



Hydrogen Storage Engineering

CENTER OF EXCELLENCE

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May 15, 2012

Overview

Timeline

- **Start: February 1, 2009**
- **End: July 31, 2014**
- **55% Complete (as of 3/31/12)**

Budget

- **Total Center Funding:**
 - DOE Share: \$ 36,232,765
 - Contractor Share: \$ 3,591,709
 - FY '11 Funding: \$ 5,144,156
 - FY '12 Funding: \$ 5,930,000
- **Prog. Mgmt. Funding**
 - FY '11: \$ 400,000
 - FY '12: \$ 400,000

Barriers

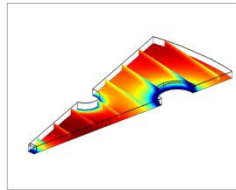
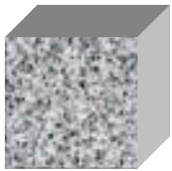
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|-------------------------------|---------------------------------------|
| A. System Weight and Volume | H. Balance of Plant (BOP) Components |
| B. System Cost | J. Thermal Management |
| C. Efficiency | K. System Life-Cycle Assessment |
| D. Durability | O. Hydrogen Boil-Off |
| E. Charging/Discharging Rates | P. Understanding Physi/Chemi-sorption |
| G. Materials of Construction | S. By-Product/Spent Material Removal |

Partners



Why Perform Materials Development and System Engineering in Parallel?

continuous feedback with
system design indicating materials requirements



Materials → Thermal Management → H₂ Storage BoP → Fuel Cell → Vehicle → Wheels



Engineered
Materials
Properties



Heat Transfer
Designs



BoP
Component
Requirements

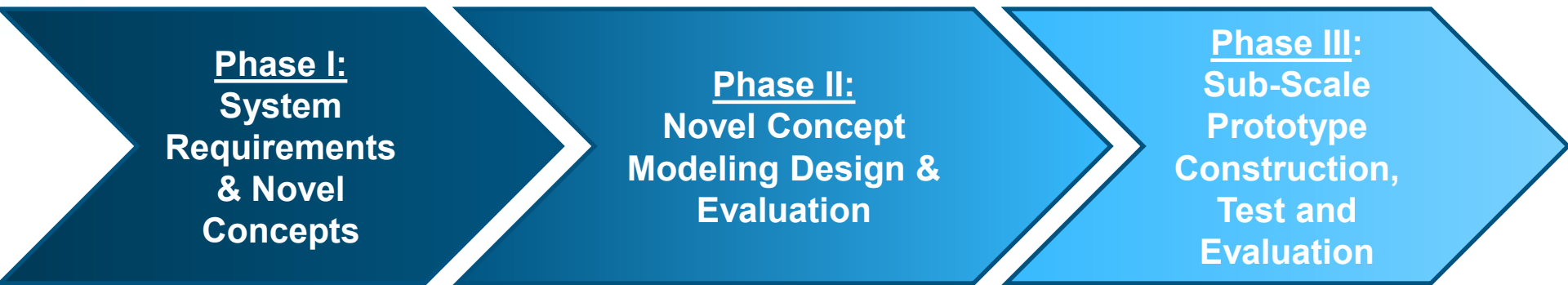


What is Needed
of the Hydrogen Storage
Media & System

HSECoE Objectives

- **Develop materials based hydrogen storage systems for On-Board Hydrogen Storage for Light Duty Vehicles**
 - Develop **system models** that lend insight into overall fuel cycle efficiency.
 - Compile all relevant **materials data** for candidate storage media and define future data requirements.
 - Using systems engineering concepts, **design innovative system architectures** for **metal hydride, chemical, and sorption materials-based storage technologies** with the potential to meet DOE performance and cost targets.
 - Design components and experimental test fixtures to **evaluate the innovative storage devices** and subsystem design concepts, validate model predictions, and improve both component design and predictive capability.
 - Design, fabricate, test, and decommission **subscale prototype systems** of selected materials-based technologies.

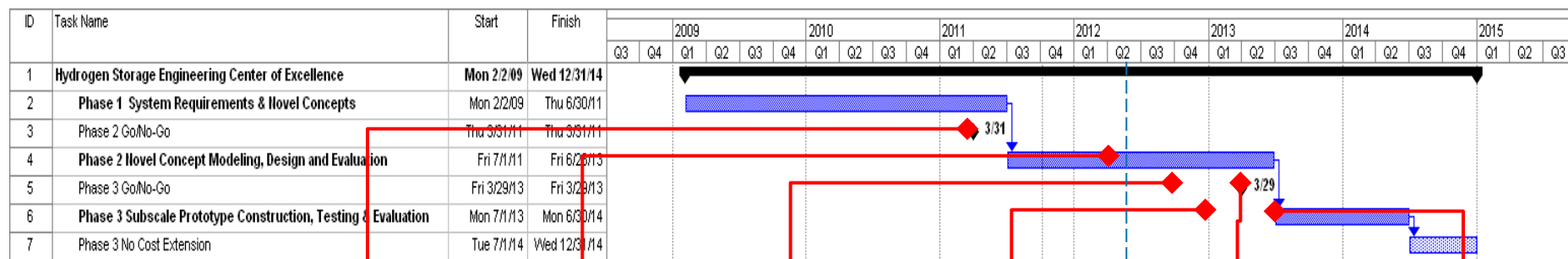
Phased Approach



- **Where are we and where can we get to?**
 - Model development
 - Benchmarking
 - Gap Identification
 - Projecting advances
- **How do we get there (closing the gaps) and how much further can we go?**
 - Component development
 - Concept validation
 - Integration testing
 - System design
- **Put it all together and confirm claims.**
 - System integration
 - System assessments
 - Model validation
 - Gap analysis
 - Performance projections

Important Dates

- Duration: 5.5 years
 - Phase 1 Start: Feb. 1, 2009
 - Phase 1-2 Transition: March 31, 2011
 - Phase 1 End: June 30, 2011
 - Phase 2 Start: July 1, 2011
 - Phase 3 Go/No-Go Determination: **March 31, 2013**
 - *Phase 2 End: **June 30, 2013***
 - Phase 3 Start: **July 1, 2013**
 - Completion Date: June 30, 2014 ⇒ **12/31/14?**



