |

¹ E.J. Carlson et al., Cost Analysis of PEM Fuel Cell Systems for Transportation, NREL/SR-560-39104, Sep 30, 2005

² R.K. Ahluwalia and X. Wang, Reference Fuel Cell System Configurations for 2007: Interim Results, ANL, Feb. 6, 2007

³ R.K. Ahluwalia, X. Wang and R. Kumar, Fuel Cell Systems Analysis, DOE Hydrogen Program Review, May 15-18, 2007

⁴ R. K. Ahluwalia, X. Wang and R. Kumar, Fuel Cell Systems Analysis, 2008 USDOE Hydrogen Program Review, Arlington, VA, June 9-13, 2008 ⁵ R. K. Ahluwalia and X. Wang, Automotive Fuel Cell System with NSTFC Membrane Electrode Assemblies and Low Pt Loading, July 21, 2009

Key assumptions in 2009 represent ANL's inclusion of new performance data from 3M at the cell/short-stack level, and from Honeywell on the CEM parasitic power.



2009 stack costs on a per kW basis are lower than the 2008 stack costs primarily due to the lower Pt loading, thinner membrane, and reduced stack assembly time.

| Stack Manufactured Cost ¹ , \$/kW | 2005 | 2007 | 2008 | 2009 | 2010 DOE Target |
|---|------|------|------|------|-----------------|
| Membrane | 4 | 2 | 2 | 2 | |
| Electrodes | 52 | 18 | 16 | 11 | 10 |
| GDL | 3 | 2 | 2 | 2 | 10 |
| Seals | 1 | 2 | 2 | 2 | |
| Bipolar plates | 3 | 3 | 3 | 3 | 5 |
| Balance of Stack (Stack manifold, tie bolts, end plates, current collectors, electrical insulators) | 1 | 1 | 1 | 1 | |
| Stack Assembly ² | 2 | 3 | 3 | 2 | |
| Total ³ | 67 | 31 | 29 | 22 | 25 |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Stack Assembly cost in 2005 includes neither QC nor Stack Conditioning, while in 2007-2009, it includes QC but not Stack Conditioning.

³ Results may not appear to calculate due to rounding of the component cost results.



2009 stack costs on an active area basis are lower than the 2008 stack costs primarily due to the lower Pt loading, thinner membrane, and reduced stack assembly time.

| Stack Manufactured Cost ¹ , \$/m ² | 2005 | 2007 | 2008 | 2009 |
|---|------|------|------|------|
| Membrane | 23 | 16 | 16 | 11 |
| Electrodes | 279 | 120 | 102 | 65 |
| GDL | 18 | 13 | 13 | 10 |
| Seals | 6 | 13 | 13 | 15 |
| Bipolar plates | 17 | 18 | 18 | 18 |
| Balance of Stack (Stack manifold, tie bolts, end plates, current collectors, electrical insulators) | 6 | 6 | 6 | 6 |
| Stack Assembly ² | 10 | 23 | 23 | 12 |
| Total ³ | 361 | 210 | 191 | 136 |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

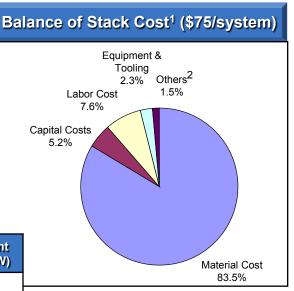
² Stack Assembly cost in 2005 includes neither QC nor Stack Conditioning, while in 2007-2009, it includes QC but not Stack Conditioning. ³ Results may not appear to calculate due to rounding of the component cost results.



Material costs represent ~84% of the Balance of Stack cost because the components have relatively simple, mature manufacturing processes.

| Balance of Stack Cost ¹ (\$) | | | | |
|---|-----------|--|--|--|
| Component | Cost (\$) | | | |
| Current Collectors | 3.7 | | | |
| Insulators | 18.2 | | | |
| End Plates | 10.2 | | | |
| Tie Bolts | 21.4 | | | |
| Stack Manifold / Outer Wrap | 21.2 | | | |
| Total | 74.7 | | | |

| Process Name | Capex Per Station (\$) | # of Stations | Labor Per Station | Cycle Time (sec/unit) | Required Space (m²) | Equipment Power (kW) |
|---|---------------------------|------------------|----------------------|--------------------------|------------------------|-------------------------|
| Die Cast Endplate | 300,000 | 1 | 1 | 10 | 40 | 10 |
| Die Cut Endplate Insulator | 40,000 | 2 | 1 | 5 | 10 | 5 |
| Cut T- Bolt | 20,000 | 3 | 0.5 | 30 | 20 | 5 |
| Wrap Manufacturing - Shear Stock | 40,000 | 5 | 1 | 0.5 | 10 | 3 |
| Wrap Manufacturing - Turret Punch | 250,000 | 1 | 0.5 | 28 | 40 | 5 |
| Wrap Manufacturing - Bend | 105,000 | 1 | 1 | 65 | 160 | 5 |



¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

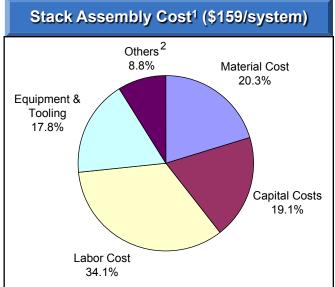
² Other costs include utilities, maintenance, and building



The assembly of the stack repeat units is assumed to be robotic, while the assembly of the balance of stack components is a manual process.

| Stack Assembly Cost ¹ (\$) | | | | | |
|---------------------------------------|-----------|--|--|--|--|
| Component/Process | Cost (\$) | | | | |
| Repeat parts (robotic) | 131.3 | | | | |
| Non-repeat parts (manual) | 5.2 | | | | |
| Stack Quality Control ³ | 22.4 | | | | |
| Total | 158.9 | | | | |

| Process Name | Capex Per Station (\$) | # of Stations | Labor Per Station | Cycle Time (sec/unit) | Required Space (m²) | Equipment Power (kW) |
|---------------------------------|---------------------------|------------------|-------------------------|--------------------------|------------------------|-------------------------|
| Stack Assembly | 400,000 | 83 | 0.2 | 1,135 | 20 | 10 |
| Balance of Stack Assembly | 20,000 | 44 | 0.2 | 600 | 20 | 5 |
| Stack QC ³ | 300,000 | 66 | 0.2 | 900 | 20 | 5 |



¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Other costs include utilities, maintenance, and building ³ Stack QC includes visual inspection, and leak tests for fuel loop, air loop and coolant loop

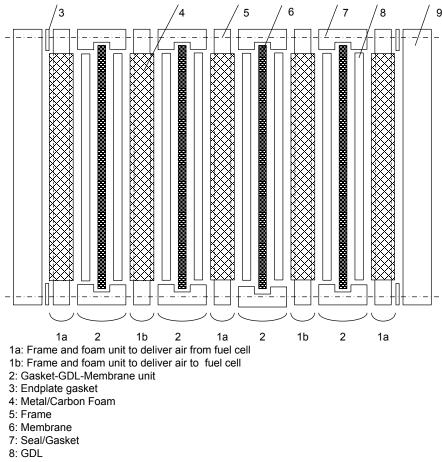
⁴ Task to "Estimate High-Volume Costs of Stack Conditioning" is planned to be completed in 2010, pending funding authorization from DOE

We estimate that 2 stacks and the BOS are assembled in ~1 hour. Stack assembly cost includes stack QC³, but not stack conditioning / burn-in costs⁴.



Progress 2009 PEMFC System Planar Membrane Humidifier

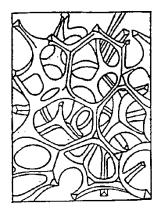
We developed bottom-up manufacturing costs for the planar membrane humidifier based on ANL specifications¹ and other patents.



9: Endplate

Referenced Patents

- U.S. Patent 6,737,183 (Nuvera)
- U.S. Patent 6,835,477 (Nuvera)
- U.S. Patent 6,864,005 (Ballard)
- U.S. Patent 7,078,117 (Ballard)



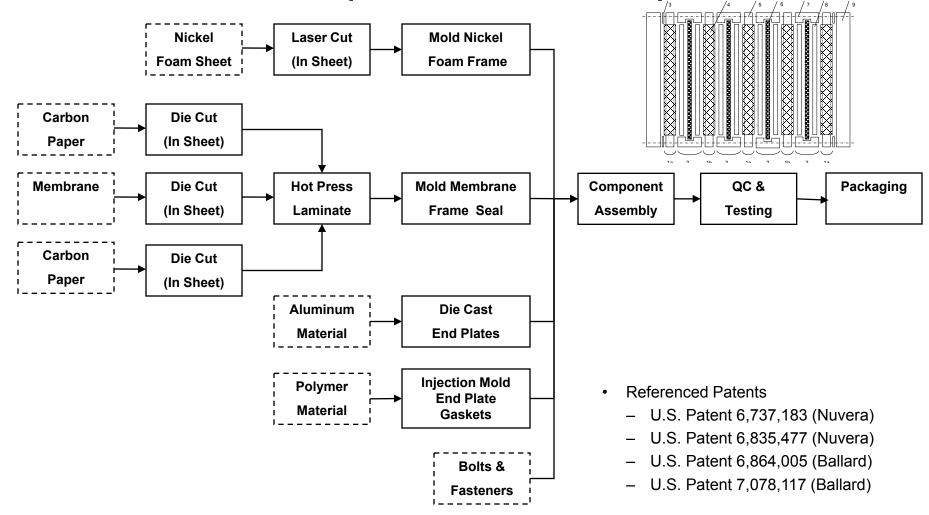
Nickel foam (U.S. Patent 6,835,477)

¹ R. K. Ahluwalia and X. Wang, Automotive Fuel Cell System with NSTFC Membrane Electrode Assemblies and Low Pt Loading, July 21, 2009



Progress 2009 PEMFC System Planar Membrane Humidifier

We developed bottom-up manufacturing costs for the planar membrane humidifier based on ANL specifications¹ and other patents.