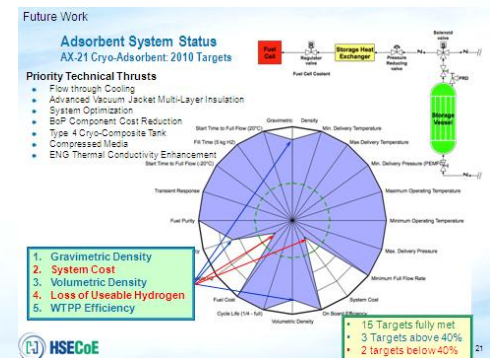
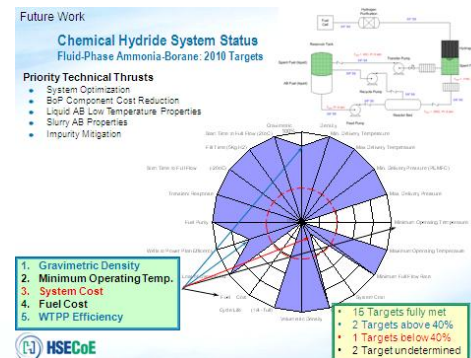
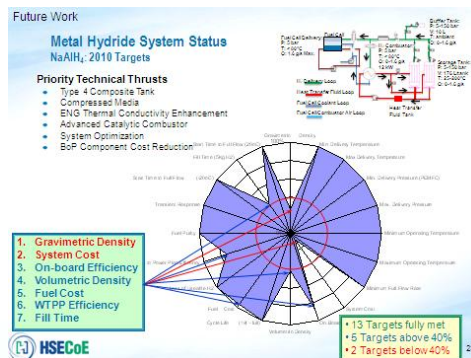
Phase 1-2 Transition **Materials Selection** **System Selection** **Design Subscale Prototypes** **Go/NoGo Decision** **Building Subscale Prototypes**

Phase 1-2 Transition

Overviewed Integrated System Model and its Role in Target Achievement

Prepared Summaries of Status for Metal Hydride, Chemical Hydride and Adsorbent Systems

- Current status vs targets
- Identification of critical **technical barriers**
- Identification of potential **solutions to barriers**
- Summary of projected system performance vs targets



Outcomes of Phase 1-2 Transition

- **Continued Work**

Adsorbent-Based Hydrogen Storage Systems

- Increasing compaction of the sorbent materials
- Demonstration of improved thermal conduction within the sorbent
- Thermal isolation of the inner storage bed.
- Flow through cooling designs must be accompanied with total cooling requirements

Liquid-Phase Chemical Hydrogen Storage Materials (including liquids, solutions and/or slurries)

- Development and validation of the critical components for baseline ammonia borane solutions
 - Thermal management within the reaction chamber,
 - Gas-liquid phase separations, and the
 - Hydrogen purification train be emphasized for the baseline ammonia borane solutions.
- Endothermic release material (e.g., AlH_3 , alane) must be modeled

Outcomes of Phase 1-2 Transition

- **Discontinued Work**

Solid-Phase Chemical Hydrogen Storage Materials

- Material transport becomes a major challenge for this class of material.
- A reliable process for loading/unloading solids from the onboard storage vessel, nor transporting it through an onboard reactor, have been identified.

Work on Reversible Metal Hydrides

- Analyses for highly optimized vessel configurations that could adequately manage thermal and mass flow rates needed for reversible onboard hydrogen storage to meet the DOE performance targets imposed requirements **substantially exceeding the properties and behavior of any single, currently existing candidate hydride.**
- The necessary combination of gravimetric and volumetric capacities, reaction kinetics, thermodynamics properties, and reversibility have not been found simultaneously in any hydride investigated to date.
- Novel engineering solutions that will allow any currently known hydride, when incorporated into a complete system, have not been identified.

HSECoE Phase 3 Go/NoGo Milestones

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Phase 2 System Status

| Chemical Hydrides | | 2015 DOE Goal (System) | 3/31/2011 | | | 3/31/2013 | | |
|---------------------------------|--------------------|----------------------------|------------------------------------|------------------------------------|---------------------------------------|-----------------------------------|-----------------------------------|---------------------------------|
| | | | Phase 1 HSECoE Baseline (Material) | Phase 1 HSECoE Baseline (BOP only) | Phase 1 HSECoE Baseline (System) | Phase 2 HSECoE Targets (Material) | Phase 2 HSECoE Targets (BOP only) | Phase 2 HSECoE Targets (System) |
| Target | Units | | | | | | | |
| Gravimetric Capacity | kg H2/kg system | 0.055 | 0.076 | 0.092 | 0.042 | 0.076 | 0.109 | 0.045 |
| <i>mass</i> | <i>liters</i> | 102 | | | 133 | | | 124 |
| Volumetric Capacity | kg H2/L system | 0.04 | 0.074 | 0.077 | 0.039 | 0.074 | 0.102 | 0.043 |
| <i>volume</i> | <i>kg</i> | 140 | | | 144 | | | 130 |
| System Cost * | \$/kWh net | 6 | | 25.6 | 25.6 | | 25.6 | 25.6 |
| | \$ | 480 | | | | | | |
| Fuel Cost | \$/gge at pump | 2.6 | | | ? | | | 4.5 |
| Min Operating Temp | °C | -40 | | | ? | | | 0 |
| Max Operating Temp | °C | 60 | | | 50 | | | 50 |
| Min Delivery Temp | °C | -40 | | | -40 | | | -40 |
| Max Delivery Temp | °C | 85 | | | 85 | | | 85 |
| Cycle Life | cycles | 1500 | | | 1000 | | | 1000 |
| Min Delivery Pressure | bar | 5 | | | 5 | | | 5 |
| Max Delivery Pressure | bar | 12 | | | 12 | | | 12 |
| Onboard Efficiency | % | 90 | | | 97 | | | 97 |
| Well to Power Plant Efficiency | % | 60 | | | 37 | | | 37 |
| System Fill Time | min | 3.3 | | | 2.7 | | | 2.7 |
| Min Full Flow Rate | (g/s/kW) | 0.02 | | | 0.02 | | | 0.02 |
| | <i>g/s</i> | 1.6 | | | 1.6 | | | 1.6 |
| Start Time to Full Flow (20°C) | sec | 5 | | | 1 | | | 1 |
| Start Time to Full Flow (-20°C) | sec | 15 | | | 1 | | | 1 |
| Transient Response | sec | 0.75 | | | 0.49 | | | 0.49 |
| Fuel Purity | %H2 | 99.97 | | | 99.97 | | | 99.99 |
| Permeation, Toxicity, Safety | Sec/h | Meets or Exceeds Standards | | | s | | | s |
| Loss of Useable Hydrogen | (g/h)/kg H2 stored | 0.05 | | | 0.1 | | | 0.1 |
| System Designing Specifics | | | | | | | | |
| LANL, PNNL, SRNL | Media | | Liquid AB at 50wt% Bladder Tank | | Liquid AB at 65wt% Bladder Tank | | | |
| PNNL | Tank | | Flow Through Reactor | | Flow Through Reactor | | | |
| LANL | Reactor | | | | | | | |
| PNNL | System Design | | | | | | | |
| | BoP | | | | | | | |
| PNNL | Pumps | | Feed/Recycle/Transfer Pumps | | Feed/Recycle/Transfer Pumps | | | |
| UTRC | Heat Exchanger | | | | Heat Exchanger mass and volume cut | | | |
| UTRC | GLS | | Gas/Liquid Separator | | Gas/Liquid Separator | | | |
| UTRC | Purification | | Purification | | Hydrogen Purification mass and volume | | | |

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Phase 2 System Status

| Adsorbants | | 2017 DOE Goal (System) | 3/31/2011 | | | 3/31/2013 | | |
|---------------------------------|--------------------|----------------------------|------------------------------------|------------------------------------|---------------------------------------|-----------------------------------|-----------------------------------|---------------------------------|
| | | | Phase 1 HSECoE Baseline (Material) | Phase 1 HSECoE Baseline (BOP only) | Phase 1 HSECoE Baseline (System) | Phase 2 HSECoE Targets (Material) | Phase 2 HSECoE Targets (BOP only) | Phase 2 HSECoE Targets (System) |
| Target | Units | | | | | | | |
| Gravimetric Capacity | kg H2/kg system | 0.055 | 0.15 | 0.05 | 0.038 | 0.15 | 0.05 | 0.045 |
| <i>mass</i> | <i>kg</i> | 102 | | | 147 | | | 124 |
| Volumetric Capacity | kg H2/L system | 0.04 | 0.042 | 0.043 | 0.022 | 0.045 | 0.074 | 0.028 |
| <i>Volumetric</i> | <i>liters</i> | 140 | | | 255 | | | 200 |
| System Cost | \$/kWh net | 6 | 3.5 | 15.0 | 18.5 | 3.5 | 10.3 | 13.8 |
| | \$ | 1,119 | | | 3,450 | | | 2,573 |
| Fuel Cost | \$/gge at pump | 2.6 | | | 4.89 | | | 4.89 |
| Min Operating Temp | °C | -40 | | | -30 | | | -40 |
| Max Operating Temp | °C | 60 | | | 50 | | | 60 |
| Min Delivery Temp | °C | -40 | | | -40 | | | -40 |
| Max Delivery Temp | °C | 85 | | | 85 | | | 85 |
| Cycle Life | Cycles | 1500 | | | 1000 | | | 1500 |
| Min Delivery Pressure | bar | 5 | | | 5 | | | 5 |
| Max Delivery Pressure | bar | 12 | | | 12 | | | 12 |
| Onboard Efficiency | % | 90 | | | 96 | | | 92 |
| Well to Power Plant Efficiency | % | 60 | | | 40.1 | | | 40.1 |
| System Fill Time | min | 3.3 | | | 3.3 | | | 3.3 |
| Min Full Flow Rate | (g/s/kW) | 0.02 | | | 0.02 | | | 0.02 |
| | <i>g/s</i> | 1.6 | | | 1.6 | | | 1.6 |
| Start Time to Full Flow (20°C) | sec | 5 | | | 5 | | | 5 |
| Start Time to Full Flow (-20°C) | sec | 15 | | | 15 | | | 15 |
| Transient Response | sec | 0.75 | | | 0.75 | | | 0.75 |
| Fuel Purity | %H2 | 99.97 | | | 99.97 | | | 99.99 |
| Permeation, Toxicity, Safety | Sec/h | Meets or Exceeds Standards | | | s | | | s |
| Loss of Useable Hydrogen | (g/h)/kg H2 stored | 0.05 | | | 0.44 | | | 0.44 |
| System Designing Specifics | | | | | | | | |
| JPL | Insulation | | MLVJ Insulation | | MLVJ Insulation | | | |
| LC | Tank | | Type III 200 bar tank | | Type IV 150 bar tank | | | |
| Ford | Media | | Uncompacted Super Activated Carbon | | Compacted MOF-5 w/ density 0.3 | | | |
| SRNL, GM | Internal HX | | Flow through Cooling | | Flow through Cooling | | | |
| SRNL, OSU | External HX | | PEMFC Fluid Coupled HX Loop | | PEMFC Fluid Coupled HX Loop | | | |
| | Initial Conditions | | | | Initial conditions: 140 bar, 80 K | | | |
| | H2 input | | | | Final/Refill conditions: ~3 bar, ~160 | | | |

Phase 2 Gantt Chart

| Phase 2 Plan | | | | | | | | | | | | | | | |
|------------------|----------------|------------------|-----------------|---------|-----------------|--|-------|-------|----|----|----|-------|----|----|----|
| Adsorbent System | | | | | | | | | | | | | | | |
| Center Task # | Partner Task # | Lead Institution | Partner | Partner | Technology Area | Task Description and Objective(s) | FY 11 | FY 12 | | | | FY 13 | | | |
| | | | | | | | Q4 | Q1 | Q2 | Q3 | Q4 | Q1 | Q2 | Q3 | Q4 |
| | | | | | | Determine out-gassing rate and species for carbon fiber coupons at elevated, room, and cryogenic | | | | | | | | | |
| Lead Institution | Partner | Partner | Technology Area | | | Evolution of temperatures | | | | | | | | | |
| | | | | | | Contributions of radiative and conductive heat transfer, and | | | | | | | | | |
| | | | | | | Models | | | | | | | | | |
| | | | | | | Coordination with experimental results | | | | | | | | | |
| | | | | | | Level | | | | | | | | | |
| JPL | Lincoln | | ET | | Determine | Evolution of temperatures | | | | | | | | | |
| PNNL | Lincoln | JPL | ET | | Complete | Carbon-based composites consisting of varying amounts of ENG | | | | | | | | | |
| | | | | | | and make available to partners in the center. | | | | | | | | | |
| JPL | PNNL | | ET | | Calibration | Assure permeability at low T | | | | | | | | | |
| | | | | | | Stiffness of SAC composite pellets | | | | | | | | | |
| 15 | 2 | GM | | | MOR | Optimize and model chemistry for best volumetric density with minimal adverse impact on gravimetric adsorption and kinetics; determine pellet D-A parameters | | | | | | | | | |
| 16 | 1 | NREL | | | MOR | Evaluate differences in engineering properties of alternate sorbents such as PEEK with optimized pore sizes that enable higher bulk densities and volumetric capacities. Provide comparative evaluations to base materials like AX-21 and MOF-5. | | | | | | | | | |
| 17 | 4 | NREL | | | MOR | Provide HSECoE appropriate engineering properties on recommended adsorbent materials for future H2 storage system analysis | | | | | | | | | |
| 18 | 7 | OSU | SRNL | | PACM | Alternative System Configuration and Modeling | | | | | | | | | |