¹ R. K. Ahluwalia and X. Wang, Automotive Fuel Cell System with NSTFC Membrane Electrode Assemblies and Low Pt Loading, July 21, 2009



Bill of Materials for the cathode/anode planar membrane humidifiers

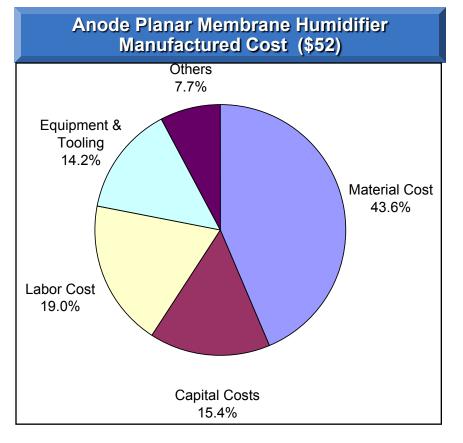
| Ca | Cathode Planar Membrane Humidifier | | | | | | |
|---------------------|------------------------------------|-----------------------|---|--|--|--|--|
| Component # | | Material | Size (mm) | | | | |
| Membrane | 42 | Nafion® | 400 (length), 140 (width), 0.03 (thickness) | | | | |
| GDL | 84 | Woven carbon fiber | 300 (length), 120 (width), 0.1 (thickness) | | | | |
| Nickel Foam | 43 | Nickel foam | 300 (length), 120 (width), 1.5 (thickness) | | | | |
| Frame | 43 | HDPE | 400 (length), 140 (width), 1.5 (thickness) | | | | |
| Membrane Gasket | 42 | Nitrile rubber | 400 (length), 140 (width), 0.22 (thickness) | | | | |
| End Plate | 2 | Al | 400 (length), 140 (width), 20 (thickness) | | | | |
| End Plate Gasket | 2 | Nitrile rubber | 400 (length), 140 (width), 0.22 (thickness) | | | | |
| Bolt | 4 | Misc. | 101 (length), 10 (OD) | | | | |
| Washer | 4 | Misc. | - | | | | |
| Nut | 4 | Misc. | - | | | | |

| Anode Planar Membrane Humidifier | | | | | | |
|----------------------------------|----|-----------------------|---|--|--|--|
| Component | # | Material | Size (mm) | | | |
| Membrane | 22 | Nafion® | 350 (length), 120 (width), 0.03 (Thickness) | | | |
| GDL | 44 | Woven carbon fiber | 250 (length), 100 (width), 0.1 (thickness) | | | |
| Nickel Foam | 23 | Nickel foam | 250 (length), 100 (width), 1.5 (thickness) | | | |
| Frame | 23 | HDPE | 350 (length), 120 (width), 1.5 (thickness) | | | |
| Membrane Gasket | 42 | Nitrile rubber | 350 (length), 120 (width), 0.22 (thickness) | | | |
| End Plate | 2 | Al | 350 (length), 120 (width), 20 (thickness) | | | |
| End Plate Gasket | 2 | Nitrile rubber | 350 (length), 120 (width), 0.22 (thickness) | | | |
| Bolt | 4 | Misc. | 68 (length), 10 (OD) | | | |
| Washer | 4 | Misc. | - | | | |
| Nut | 4 | Misc. | - | | | |



Progress 2009 PEMFC System Anode Planar MH Cost

Material costs represent approximately 44% of the anode planar membrane humidifier manufactured cost of \$52.

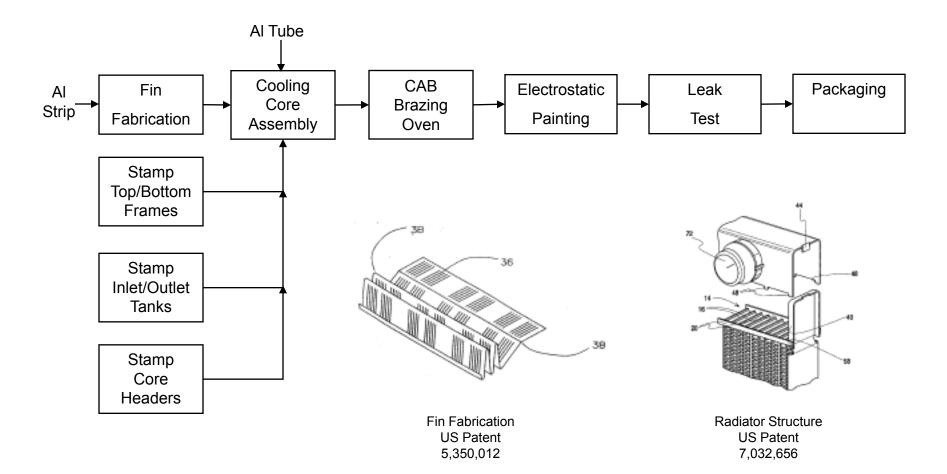


| Anode Planar Membrane Humidifier Manufactured Cost (\$) | | | | | | |
|---|----|----------|---------|--|--|--|
| Process | # | Material | Process | | | |
| Die Cut GDL | 1 | 0.91 | 1.05 | | | |
| Die Cut Membrane | 2 | 3.68 | 1.12 | | | |
| Hot Press Lamination | 3 | 0.00 | 3.18 | | | |
| Injection Molding Frame Seal | 4 | 0.00 | 2.20 | | | |
| Laser Cut Nickel Foam | 5 | 5.74 | 9.09 | | | |
| Injection Molding Foam Frame | 6 | 2.35 | 2.47 | | | |
| Injection Molding End Plate Gasket | 7 | 0.09 | 0.45 | | | |
| Die Casting End Plate | 8 | 7.11 | 1.26 | | | |
| Component Assembly | 9 | 0.00 | 3.62 | | | |
| QC & Testing | 10 | 0.00 | 3.56 | | | |
| Packaging | 11 | 0.00 | 1.06 | | | |
| Fastener Cost | - | 2.63 | 0.00 | | | |
| Total | - | 52 | | | | |

The high-volume manufactured cost of the cathode planar membrane humidifier is estimated to be \$96.



We developed a manufacturing process flow chart for the HT and LT radiators based on Modine patents and in-house experience.



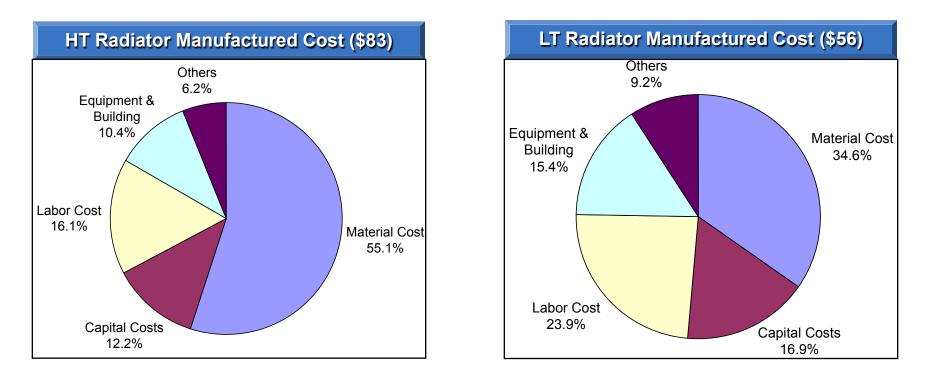


We used a Modine all-aluminum automobile radiator structure as our baseline for developing a Bill of Materials for the HT/LT radiators.

| | High-Temperature (HT) Radiator | | | | Low-Temperature (LT) Radiator | | | | Radiator |
|----|------------------------------------|-------|---------|------------------------|-------------------------------|------------------------------------|-------|---------|------------------------|
| # | Components | # | Mtl. | Size (L x W x H) (mm) | # | Components | # | Mtl. | Size (L x W x H) (mm) |
| 1 | Serpentine Louvered Fin | 39208 | AI 3003 | 59.70 x 4.44 x 0.10 | 1 | Serpentine Louvered Fin | 38381 | AI 3003 | 17.00 x 4.04 x 0.08 |
| 2 | Core Tube | 61 | AI 3003 | 700.00 x 59.70 x 2.80 | 2 | Core Tube | 64 | AI 3003 | 700.00 x 17.00 x 2.80 |
| 3 | Inlet Header, Solder Well Type | 1 | AI 3003 | 546.00 x 99.70 x 1.80 | 3 | Inlet Header, Solder Well Type | 1 | AI 3003 | 523.80 x 57.00 x 1.80 |
| 5 | Outlet Header, Solder Well Type | 1 | AI 3003 | 546.00 x 99.70 x 1.80 | 5 | Outlet Header, Solder Well Type | 1 | AI 3003 | 523.80 x 57.00 x 1.80 |
| 8 | Top Side Piece | 1 | AI 3003 | 720.00 x 99.70 x 1.80 | 8 | Top Side Piece | 1 | AI 3003 | 720.00 x 57.00 x 1.80 |
| 9 | Bottom Side Piece | 1 | AI 3003 | 720.00 x 99.70 x 1.80 | 9 | Bottom Side Piece | 1 | AI 3003 | 720.00 x 57.00 x 1.80 |
| 10 | Inlet Tank | 1 | AI 3003 | 446.00 x 140.00 x 1.80 | 10 | Inlet Tank | 1 | AI 3003 | 423.80 x 140.00 x 1.80 |
| 11 | Inlet Hose Connection | 1 | AI 3003 | 50.40 | 11 | Inlet Hose Connection | 1 | AI 3003 | 50.40 |
| 12 | Outlet Tank | 1 | AI 3003 | 446.00 x 140.00 x 1.80 | 12 | Outlet Tank | 1 | AI 3003 | 423.80 x 140.00 x 1.80 |
| 13 | Outlet Hose Connection | 1 | AI 3003 | 50.40 | 13 | Outlet Hose Connection | 1 | AI 3003 | 50.40 |
| 14 | Filler neck/Overflow Tub | 1 | AI 3003 | 25.40 | 14 | Filler neck/Overflow Tub | 1 | AI 3003 | 25.40 |
| 15 | Drain Fitting | 1 | AI 3003 | 25.40 | 15 | Drain Fitting | 1 | AI 3003 | 25.40 |
| 16 | Heater Return Line Connection | 1 | AI 3003 | 25.40 | 16 | Heater Return Line Connection | 1 | AI 3003 | 25.40 |
| 17 | Coolant Level Indicator Fitting | 1 | AI 3003 | 25.40 | 17 | Coolant Level Indicator Fitting | 1 | AI 3003 | 25.40 |



The HT radiator manufactured cost is projected to be \$83, while the LT radiator manufactured cost is projected to be \$56.



Since the electric drive motor accounts for 10 kW of the 12.9 kW heat duty of the LT radiator, we account for ~22.5% of the \$56/unit cost of the LTR within the scope of the Fuel Cell System cost.



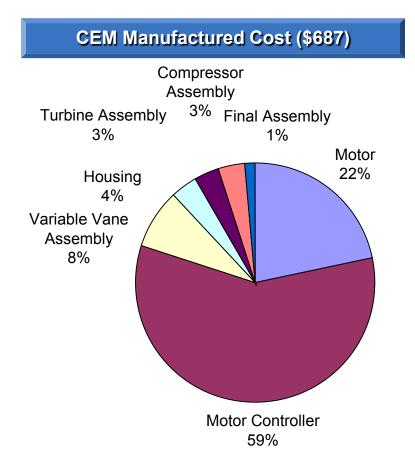
The motor assembly and motor controller are projected to cost \$564, representing 82% of the CEM manufactured cost.

| Motor Subsystems | Components | Manufactured Cost (\$) | Comments |
|------------------------|---|---------------------------|--|
| | Copper Coils | | Assumed purchased part. The price is direct |
| Stator Assembly | Steel Laminations | 26 | materials with a markup of 1.15. 1 kg copper coil (\$7/kg) and 3.6 kg laminated steel (\$4.4/kg) with a markup of 1.15. |
| | Shaft | 11 | DFMA [®] machining package |
| | Magnets | 49 | 0.55 kg NdFeB magnet with a cost of \$88/kg |
| | Journal Foil Bearing | 21 | Assumed purchased part at \$10 each |
| Rotor Assembly | Thrust Journal Bearings | 21 | Assumed purchased part at \$10 each |
| | Thrust Bearing Runner | 8 | DFMA [®] machining package |
| | Thrust Bearing Holder | 9 | DFMA [®] machining package |
| | Seals, collar, etc. | 17 | Assumed purchased parts |
| Motor Controller | 9.3 kW _e Inverter with DSP controller | 372 | \$40/kW from "A Novel Bidirectional Power Controller for Regenerative Fuel Cells", Final Report for DE-FG36-04GO14329, J. Hartvigsen and S.K. Mazumder, Oct. 10, 2005 |
| | Packaging, Wire harness, thermal management, etc | 30 | |
| Total Motor Cost (\$/u | init) | 564 | |

The 9.3 kW_e inverter is projected to dominate the motor controller cost.



The CEM manufactured cost of \$687, is the single largest cost contributor to the overall BOP cost.



| CEM Cost (\$) | | | | | |
|-------------------------------|---------------------------|-------------------------|--|--|--|
| Component | Factory Cost ¹ | OEM Cost ^{1,2} | | | |
| Motor | 162 | | | | |
| Motor Controller ³ | 402 | | | | |
| Variable Vane Assembly | 50 | | | | |
| Housing | 28 | 790 | | | |
| Turbine Assembly | 24 | | | | |
| Compressor Assembly | 21 | | | | |
| Total: | 687 | | | | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Assumes 15% markup to the automotive OEM for BOP components

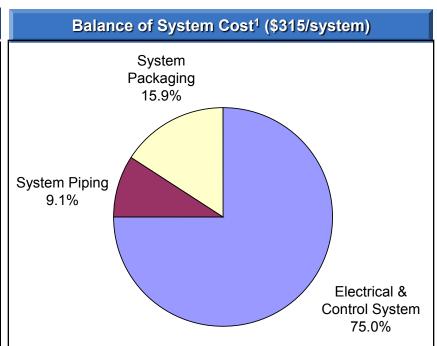
³ \$40/kW from "A Novel Bidirectional Power Controller for Regenerative Fuel Cells", Final Report for DE-FG36-04GO14329, J. Hartvigsen and S.K. Mazumder, Oct. 10, 2005

The motor assembly and motor controller (9.3 kW_e) are projected to cost \$564, representing 82% of the CEM manufactured cost.



The balance of system includes the electrical & controls system, system piping, and system packaging.

| Balance of System Cost ¹ | · (\$) | |
|---|--------|----------|
| Balance of System | # | \$315.38 |
| Startup Power | 0 | |
| Startup Battery | 0 | |
| Switching Regulator for recharging (on MB) | 0 | |
| Electrical & Controls System | 1 | \$236.58 |
| Main Control Board | 1 | \$6.00 |
| Control Power Regulator | 1 | \$6.00 |
| Control Power Circuit Breaker | 1 | \$2.00 |
| Distributed Processors | 3 | \$6.00 |
| On/off Power FET to control solenoid valves | 3 | \$3.00 |
| Pre Cooler Fan Motor Relay | 1 | \$2.00 |
| Sensor Signal Conditioning | 1 | \$10.00 |
| Memory chip for history | 1 | \$10.00 |
| Main Wiring Harness | | |
| RTD Sensor Wiring | 12 | \$7.02 |
| Other Sensor Wiring | 24 | \$14.05 |
| On/Off Valve Wiring | 4 | \$3.51 |
| Motor Control Wiring | 24 | \$14.05 |
| Connectors | 18 | \$6.58 |
| Power Wiring | 8 | \$19.20 |
| Safety Contactor | 1 | \$30.00 |
| Sensors | | |
| Humidity | 1 | \$8.36 |
| Flow Rate | 1 | \$10.00 |
| Differential Pressure | 2 | \$18.80 |
| Temperature | 2 | \$5.00 |
| H ₂ sensor for anode exhaust | 1 | \$45.00 |
| Prestack CO sensor | 1 | \$10.00 |
| System Piping | | \$28.80 |
| Piping | | \$4.80 |
| Fittings (Ts/ends) | | \$24.00 |
| System Packaging | 1 | \$50.00 |

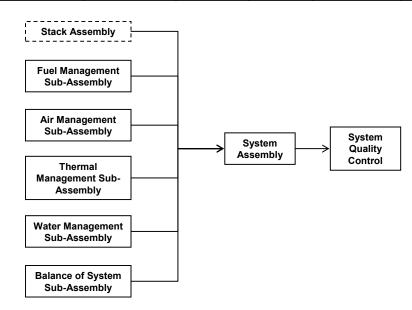


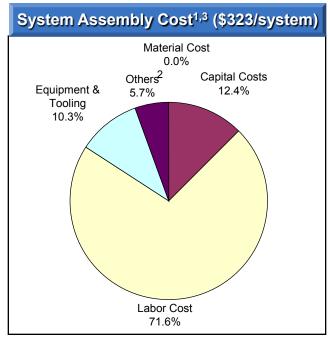
¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).



A complete 80 kW_{net} PEMFC system (including two stacks, balance-of-stack, BOP subsystems, balance-of-system, stack QC, and system QC) is estimated to be assembled in ~ 5 hours.

| Process Name | Capex Per Station (\$) | # of Stations | Labor Per Station | Cycle Time (min/unit) | Required Space (m²) | Equipment Power (kW) |
|---------------------------------|---------------------------|------------------|-------------------------|--------------------------|------------------------|-------------------------|
| System Assembly ³ | 200,000 | 462 | 1 | 213 | 20 | 10 |
| System QC ⁴ | 300,000 | 33 | 2 | 15 | 20 | 10 |





¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Other costs include utilities, maintenance, and building

³ System Assembly category includes BOP subsystem assembly, balance-ofsystem assembly, and final system assembly

⁴ System QC includes visual inspection, leakage tests, and power-on/voltage test

System Quality Control⁴ cost is included, while system conditioning / break-in is not included.



We performed single- and multi-variable sensitivity analyses to examine the impact of major stack and BOP parameters on PEMFC system cost.

- Single variable stack sensitivity analysis
 - Varied one parameter at a time, holding all others constant
 - Varied overall manufacturing assumptions, economic assumptions, key stack performance parameters, and direct material cost, capital expenses and process cycle time for individual stack components
 - Assumed stack rated power, operating pressure, temperature, humidity requirements and cell voltage remained invariant
- Single variable BOP sensitivity analysis
 - Varied one parameter at a time, holding all others constant
 - Varied overall manufacturing assumptions, economic assumptions, and direct material cost, capital expenses and process cycle time for individual BOP components
 - Assumed stack rated power, operating pressure, temperature, humidity requirements and cell voltage remained invariant
- Multi-variable (Monte Carlo) system sensitivity analysis
 - Varied all stack and BOP parameters simultaneously, using triangular PDF
 - Performed Monte Carlo analysis on individual stack and BOP components, the results of which were then fed into a system-wide Monte Carlo analysis



Pt loading, power density, and Pt cost are the top three drivers of the PEMFC system cost¹.

| 2009 PEMF0 | C Systen | | ost ¹ (\$/kW) | | # | Variables | Min | Max | Base | Comments |
|--|----------|------|--------------------------|-------|---|---|------|------|------|---|
| | 40 | \$60 | \$80 | \$100 | 1 | Pt Loading (mg/cm ²) | 0.15 | 0.75 | 0.15 | Minimum: 2009 status; Maximum: TIAX 2005 report ² |
| Pt Loading (mg/cm ²) | _ | - | | | 2 | Power Density (mW/cm ²) | 350 | 1000 | 701 | Minimum: industry feedback; Maximum: DOE 2015 target ³ . |
| Power Density (mW/cm ²) Pt Cost (\$/tr.oz.) | | - | | | 3 | Pt Cost (\$/tr.oz.) | 450 | 1675 | 1100 | Minimum: ~ 108-year min. in 2007 \$ ⁴ ; Maximum: 12-month maximum LME price ⁵ |
| Membrane Cost (\$/m ²) | - | - | | | 4 | Membrane Cost (\$/m²) | 10 | 50 | 11.4 | Minimum:GM ⁶ study; Maximum: DuPont ⁷ projection from 2002 |
| Bipolar Plate Cost (\$/kW) | | | | | 5 | Bipolar Plate Cost (\$/kW) | 1.8 | 5.0 | 2.9 | Minimum: Based on component single variable sensitivity analysis; Maximum: DOE 2010 target ³ |
| Interest Rate (%) | - | - | | | 6 | Interest Rate (%) | 8% | 20% | 15% | Based on industry feedback |
| GDL Cost (\$/kW) | - | _ | | | 7 | GDL Cost (\$/kW) | 1.3 | 1.9 | 1.6 | Minimum: 80% of the baseline; Maximum: 120% of the baseline |
| Viton [®] Cost (\$/kg) | | | | | 8 | Viton [®] Cost (\$/kg) | 39 | 58 | 48 | Based on industry feedback |

1. High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Assumes a % markup to automotive OEM for BOP components.

2. Carlson, E.J. et al., "Cost Analysis of PEM Fuel Cell Systems for Transportation", Sep 30, 2005, NREL/SR-560-39104

3. http://www1.eere.energy.gov/hydrogenandfuelcells/mypp/pdfs/fuel_cells.pdf

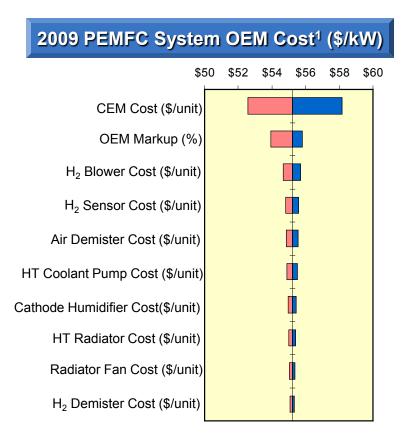
4. www.platinum.matthey.com

5. www.metalprices.com

6. Mathias, M., "Can available membranes and catalysts meet automotive polymer electrolyte fuel cell requirements?", Am. Chem. Soc. Preprints, Div. Fuel Chem., 49(2), 471, 2004 7. Curtin, D.E., "High volume, low cost manufacturing process for Nafion membranes", 2002 Fuel Cell Seminar, Palm Springs, Nov 2002



Among the BOP components, the CEM has the greatest impact on the PEMFC system cost¹.



¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW). Assumes a % markup to automotive OEM for BOP components.

² Knight, B., Clark, T. et al., "Development of Sensors for Automotive PEM-based Fuel Cells", DE-FC04-02AL67616, Dec. 2005



| # | Variables | Min | Max | Base | Comments |
|----|---|-----|-----|------|---|
| 1 | CEM Cost (\$/unit) | 472 | 925 | 687 | Based on component single variable sensitivity analysis |
| 2 | OEM Markup (%) | 5% | 20% | 15% | Based on industry feedback |
| 3 | H ₂ Blower Cost (\$/unit) | 177 | 259 | 219 | Based on component single variable sensitivity analysis |
| 4 | H ₂ Sensor Cost (\$/unit) | 10 | 80 | 45 | UTRC Final Report ² |
| 5 | Air Demister Cost (\$/unit) | 125 | 187 | 156 | Min. & Max: 20% of the base |
| 6 | HT Coolant Pump Cost (\$/unit) | 120 | 180 | 150 | Min. & Max: 20% of the base |
| 7 | Cathode Humidifier Cost (\$/unit) | 77 | 116 | 96 | Min. & Max: 20% of the base |
| 8 | HT Radiator Cost (\$/unit) | 66 | 99 | 83 | Min. & Max: 20% of the base |
| 9 | HT/LT Radiator Fan Cost (\$/unit) | 60 | 90 | 75 | Min. & Max: 20% of the base |
| 10 | H ₂ Demister Cost (\$/unit) | 49 | 73 | 61 | Min. & Max: 20% of the base |
| 11 | Anode Humidifier Cost (\$/unit) | 41 | 62 | 52 | Min. & Max: 20% of the base |
| 12 | System Packaging Cost (\$/unit) | 40 | 60 | 50 | Min. & Max: 20% of the base |
| 13 | Fuel Solenoid Valve Cost (\$/unit) | 37 | 56 | 46 | Min. & Max: 20% of the base |
| 14 | Air Precooler Cost (\$/unit) | 35 | 52 | 43 | Min. & Max: 20% of the base |
| 15 | LT Coolant Pump Cost (\$/unit) | 24 | 36 | 30 | Min. & Max: 20% of the base |
| 16 | Power System Safety Contactor Cost (\$/unit) | 24 | 36 | 30 | Min. & Max: 20% of the base |
| 17 | Air/H ₂ Mixer Cost (\$/unit) | 22 | 33 | 27 | Min. & Max: 20% of the base |
| 18 | H ₂ Purge Valve Cost (\$/unit) | 10 | 16 | 13 | Min. & Max: 20% of the base |
| 19 | H ₂ Check Valve Cost (\$/unit) | 7 | 11 | 9 | Min. & Max: 20% of the base |

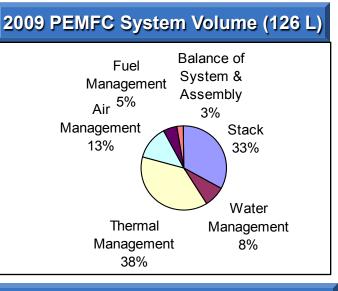
The power density and specific power of the 2009 stack and system do not meet the DOE 2010 targets.

| PEMFC Subsystem | Volume ¹ (L) | Weight (kg) | DOE 2010 Target |
|--|-------------------------|-------------|-----------------|
| Stack | 42 | 45 | |
| Membrane | 0.3 | 0.4 | |
| Electrodes | 0.0 | 0.0 | |
| GDL | 4.8 4.8 | | |
| Seals | 0.9 | 1.8 | |
| Bipolar plates | 31.0 | 26.2 | |
| Balance of Stack | 4.5 | 11.9 | |
| Power Density ^{1,2} (W _e /L) | 1,9 | 2,000 | |
| Specific Power ² (W _e /kg) | 1,7 | 2,000 | |
| Balance of Plant | 84 | 96 | |
| Water Management | 10 | 8 | |
| Thermal Management | 48 | 31 | |
| Fuel Management | 6 | 10 | |
| Air Management | 17 | 19 | |
| Balance of System & System Assembly | 3 | 27 | |
| Total System | 126 | 141 | |
| Power Density ^{1,2} (W _e /L) | 63 | 650 | |
| Specific Power ² (W _e /kg) | 56 | 650 | |

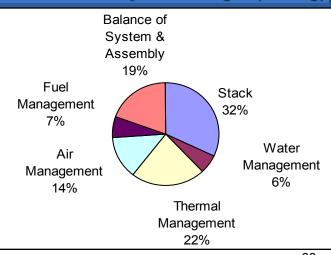
¹ Does not include packing factor, which would lower volumetric power density

² Based on stack net power output of 80 kW, and **not** on the gross power output



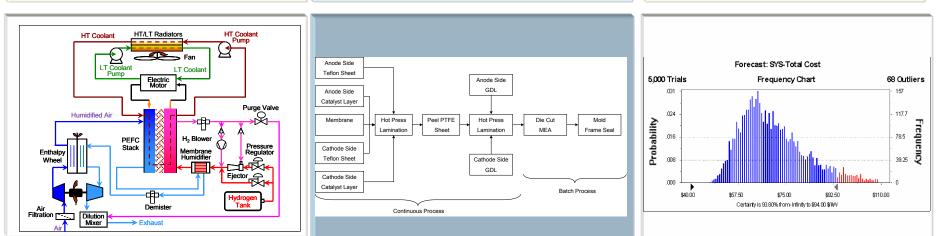


2009 PEMFC System Weight (141 kg)



Manufacturing cost estimation involves technology assessment, cost modeling, and industry input to vet assumptions and results.



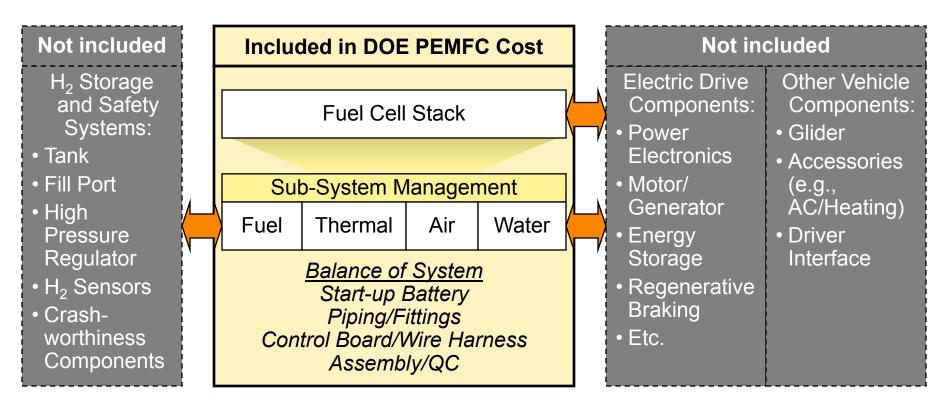




BOM = Bill of Materials

Teflon is a registered trademark of E.I. du Pont de Nemours and Company 69

Our cost assessment includes the fuel cell stack and related BOP subsystems, but does not include electric drive or other necessary powertrain components.



Quality Control (QC) includes leak and voltage tests, but does not include stack conditioning¹.



¹ Task to "Estimate High-Volume Costs of Stack Conditioning" is planned to be completed in 2010, pending funding authorization from DOE

Approach Cost Definition

We estimate an automotive OEM cost, applying no markup on stack components, and assuming a 15% markup on BOP components.

| Markup applied to BOP components | Factory Cost for Stack and BOP Components | | | | |
|--|--|---|--|--|--|
| Corporate Expenses Research and Development Sales and Marketing General & Administration Warranty Taxes | Fixed Costs Operating Tooling & Fixtures Amortization Equipment Maintenance Indirect Labor Cost of operating capital (working period 3 months) Non-Operating Equipment & Building Depreciation Cost of non-operating capital | Variable Costs Manufactured Materials Purchased Materials Direct Labor (Fabrication & Assembly) Indirect Materials Utilities | | | |

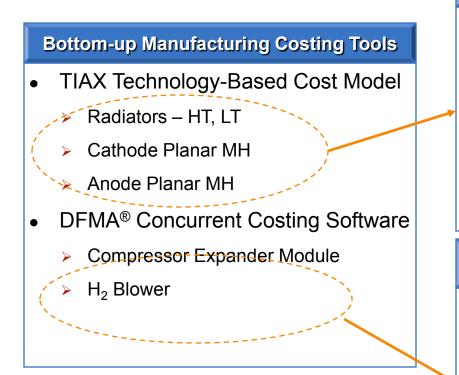
Automotive OEM Cost

- We assume a vertically integrated process for the manufacture of the stack by the automotive OEM, so no mark-up is included on the major stack components
- Raw materials are assumed to be purchased, and therefore implicitly include supplier markup
- We assume 100% debt financed with an annual interest rate of 15%, 10-year equipment life, and 25-year building life.



OEM = Original Equipment Manufacturer (i.e., car company)

We used two different bottom-up costing tools to estimate the highvolume cost of the major BOP components¹.



¹ We scaled quotes/catalog-based estimates for BOP components such as air precooler, needle metering valve, coolant pumps, radiator fans, H₂ ejectors, valves/regulators and piping/fittings.

TIAX Technology-Based Cost Model

- Defines process scenarios according to the production volume
- Easily defines both continuous as well as batch processes
- Breaks down cost into various categories, such as material, labor, utility, capital, etc.
- Assumes dedicated process line yields higher cost at low production volumes

DFMA[®] Concurrent Costing

- Has a wide range of built-in manufacturing databases for traditional batch processes, such as casting, machining, injection molding, etc.
- Initially developed for the automotive industry; not well suited for processes used in manufacture of PEMFC stacks
- Does not assume dedicated process line yields lower cost at low production volumes



To be consistent with ANL's stack performance model, we made the following material assumptions for the 2009 cost projection.

| Component | Parameter | Selection |
|--------------------------------|-----------|---|
| | Material | 20 μm PFSA |
| Membrane | Supported | No mechanical reinforcement; assumed to be chemically stabilized |
| | Catalyst | Ternary PtCo _x Mn _y alloy |
| Electrodes (Cathode and Anode) | Туре | Nano-Structured Thin Film |
| | Support | PR-149 Organic whiskers |
| Cas Diffusion Lavor (CDL) | Material | 180 μ m Woven carbon fiber |
| Gas Diffusion Layer (GDL) | Porosity | 70% |
| Bipolar Plate | Туре | Expanded graphite foil |
| Seal | Material | Viton® |

We used a Pt price of \$1,100/tr.oz. for the baseline analysis and captured the impact of variation in Pt price through sensitivity analyses.