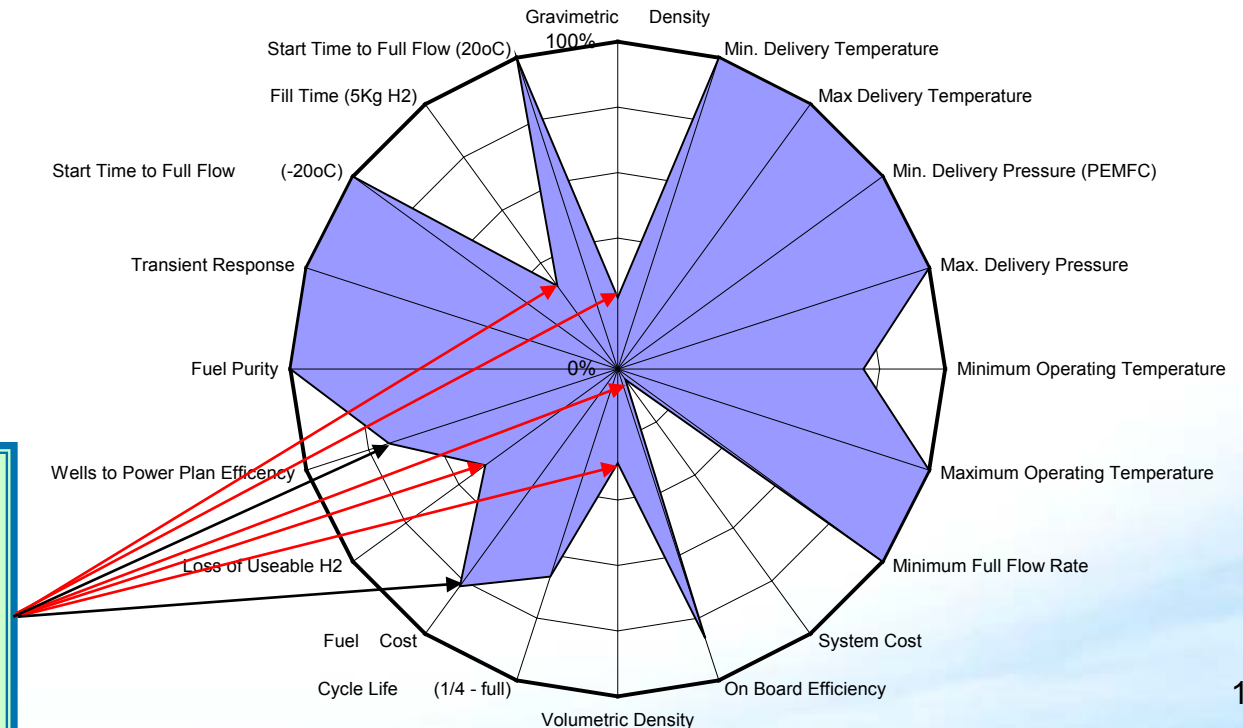
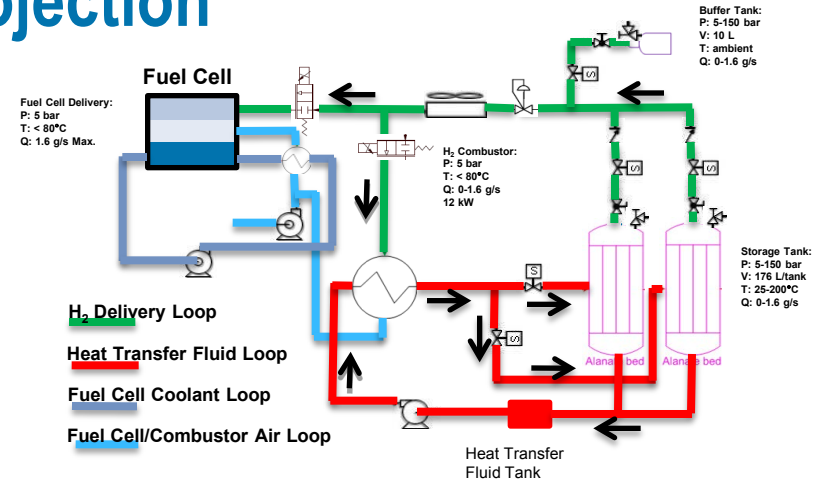
| Task Description and Objective(s) | | | | | | | | | |
|---|--|--|--|--|--|--|--|--|--|
| | | | | | | | | | |
| Determine out-gassing rate and species for carbon fiber coupons at elevated, room, and cryogenic temperatures. | | | | | | | | | |
| Complete materials testing of liner and composite at cryogenic temperatures | | | | | | | | | |
| Calibrate parasitics model, confirm the relative contributions of radiative and conductive heat transfer, and address ways of reducing the most significant parasitics. | | | | | | | | | |

| | | | | | | | | | | | | | | | | |
|----|---|------|---------|------|------|--|--|--|--|--|--|--|--|--|--|--|
| 33 | 6 | SRNL | UQTR | Ford | MOR | Characterize adsorption isotherms of MOF-5 at 3 temperatures and confirm DA parameters | | | | | | | | | | |
| 34 | 3 | NREL | | | PACM | Perform efficiency analysis and report rank order results of WPP efficiency and GHG emission for each storage system design being evaluated. | | | | | | | | | | |
| 35 | 8 | SRNL | UQTR | | TP | Complete low temperature adsorbent tests, modify test bench, to accommodate flow through, cooling, and construct flow through cooling models. Establish viability of flow-through cooling. | | | | | | | | | | |
| 36 | 3 | OSU | | | TP | Design and Test subscale stainless steel Multi Storage Module with flow-through cooling. | | | | | | | | | | |
| 37 | 5 | OSU | | | TP | Design, fabricate and evaluate scale-up single module out of either the system operating pressure between 200 and 300 Bar. | | | | | | | | | | |
| 38 | 3 | JPL | Lincoln | | ET | Perform cryogenic burst test for 200 bar Type IV carbon-fiber vessel material properties present any unknown issues. | | | | | | | | | | |
| 39 | 8 | JPL | | | ET | Downstream H2 HX development and testing. Construct and test an conditioner to verify hydrogen and coupling fluid temperatures, heat transfer. | | | | | | | | | | |
| 40 | 5 | JPL | | | ET | Perform mechanical testing of thermal stand-offs. | | | | | | | | | | |
| 41 | 5 | SRNL | UQTR | | MOR | Characterize structural properties, adsorption capacities, modified conduct advanced flow-through cooling experiments using various orientations. Validate models; tune and incorporate necessary physical properties. | | | | | | | | | | |
| 42 | 9 | SRNL | UQTR | | TP | Experimental validation of flow-through cooling concept for H2 cryogenic pellet bed. | | | | | | | | | | |
| 43 | 5 | GM | | | TP | Mid-scale dormancy test. Using a geometrically similar tank configuration transfer in a tank. | | | | | | | | | | |
| 44 | 6 | JPL | Lincoln | | ET | Deliver particulate mitigation filter | | | | | | | | | | |
| 45 | 4 | UTRC | | | ET | Determine cyclic stability of MOF-5 pellets. | | | | | | | | | | |
| 46 | 4 | Ford | UM | BASF | MOR | Desorption strategy validation experiments for powder and pellet beds: (a) Hot gas recirculation (b) Embedded electrical heater | | | | | | | | | | |
| 47 | 6 | GM | | | TP | Mid-scale permeability test. Using a subscale tank of the same type as above, assess tank-scale permeability. | | | | | | | | | | |
| 48 | 7 | JPL | Lincoln | | ET | | | | | | | | | | | |

P1/2 Metal Hydride System Projection

2017 Targets

- Dual Vessel Sodium Alanate Design (w. 4 mol%TiCl₃ & 5 wt% ENG)
- GM1 Design: fin and tube heat exchanger optimized to meet 10.5 min refueling time at the expense of wt %
- 2 Type 3 composite tanks with SS liners
- System includes a 10 l buffer tank and a 12 kW H₂ combustor

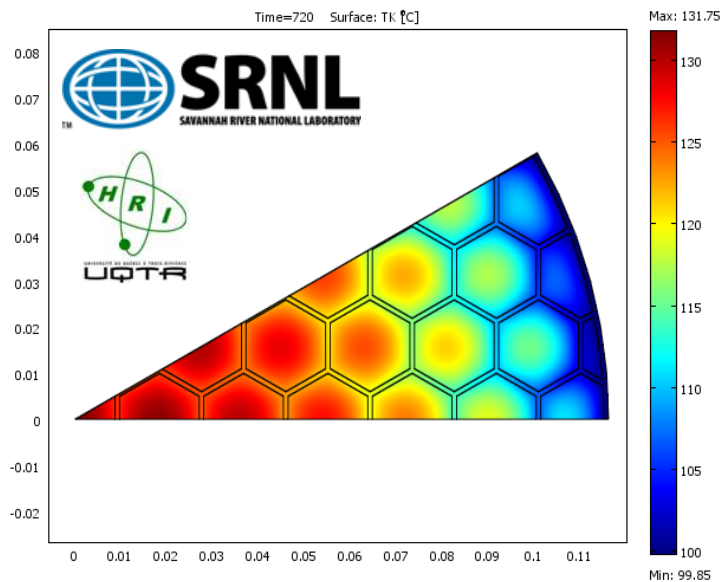


1. Gravimetric Density
2. System Cost
3. Onboard Efficiency
4. Volumetric Density
5. Fill Time
6. Fuel Cost

MH Barriers and Approaches

● Gravimetric & Volumetric Density

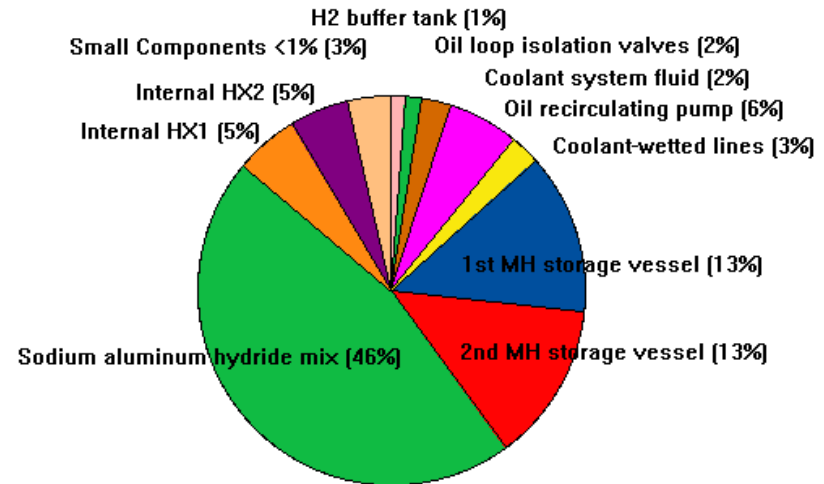
- New materials discovery
- Improved Tank Design
- Low mass BoP Components
- Improved Internal HX
 - Media Thermal Conductivity
 - Internal HX Design



Improved Internal HX Concept

MH System Gravimetric BOP

System mass 457.5 kg



NaAlH₄ systems



as-milled



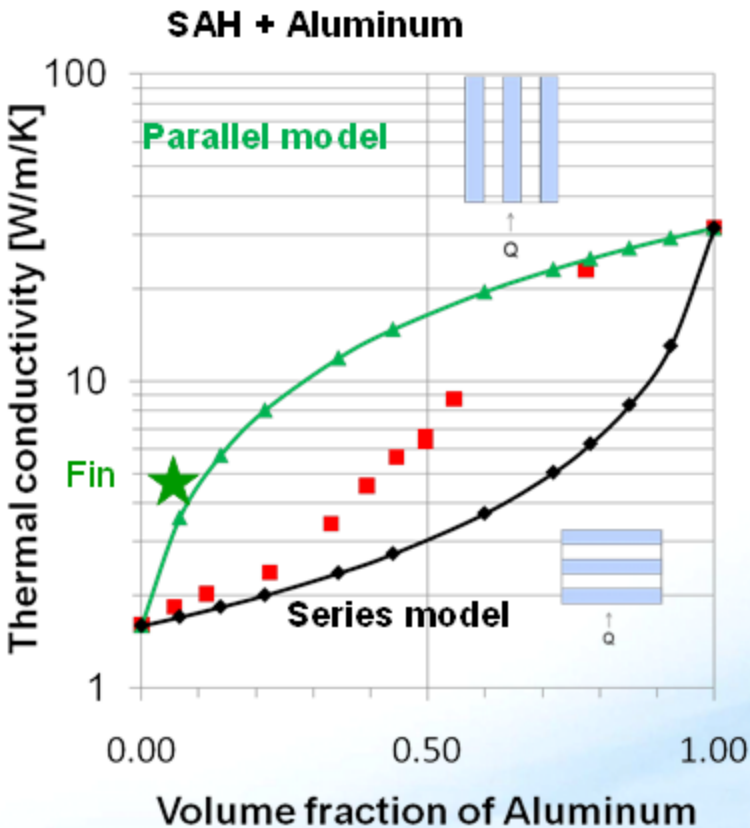
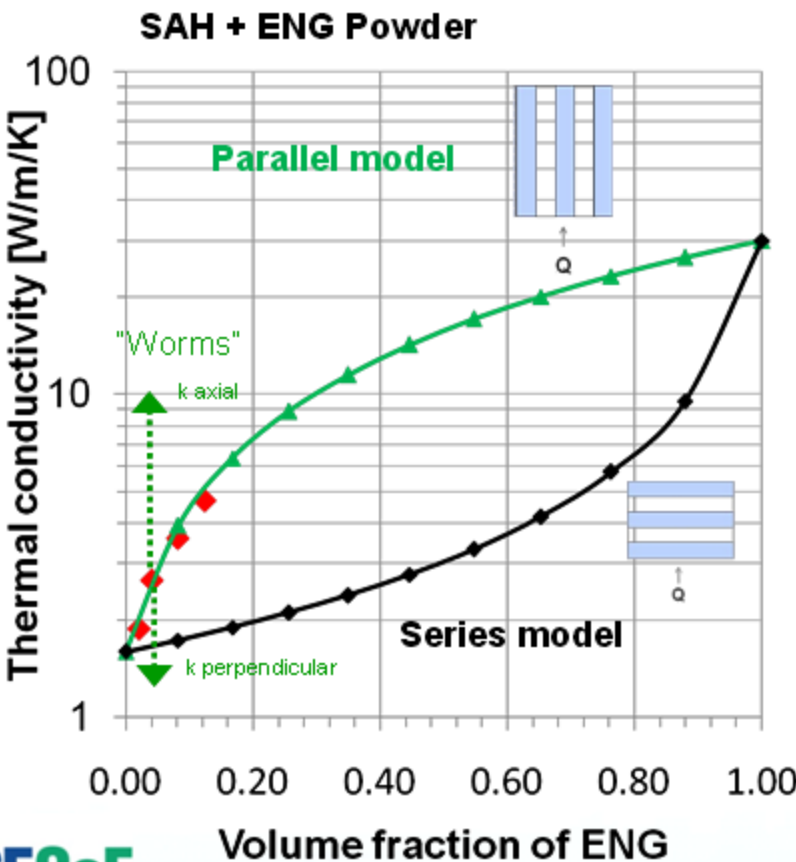
discharged