Platinum at \$1,100/tr.oz. is close to the average price (\$1,096/tr.oz.) over the 12 month period from Aug. 2008 to Aug. 2009.



The Pt price averaged over the last five years is ~\$1,188/tr.oz.



Raw materials for stack and BOP components are assumed to be purchased, and therefore implicitly include supplier markup.

| PEMFC Sub-system | Raw Materials / Purchased Components |
|--------------------|---|
| Stack | |
| Membrane | PFSA ionomer, isopropanol, silicone-treated PET film, polypropylene film, water |
| Electrodes | Pt, Co, Mn, perylene red (PR-149) dye, aluminum-coated film substrate, Teflon [®] sheet |
| GDL | Woven carbon fiber, PTFE, carbon powder, water |
| Seal | Viton® |
| Bipolar Plates | Expanded graphite flake, vinyl ester, carbon fiber, poly dimethylsiloxane (SAG), methyl ethyl ketone peroxide, cobalt naphthenate |
| Balance of Stack | Stack manifold, tie bolts, end plates, current collectors, electrical insulators |
| Balance of Plant | |
| Water Management | Nickel foam, Nafion [®] , nitrile rubber, aluminum, HDPE, woven carbon fiber |
| Thermal Management | Aluminum coil, aluminum tubing, radiator fan, coolant pumps, air precooler, temperature sensors |
| Air Management | NdFeB magnet, steel bar stock, Teflon [®] insulation, copper coils, steel laminations, bearings, seals, motor controller, wire harness, air demister, air/H ₂ mixer, flow orifice, air filter |
| Fuel Management | SS316 bar, SS316 sheet, seals, H_2 blower motor, H_2 ejectors, H_2 demister, solenoid valves, purge valve, check valve |



Progress 2009 PEMFC Stack Cost Breakdown

Detailed results of 2009 PEM fuel cell stack cost breakdown.

| | | | Active / | Area Basis | , ¹ | | | | | |
|-------------------------------------|----------------------|---|--|--|--|-----------------------------------|---|--|---|---|
| 2009 PEMFC Stack Costs ² | | Material Cost ¹ (\$/m ²) | Process Cost ¹ (\$/m ²) | Total Cost ¹ (\$/m ²) | Unit Cell Weight/Area (g/cm ²) | Stack Module Weight (kg) | Stack Module Material Cost ² (\$) | Stack Module Process Cost ² (\$) | Stack Module Cost ² (\$) | Stack Module Cost ² (\$/kW) |
| | Anode GDL | \$4.12 | \$0.72 | \$4.84 | 0.02 | 2.37 | \$54.21 | \$9.50 | \$63.71 | \$0.80 |
| | Anode Active Layer | \$19.28 | \$3.15 | \$22.43 | 0.00 | 0.01 | \$253.95 | \$41.52 | \$295.47 | \$3.69 |
| MEA | Electrolyte | \$9.77 | \$1.67 | \$11.44 | 0.00 | 0.40 | \$128.74 | \$21.96 | \$150.70 | \$1.88 |
| | Cathode Active Layer | \$36.97 | \$5.14 | \$42.11 | 0.00 | 0.00 | \$486.97 | \$67.67 | \$554.64 | \$6.93 |
| | Cathode GDL | \$4.12 | \$0.72 | \$4.84 | 0.02 | 2.37 | \$54.21 | \$9.50 | \$63.71 | \$0.80 |
| | MEA Total | \$74.26 | \$11.40 | \$85.66 | 0.04 | 5.16 | \$978.08 | \$150.15 | \$1,128.23 | \$14.10 |
| Bij | polar Coolant Plate | \$10.25 | \$7.35 | \$17.60 | 0.10 | 26.17 | \$135.00 | \$96.83 | \$231.83 | \$2.90 |
| | Seals | | | | | 1.81 | \$79.09 | \$114.55 | \$193.64 | \$2.42 |
| | End Plates | | | | | 1.97 | \$3.91 | \$6.33 | \$10.24 | \$0.13 |
| C | Current Collectors | | | | | 1.23 | \$1.40 | \$2.26 | \$3.67 | \$0.05 |
| | Insulators | | | | | 0.80 | \$8.62 | \$9.56 | \$18.18 | \$0.23 |
| Stack Manifold/Outer Wrap | | | | | | 5.40 | \$8.13 | \$13.09 | \$21.22 | \$0.27 |
| | Tie Bolts | | | | | 2.49 | \$19.68 | \$1.72 | \$21.40 | \$0.27 |
| | Stack Assembly | | | | | | | \$158.87 | \$158.87 | \$1.99 |
| | Total Unit Cell | \$84.51 | \$18.75 | \$103.26 | 0.21 | 45.02 | \$1,233.93 | \$553.35 | \$1,787.27 | \$22.34 |

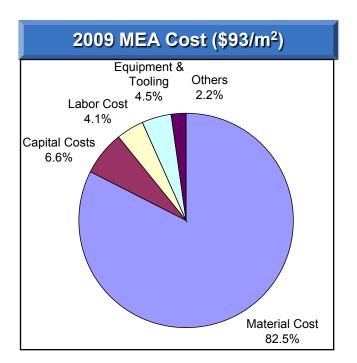
¹ Manufactured cost on an active area basis

² High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).



Material costs dominate the manufactured cost of the stack components. For example, materials make up \sim 83% of the MEA cost in 2009.

| Manufactured Cost | 2008 MEA ¹ (\$/m²) | 2009 MEA ¹ (\$/m ²) |
|---------------------|----------------------------------|---|
| Material | 117.71 | 76.70 |
| - Membrane | - 13.83 | - 9.77 |
| - Electrode | - 91.90 | - 58.69 |
| - GDL | - 11.98 | - 8.23 |
| Capital Cost | 6.57 | 6.18 |
| Labor | 1.02 | 3.85 |
| Tooling & Equipment | 3.73 | 4.21 |
| Other ² | 1.71 | 2.03 |
| Total | 131 | 93 |

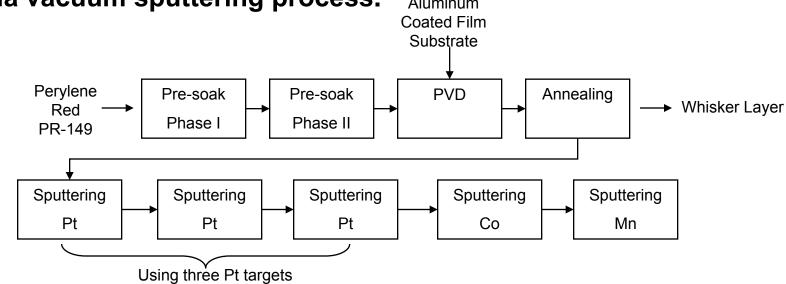


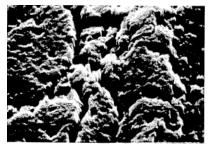
In 2009, the MEA cost was lower due to lower material costs for the membrane (20 μ m), electrodes (Pt loading = 0.15 mg/cm²) and GDL (180 μ**m)**.



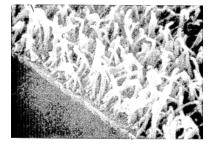
¹ m² of active area and kW of net power
 ² Other costs include utilities, maintenance, and building

Organic whisker support was fabricated by physical vapor deposition (PVD) with vacuum annealing process. Catalysts were coated to this layer via vacuum sputtering process. Aluminum





US Patent 4,812,352 PVD coated thin film before annealing



US Patent 4,812,352 PVD coated thin film after annealing

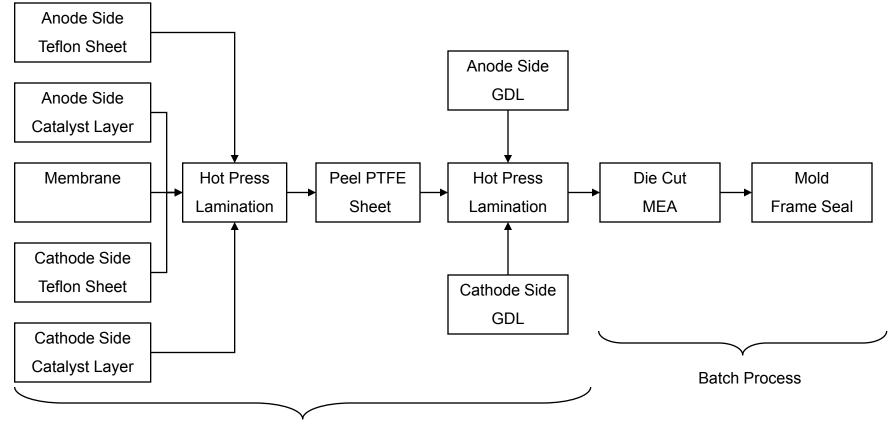


Nanostructured Thin Film Catalyst before transfer to a PEM¹

¹M. K. Debe, Durability Aspects of Nanostructured Thin Film Catalysts for PEM Fuel Cells, ECS Transactions, 1(8) 51-66 (2006)



The anode and cathode organic whisker layers were hot pressed to the membrane with Teflon[®] backing sheets.



Continuous Process

The catalyst coated membrane and GDL layers were laminated to form an MEA in roll good form; the MEA was cut into sheets and molded with a frame seal.

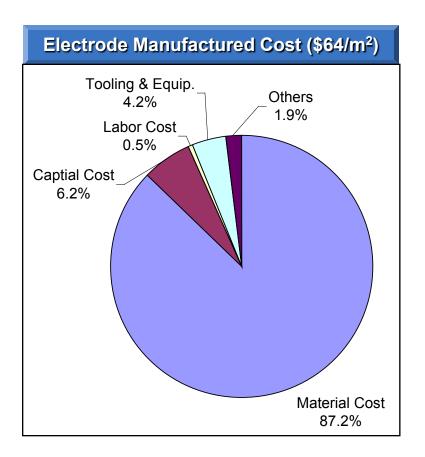


Platinum price dominates the electrode cost of \$64/m². We have assumed Pt price to be \$1,100/tr.oz. or \$35.4/g.

| Manufactured Cost | Anode ¹ (\$/m²) | Cathode ¹ (\$/m ²) | Total ¹ (\$/m²) | |
|----------------------|-------------------------------|--|-------------------------------|--|
| Material | 19.28 | 36.97 | 56.25 | |
| Capital Cost | 1.49 | 2.54 | 4.02 | |
| Labor | 0.16 | 0.19 | 0.35 | |
| Tooling | 1.04 | 1.68 | 2.72 | |
| Other ² | 0.47 | 0.73 | 1.20 | |
| Total | 22 | 42 | 64 | |

¹ m² of active area

² Other costs include utilities, maintenance, and building

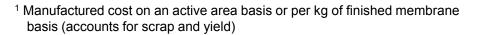


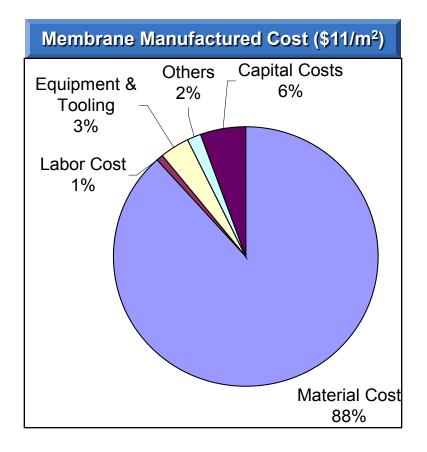
Platinum at \$1,100/tr.oz. is close to the average price (\$1,096/tr.oz.) over the last year.