Compacted Media

MH Barriers and Approaches

- **Fill Time**

- Improved Internal HX
- Enhanced Media Thermal Conductivity

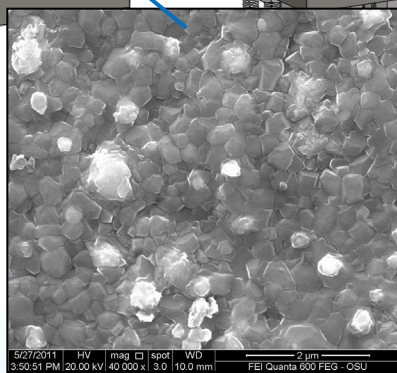
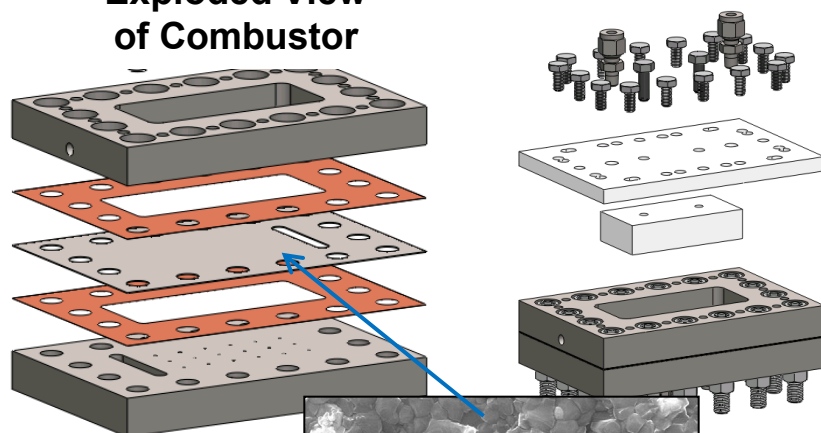


MH Barriers and Approach

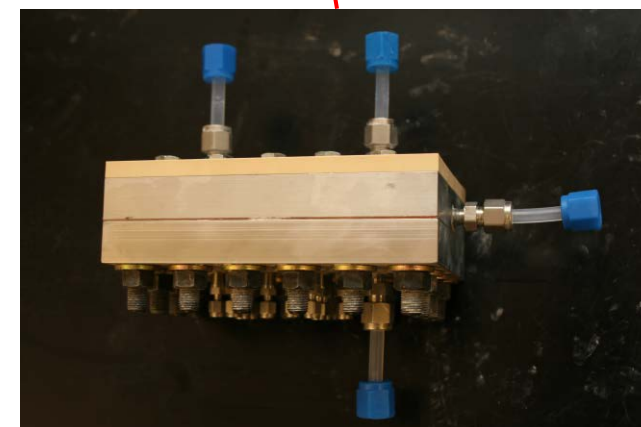
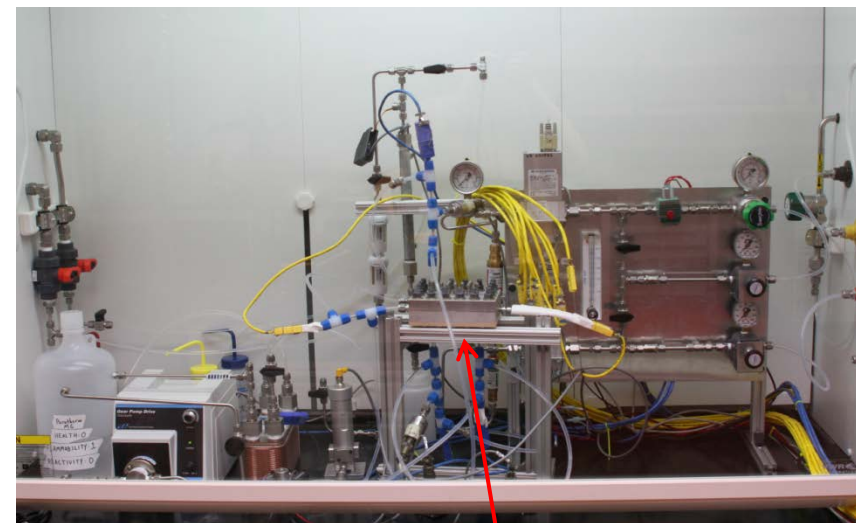
- **On Board Efficiency**
 - Improved Catalytic Combustor

Microchannel Catalytic Combustor >96% Efficiency

Exploded View
of Combustor



Wet Deposited Pt
Catalyst



Assembled Experimental Facility

V. Narayanan, D. Haley, M. Ghazvini & K.
Drost

Metal Hydride System 1: Use Waste Heat Only

Attributes

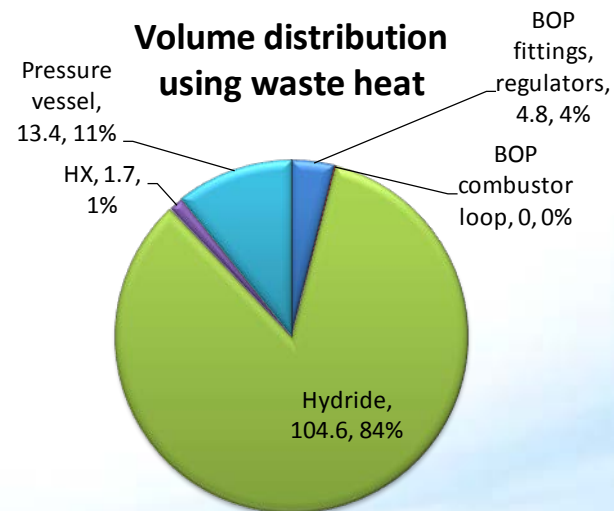
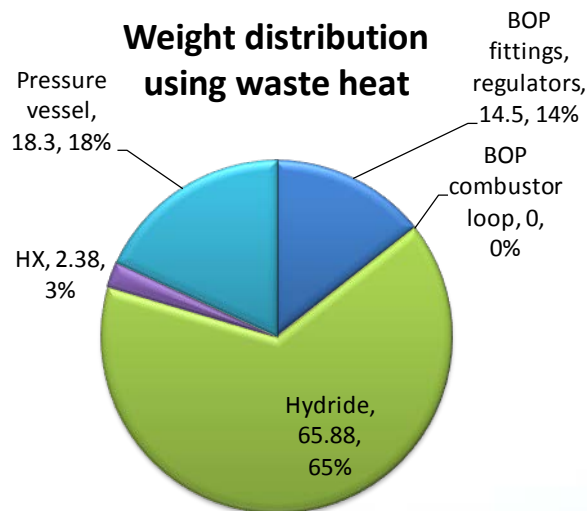
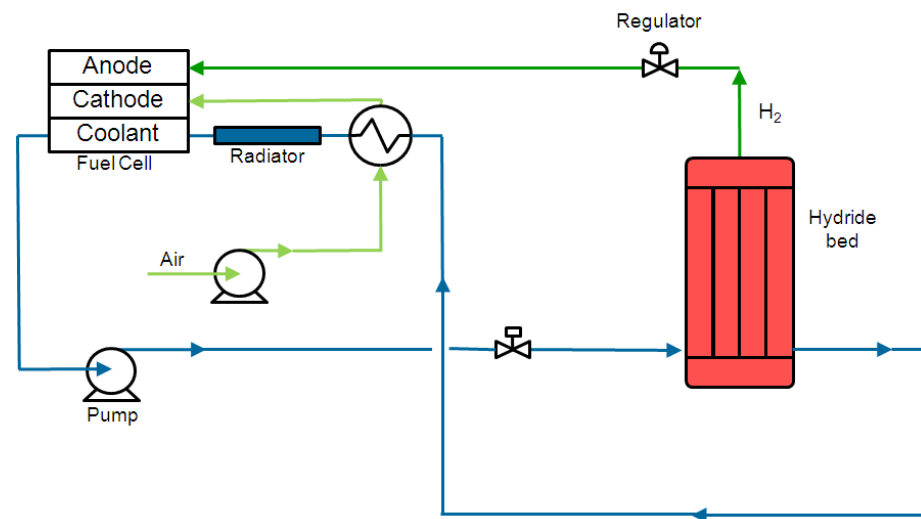
- Very simple system.
- Fuel cell waste heat stream used
- No separate buffer tank: use H_2 in pores.

Media Characteristics

- $\Delta H = 27 \text{ kJ/mol-}H_2$ ($T_{5 \text{ bar}} = 20.7 \text{ }^\circ\text{C}$)
- 11 wt.% material capacity

Results

- Satisfies all targets.
- On-board efficiency: ~100%
- System: 101 kg, 124 liters



Metal Hydride System 2: Combust Some H₂

Attributes

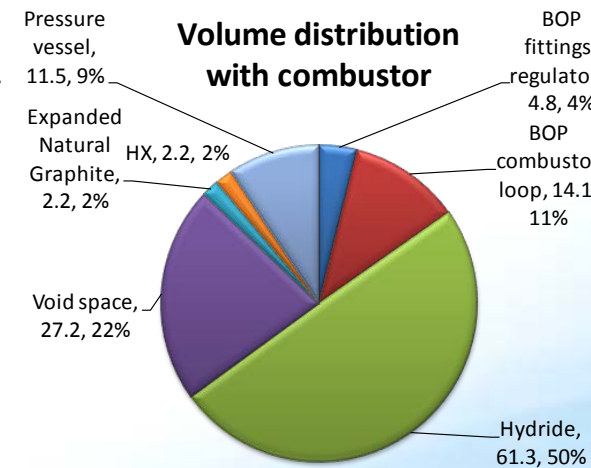
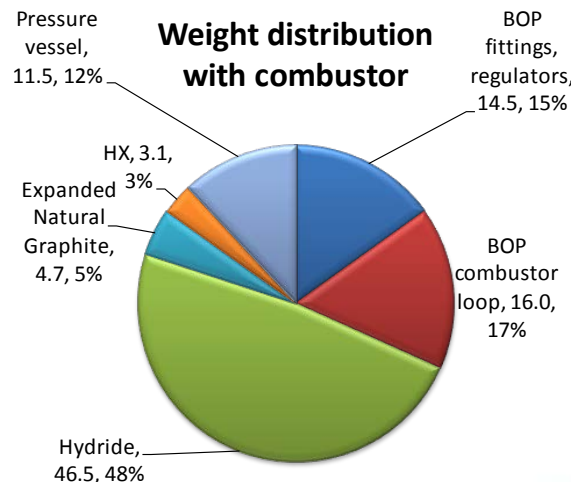
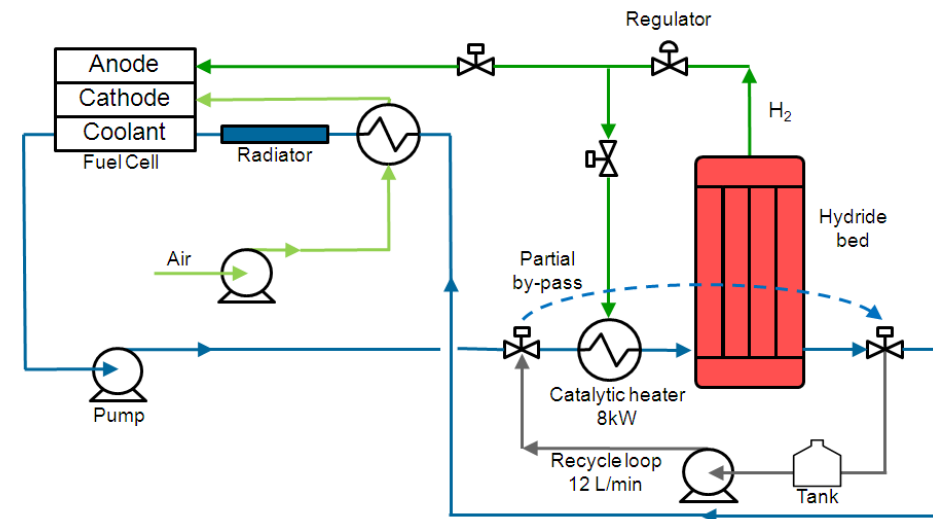
- Mix of fuel cell coolant and recycled fluid used for warm-up and to maintain T_{tank} .
- No separate buffer tank: use H₂ in pores.