The estimated membrane cost on an active area basis is \$11/m², with material cost representing about 88% of the total cost.

| Membrane Manufactured Cost ¹ | | | | | | | | |
|---|---------------------|---------|---------|---------|--|--|--|--|
| Component | Mat | erial | Process | | | | | |
| | (\$/m²) | (\$/kg) | (\$/m²) | (\$/kg) | | | | |
| Film Handling | 0.31 | 5.25 | 0.22 | 3.71 | | | | |
| Coating | 7.80 | 132.62 | 0.29 | 4.90 | | | | |
| Drying & Cooling | 0.00 | 0.00 | 1.00 | 17.02 | | | | |
| Quality Control | 0.00 | 0.00 | 0.04 | 0.60 | | | | |
| Laminating | 0.00 | 0.00 | 0.06 | 0.94 | | | | |
| Packaging | 1.66 | 28.29 | 0.07 | 1.16 | | | | |
| Subtotal | 9.77 166.16 1.67 28 | | | | | | | |
| Total | 11.44 (\$/m²) | | | | | | | |
| | 194.50 (\$/kg) | | | | | | | |





In 2008, the membrane cost was \$16/m² due to higher material costs associated with a thicker 30 μ m membrane.

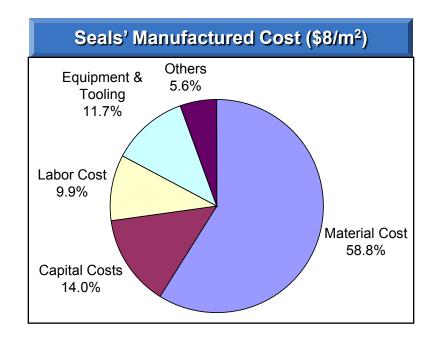


Transfer molding is used to fabricate the seals between the MEA and bipolar/cooling plate. The seal cost is ~\$8/m².

| Manufactured Cost ¹ | Seals (\$/m²) |
|-----------------------------------|------------------|
| Material | 4.78 |
| Capital Cost | 1.14 |
| Labor | 0.81 |
| Tooling | 0.95 |
| Other ² | 0.45 |
| Total | 8.13 |

¹ Manufactured cost on an active area basis

² Other costs include utilities, maintenance, and building



The seal material is Viton[®] which costs ~\$20/lb.

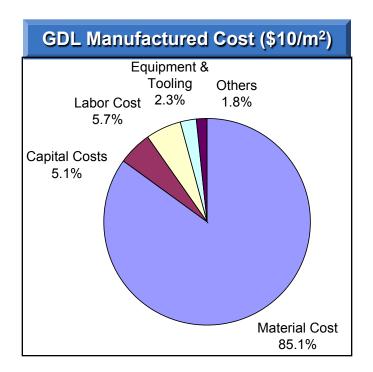


The estimated high-volume cost of the woven carbon fiber GDL (for *both* anode and cathode), is \sim \$10/m², on an active area basis.

| Manufactured Cost ¹ | GDL (\$/m²) | | |
|-----------------------------------|----------------|--|--|
| Material | 8.23 | | |
| Capital Cost | 0.50 | | |
| Labor | 0.55 | | |
| Tooling | 0.22 | | |
| Other ² | 0.17 | | |
| Total | 9.67 | | |

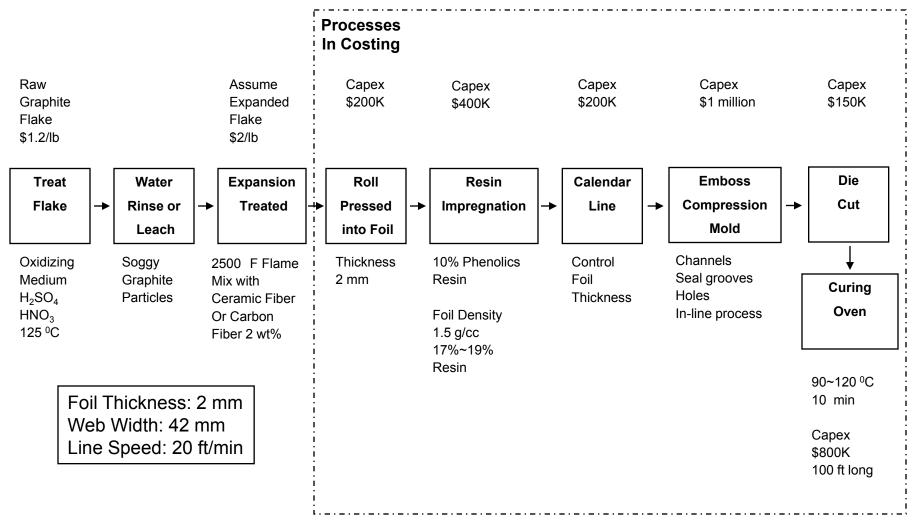
¹ Manufactured cost on an active area basis

² Other costs include utilities, maintenance, and building





Our process flow for the expanded graphite bipolar plate is based on a GrafTech[®] process chart and related patents.

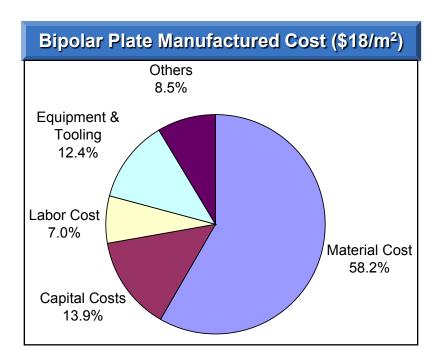




We estimate the expanded graphite foil bipolar plate cost is \$18/m² at high volume.

| Bipolar Plate Manufactured Cost ¹ (\$/m ²) | | | | | | | |
|---|------------|---------|--|--|--|--|--|
| Component | Material | Process | | | | | |
| Roll Form | 10.25 | 0.92 | | | | | |
| Impregnation | | 1.03 | | | | | |
| Calendar | | 0.66 | | | | | |
| Compression Molding | | 2.15 | | | | | |
| Die Cut | | 0.57 | | | | | |
| Curing | | 2.01 | | | | | |
| Subtotal | 10.25 7.35 | | | | | | |
| Total | 17.60 | | | | | | |

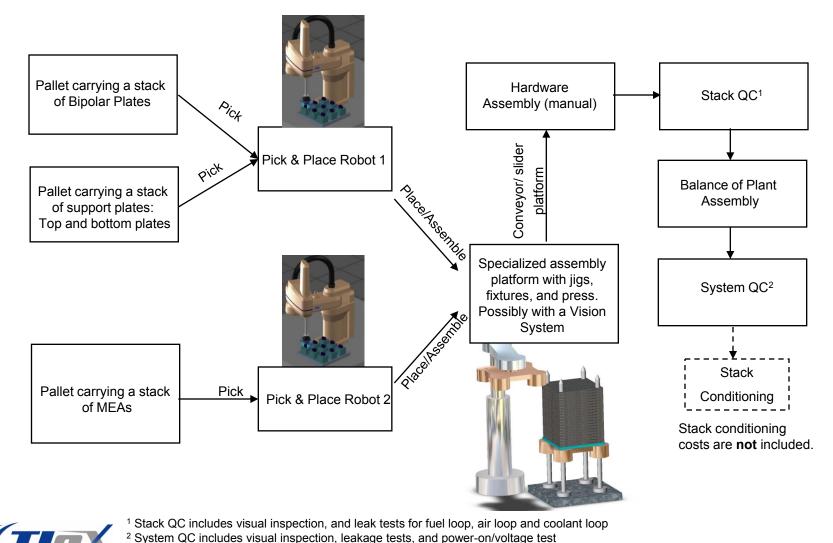
¹ Manufactured cost on an active area basis



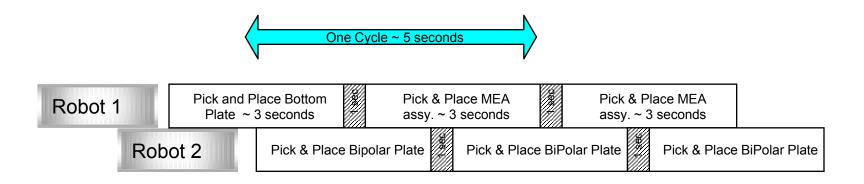
We assumed a raw graphite flake cost of \$1.2/lb and expanded graphite flake cost of \$2/lb.



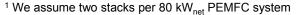
A pair of robots in a specialized assembly station with a vision system is assumed to assemble the stack.



Assuming a two-robot assembly station, we estimate that two stacks¹ and the Balance of Stack are assembled in ~ 1 hour.



| Stack assembly step | Time | Comments | | | |
|--------------------------------------|--------------|---|--|--|--|
| Pick & place a single repeat unit | ~ 5 seconds | Based on two-robot setup | | | |
| Assemble a single stack ¹ | ~ 19 minutes | For 217 MEAs and bipolar plates | | | |
| Assemble balance of stack (BOS) | ~ 10 minutes | BOS includes endplates, electrical insulators, outer wrap/stack manifold, current collectors, tie bolts | | | |
| Stack Quality Control ² | ~ 15 minutes | Stack burn-in / conditioning time is not included | | | |





² Stack QC includes visual inspection, and leak tests for fuel loop, air loop and coolant loop

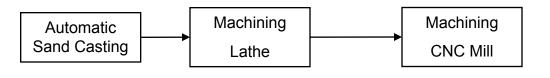
The rotor and single vane structure in the Parker Hannifin Model 55 Univane H_2 blower are referenced from U.S. Patent 5,374,172.

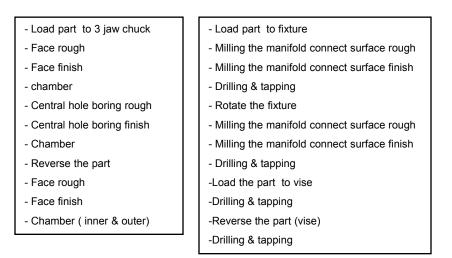
| # | Selected Components | Material | Major Manufacturing Processes | | | | |
|---|------------------------------|----------|--|--|--|--|--|
| 1 | 1 Motor Side End Plate SS316 | | Automatic sand casting; Turning; Drilling | | | | |
| 2 | Blower Housing | SS316 | Automatic sand casting; Turning; Drilling | | | | |
| 3 | Inlet Manifold | SS316 | Powder metallurgy | | | | |
| 4 | Outlet Manifold | SS316 | Powder metallurgy | | | | |
| 5 | 5 End Plate SS316 | | Automatic sand casting; Turning; Drilling | | | | |
| 6 | Blower Shaft | SS316 | Turning; Milling; Heat treatment; Grinding | | | | |
| 7 | Rotor Al | | Casting; Turning; Milling; Broaching | | | | |
| 8 | Vane | SS316 | Hot forging; Drilling; Reaming | | | | |

The major manufacturing processes for selected components of the H₂ blower are tabulated above.



The blower housing manufacturing process represents the level of detail we captured in the costing¹ of the H_2 blower.





H₂ Blower Housing Manufacturing Process



The projected H₂ blower manufactured cost is \$219 per unit.

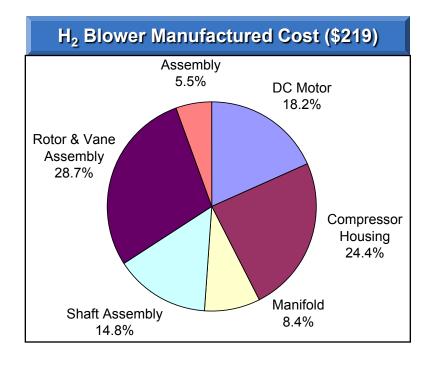
| # | | Part Name | Quantity | Material | OD (cm) | L (cm) | W (cm) | Wall Thickness (cm) | Total Vol. (Cm^3) | Total Wt. (kg) | TIAX Model Total (unit Cost) |
|----------|----------|-----------------------------|----------|----------------|--------------|---------------|----------|---------------------------|----------------------|-------------------|------------------------------------|
| | 100 | We DC Motor | 1 | Misc | 16.51 | 8.89 | w (cm) | (011) | 1902.24 | 1.00 | 40.00 |
| 2 | _ | d Plate (motor side) | 1 | SS316 | 16.51 | 2.54 | | 0.32 | 96.48 | 0.75 | \$13.75 |
| 2 | | Screw | 4 | Misc | 0.64 | 2.54 | | 0.52 | 0.80 | 0.02 | 0.20 |
| | | 00.011 | · · | | 0.01 | 2.01 | | | 0.00 | 0.02 | 0.20 |
| 4 | | O-Ring | 1 | Misc | 13.97 | | | | | 0.01 | 0.50 |
| 5 | | Labyrith Seal (main) | 1 | Misc | 5.08 | 1.27 | | | | 0.02 | 2.00 |
| 6 | | O-Ring | 1 | Misc | 5.08 | | | | | 0.01 | 0.20 |
| 7 | | C-Clip | 1 | SS316 | 5.08 | | - | | | 0.01 | 0.20 |
| ' | | 0 Olip | <u> </u> | 00010 | 0.00 | | | | | 0.01 | 0.10 |
| 8 | | Labyrith Seal | 1 | Misc | 4.45 | | | | | 0.02 | 2.00 |
| 9 | Blo | wer Housing | 1 | SS316 | 15.24 | 8.89 | | 0.32 | 106.65 | 0.83 | \$19.66 |
| 10 | | Screw | 8 | Misc | 0.64 | | | | | 0.04 | 0.40 |
| 11 | | O-Ring | 1 | Misc | 13.97 | | | | | 0.01 | 0.50 |
| 40 | | O Ob .th | | 00040 | 4.50 | 40.70 | | | 05.40 | 0.00 | 60.47 |
| 12 13 | | Compressor Shaft Bearing | 1 | SS316 SS316 | 1.59 3.81 | 12.70 2.54 | | | 25.12 28.94 | 0.20 | \$9.17 18.70 |
| 14 | | Seal | 2 | Misc | 3.81 | 2.04 | | | 20.94 | 0.23 | 0.40 |
| 15 | | Rotor | 1 | Al | 10.16 | 7.62 | | | 308.73 | 0.83 | \$9.40 |
| | | | | | | | | | | | |
| 16 | | Vane Guide | 2 | SS316 | 7.62 | 1.27 | | 1.27 | 32.06 | 0.50 | \$15.60 |
| 17 | | Vane Guide Bearing | 2 | Misc | 7.62 | 1.60 | | | 61.62 | 0.48 | 30.00 |
| 18 | | Vane | 1 | SS316 | | 7.62 | 2.54 | 1.27 | 24.58 | 0.19 | \$3.82 |
| 19 | | Vane Pin | 1 | SS316 | 0.95 | 9.62 | | | 6.85 | 0.05 | 4.00 |
| 20 | | C-Clip | 2 | SS316 | 1.35 | | | | | 0.01 | 0.10 |
| 21 | Inle | t Manifold | 1 | SS316 | 4.45 | 8.89 | | 0.64 | 35.17 | 0.27 | \$7.33 |
| 22 | | Seal | 1 | Misc | | 5.08 | 3.81 | | | 0.01 | 0.50 |
| ~~~ | | 0 | | | 0.00 | | | | | 0.02 | 0.00 |
| 23 | - | Screw | 4 | Misc | 0.32 | | | | | | 0.20 |
| 24 | | Fitting | 1 | SS316 | 4.45 | 5.08 | | | | 0.10 | 1.00 |
| 25 26 | Out | O-Ring tlet Manifold | 1 1 | Misc SS316 | 2.54 4.45 | 8.89 | | 0.64 | 35.17 | 0.01 0.27 | 0.20 \$7.33 |
| 27 | | Seal | 1 | Misc | | 5.08 | 3.81 | | | 0.01 | 0.50 |
| 28 | | Screw | 4 | Misc | | | | | | 0.02 | 0.20 |
| 29 | | Fitting | 1 | SS316 | 4.45 | 5.08 | | | | 0.10 | 1.00 |
| 30 | | O-Ring | 1 | Misc | 2.54 | | | | | 0.01 | 0.20 |
| 31 | Enc | d Plate | 1 | SS316 | 15.24 | 3.81 | | 0.64 | 72.36 | 0.56 | \$11.97 |
| 32 33 | \vdash | Screw O-Ring | 8 | Misc Misc | 8.89 | | | | | 0.04 | 0.40 |
| 34 | | End Cover | 1 | SS316 | 7.62 | 0.64 | <u> </u> | | 28.94 | 0.01 | \$5.21 |
| 35 | | Screw | 4 | Misc | | 2.01 | <u> </u> | | | 0.02 | 0.20 |
| 36 | | O-Ring | 1 | Misc | 6.35 | | | | | 0.01 | 0.20 |
| 37 | Sup | oport | 1 | Steel | | 15.24 | 15.24 | 0.25 | 58.99 | 0.46 | 0.00 |
| | | | | | | | | | | SubTotal: | \$207.44 |



Assembly: \$12.00

Total: \$219.44

The rotor & vane assembly, blower housing, and DC motor are the top three cost drivers for the H_2 blower.



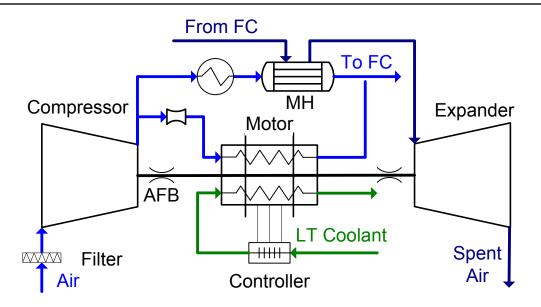
| H ₂ Blower Cost (\$) | | | | | | | | | |
|---------------------------------|---------------------------|-------------------------|--|--|--|--|--|--|--|
| Component | Factory Cost ¹ | OEM Cost ^{1,2} | | | | | | | |
| DC Motor | 40 | | | | | | | | |
| Blower Housing | 53 | | | | | | | | |
| Manifold | 18 | | | | | | | | |
| Shaft Assembly | 33 | | | | | | | | |
| Rotor & Vane Assembly | 63 | | | | | | | | |
| Assembly | 12 | | | | | | | | |
| Total: | 219 | 252 | | | | | | | |

¹ High-volume manufactured cost based on a 80 kW net power PEMFC system. Does not represent how costs would scale with power (kW).

² Assumes 15% markup to the automotive OEM for BOP components



Progress 2009 PEMFC System CEM



- Mixed axial flow compressor
- Variable nozzle turbine
- 3-phase brushless DC motor, liquid and air cooled
- Motor controller, liquid cooled
- Air foil bearing (AFB)
- Efficiencies at rated power: 70% compressor, 73% expander, 86% motor, 87% controller

R. K. Ahluwalia and X. Wang, Automotive Fuel Cell System with NSTFC Membrane Electrode Assemblies and Low Pt Loading, July 21, 2009



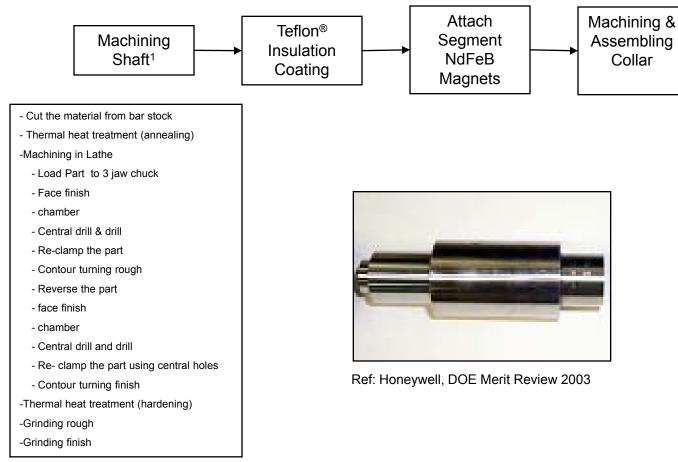
AFB = Air-foil Bearing LT = Low-Temperature

The references used to determine the overall design and major manufacturing processes for the CEM are tabulated below.

| Component | References | | # | Selected | Material | Major Manufacturing | | | |
|-----------------------------------|--|--|---|----------------------------|----------|---|--|--|--|
| Overall System | Honeywell, DOE program review, progress report & annual report, 2005, 2004, 2003, 2000; U.S. Patent | | 1 | Components Turbine Housing | AI | Processes Cold chamber die casting; Turning; Drilling | | | |
| | 5,605,045 Honeywell, DOE program review, | | 2 | Motor Housing | AI | Cold chamber die casting; Turning; Drilling | | | |
| Electrical Motor | progress report & annual report 2004; U.S. Patent 5,605,045 | | 3 | Compressor Housing | AI | Cold chamber die casting; Turning; Drilling | | | |
| Motor Power Electronics | Honeywell, DOE program review, progress report & annual report, 2005; Caterpillar, DOE Contract DE- SC05-00OR-99OR22734 | | 4 | Motor connecting shaft | Steel | Turning; Heat treatment; Grinding | | | |
| | | | 5 | NdFeB Magnet | NdFeB | Mixing; Molding; Sintering (purchased) | | | |
| Turbine Variable Nozzle Vanes, | anes, Garrett/Honeywell, DE-FC05- 000R22809 | | 6 | Turbine Wheel | AI | Investment casting; HIP | | | |
| Unison Ring | | | 7 | Compressor Impeller | AI | Investment casting; HIP | | | |
| Journal Bearings | | | 8 | Thrust Bearing Runner | Steel | Turning; Heat treatment; Grinding | | | |



The motor rotor manufacturing process represents the level of detail we captured in the costing of the CEM.



CEM Motor Rotor Manufacturing Process



¹ Boothroyd Dewhurst Machining package

The estimated CEM (including motor and motor controller) cost is \$687 per unit.

| | | | | | | | | | | | Wall | | | |
|----------|------|--|----------|--|-------------|------------|---------------|---------------|--------|--------|-----------|----------------|-----------|------------------------|
| | | | 0 | | | | | | | | Thickness | Total Vol. | Total Wt. | TIAX Model Total (unit |
| # | Too | Part Name | Quantity | Reference | Ref. Part # | Material | OD (cm) | L (cm) | W (cm) | H (cm) | (cm) | (Cm^3) | (kg) | Cost) |
| 2 | Ιu | rbine Housing Bolt | 1 | US6269642 | 24 | Al Misc | 20.32 0.60 | 1.20 | | 7.62 | 0.16 | 127.19 2.03 | 0.34 | \$5.39 \$0.30 |
| 3 | _ | Washer | 6 | | | Misc | 1.00 | 0.10 | | | | 2.03 | 0.02 | \$0.30 |
| - | Tie | Rod | 1 | US6269642 | 30 | Steel | 1.00 | 4.00 | | | | 3.14 | 0.02 | \$3.72 |
| | | rbine Wheel | 1 | | | Al | 5.00 | 5.00 | | | | 0.07 | 0.20 | \$20.00 |
| 6 | Va | riable Vane Assembly | | | | | | | | | | | | \$0.00 |
| 7 | va | Nozzle Wall | 1 | US6269642 | 38 | Steel | 17.78 | | | | 0.30 | 36.46 | 0.28 | \$2.54 |
| 8 | | Vane | 9 | US6269642 | 36 | Steel | 3.00 | 0.50 | 0.50 | | | 6.75 | 0.47 | \$15.39 |
| 9 | | Vane Post | 9 | US6269642 | 40 | Steel | 0.20 | 1.00 | | | | 0.28 | 0.02 | \$0.00 |
| 10 | | Actution Tab | 9 | US6269642 | 44 | Steel | | 1.00 | 0.30 | 0.30 | | 0.81 | 0.06 | \$0.00 |
| 11 | | Unison Ring | 1 | US6269642 | 48 | Steel | 15.24 | 0.50 | | | | 84.88 | 0.66 | \$16.88 |
| 12 | - | Actuator Crank | 1 | US6269642 | 50 | Steel | 10.21 | 2.00 | 1.00 | 1.00 | | 2.00 | 0.02 | \$1.11 |
| 13 | _ | Crank Bushing | 1 | US6269642 | 60 | Steel | 1.20 | 1.00 | | | 0.10 | 0.35 | 0.00 | \$0.05 |
| 14 | | Crank Gear | 1 | US6269642 | 62 | Steel | 2.00 | 1.00 | | | 0.50 | 2.36 | 0.02 | \$4.21 |
| 15 | | Crank Gear Pin | 1 | US6269642 | 64 | Steel | 0.20 | 2.00 | | | | 0.06 | 0.00 | \$0.10 |
| 16 | - | Crank End Bearing | 1 | US6269642 | 66 | Misc | | | | | | 3.00 | 0.02 | \$2.15 |
| 17 | | Actuator Housing | 1 | | | Al | 20.32 | 1.50 | | | 2.54 | 212.71 | 0.57 | \$6.03 |
| 18 | | Solenoid Valve | 1 | US6269642 | 85 | Misc | | | | | | | 0.20 | \$5.00 |
| 19 | | Solenoid Valve Bracket | 1 | US6269642 | 108 | Steel | | 3.00 | 1.20 | | 0.20 | 0.72 | 0.01 | \$0.01 |
| 20 | | Solenoid Valve Bracket Bolt | 1 | US6269642 | 110 | | 0.40 | 1.00 | | | | 0.13 | 0.00 | \$0.05 |
| 21 | | Washer | 1 | US6269642 | | | 0.60 | | | | 0.10 | | 0.00 | \$0.05 |
| 22 | | Rack Gear Rod | 1 | US6269642 | 88 | Steel | 0.60 | 6.00 | | | | 1.70 | 0.01 | \$0.46 |
| 23 | Mc | otor Rotor Assembly | | | | | | | | | | | | \$0.00 |
| 24 | | Motor Shaft | 1 | US5605045 | 16 | Steel | 3.31 | 20.32 | | | 0.00 | 115.21 | 0.90 | \$10.64 |
| 25 | | Thermal Insulation | 1 | US5605045 | 60 | Teflon | 3.81 | 12.70 | | | 0.25 | 35.49 | 0.07 | \$1.47 |
| 26 | | NdFeB Magnet | 4 | US5605045 | 62 | NdFeB | 4.68 | 12.70 | | | 0.44 | 73.64 | 0.55 | \$48.60 |
| 27 | | Collar | 1 | US5605045 | 70 | Steel | 5.08 | 12.70 | | | 0.20 | 38.92 | 0.30 | \$7.58 |
| | | byrith Seal | 1 | US2006/0153704 | 130 | Misc | 5.31 | | | | 1.00 | | 0.02 | \$2.00 |
| | | unal Foil Bearing otor Housing | 1 | US2006/0153705 DE-FC36-02AL67624 | | Steel | 3.31 20.32 | 5.08 20.32 | | | 0.20 | 432.55 | 0.10 | \$10.00 \$12.26 |
| 31 | IVIC | Bolt | 8 | DE-1-030-02AE07024 | | Misc | 0.60 | 1.20 | | | 0.20 | 2.03 | 0.16 | \$12.20 |
| 31 | _ | Washer | 8 | | | Misc | 1.00 | 0.10 | | | | 2.03 | 0.16 | \$0.40 |
| | | | | | | | | | | | | | | |
| | | otor Stator Assembly otor Sator Position Ring | 1 | FY2000 Progress Report FY2000 Progress Report | | Misc | 9.20 | 12.70 | | | 1.50 | 460.59 | 2.95 | \$17.91 \$0.50 |
| 34 | IVIC | Bolt | 8 | FY2000 Progress Report | - | Misc | 0.60 | 1.20 | 0.00 | 0.00 | 0.00 | 2.03 | 0.16 | \$0.50 |
| 36 | _ | Washer | 8 | FY2000 Progress Report | | Misc | 1.00 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 | \$0.40 |
| | Mc | otor Connector | 1 | · · _ · · · · · · · · · · · · · · · · · | | Misc | | | | | | | | \$0.50 |
| 38 | | byrith Seal | 1 | FY2000 Progress Report | | Misc | 5.31 | | | | | | 0.02 | \$2.00 |
| | | rust Bearing Runner | 1 | FY2000 Progress Report | | Steel | 8.00 | 5.08 | | | 0.50 | 25.00 | 0.20 | \$7.59 |
| | | rust Bearing | 2 | FY2000 Progress Report | 1 | Misc | 8.00 | | | | | | 0.20 | \$20.00 |
| 40 | | rust Bearing Holder | 2 | FY2000 Progress Report | | Steel | 10.00 | 1.00 | | | 0.50 | 50.00 | 0.20 | \$20.00 |
| | | byrith Seal | 1 | · · 2000 i rogicos i tepolit | | Misc | 10.00 | 1.00 | | | 0.00 | 50.00 | 0.00 | \$0.00 |
| | _ | unal Foil Bearing | 1 | US2006/0153705 | | Misc | 3.31 | 5.08 | | | | | 0.10 | \$10.00 |
| | | mpressor Housing | 1 | FY2000 Progress Report | | Al | 25.40 | | | 7.62 | 0.16 | 134.69 | 0.36 | \$5.39 |
| 45 | | Bolt | 8 | FY2000 Progress Report | | Misc | 0.60 | 1.20 | 0.00 | 0.00 | 0.00 | 2.03 | 0.02 | \$0.40 |
| 46 | | Washer | 8 | FY2000 Progress Report | | Misc | 1.00 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | \$0.40 |
| 47 | Co | mpressor Impeller | 1 | FY2000 Progress Report | | Al | 5.00 | 5.00 | | | | | 0.20 | \$20.00 |
| | | mpressor Impeller Tie Rod | 1 | FY2000 Progress Report | | Misc | 1.00 | 10.00 | | | | 7.85 | 0.06 | \$3.91 |
| | | M Mounting Bracket Left | 1 | | | Steel | | 25.40 | 7.62 | | 0.10 | 19.35 | | \$0.00 |
| | | M Mounting Bracket Right | 1 | | | Steel | | 25.40 | 7.62 | 0.00 | 0.10 | 19.35 | | \$0.00 |
| 51 52 | Co | ntrol Box Assembly Box | 1 | DOE target \$40/kW / 5.5kW | Input | | | | | | | | 6.50 | \$402.00 \$0.00 |
| 52 | - | Integrated Motor Cable | 1 | | | | | | | | | | | \$0.00 |
| 54 | - | Inverter | 1 | | | | | | | | | | | \$0.00 |
| 55 | | EMI Section | 1 | | | | | | | | | | | \$0.00 |
| 56 | _ | Wire Harness & Cooling pipes | 1 | | | | | | | | | | | \$0.00 |
| 57 | Fir | nal Assembly | | | | | | | | | | | | \$9.65 |
| | | | | | | | | | | | | | | \$686.73 |
| | | | | | | | | | | | | | | |