Media Characteristics

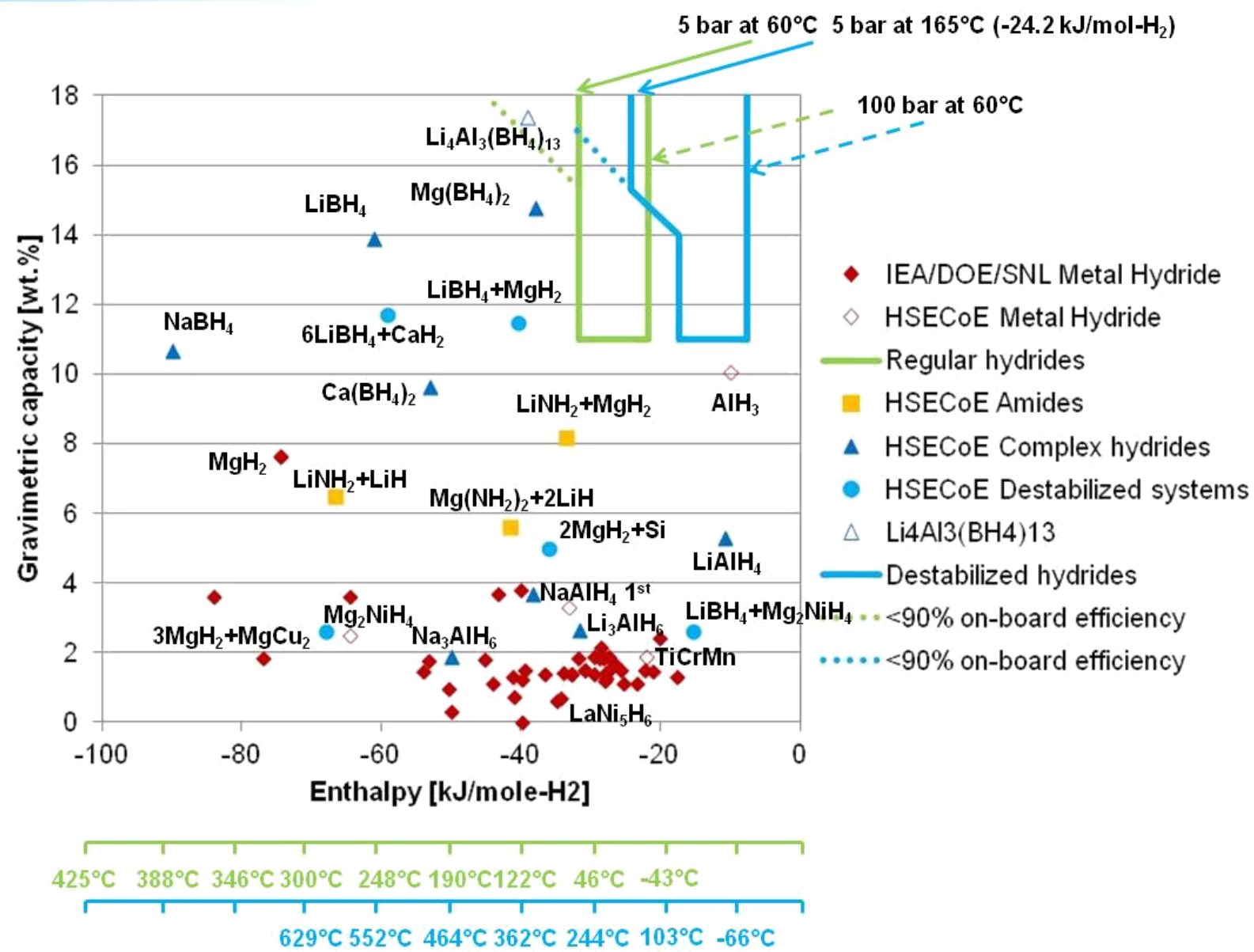
- $\Delta H = -40 \text{ kJ/mol-H}_2$ ($T_{5 \text{ bar}} = 122.8 \text{ }^\circ\text{C}$)
- 17 wt.% pure material capacity

Results

- Satisfies all targets except on-board system efficiency.
- On-board efficiency: ~81%
- System: 103 kg, 126 liters
- Operating at 130°C delivers 5.4 kg-H₂ (delivered + combusted: 6.6 kg-H₂)



Gravimetric Capacity vs. Enthalpy



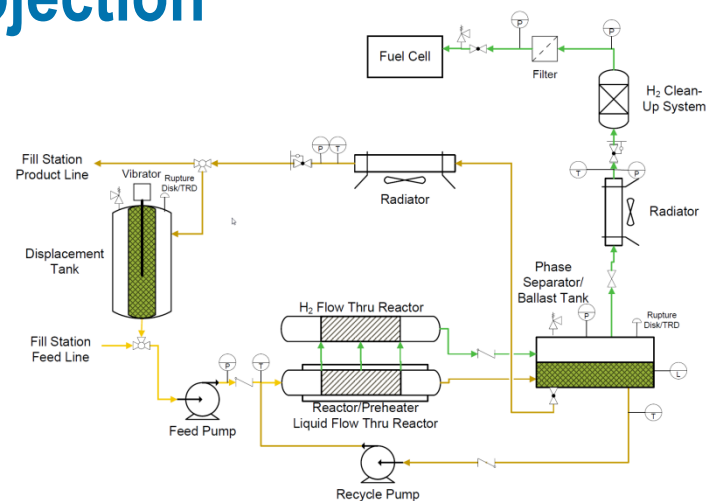
MH System Conclusions

- A material will need reasonably **fast charging kinetics** (3-8X better than SAH), at moderate pressures (< 100 bar).
- Any additional hydrogen capacity (1 to 1.5 wt%) gained by using higher pressure, **hybrid tanks** would be negated by the additional weight associated with the additional carbon fiber needed to reinforce the tank walls.
- For many material densities (>800 kg/m³) – the volumetric target can be easily met if the gravimetric target is met
- A minimum material H₂ capacity to meet the DOE 2017 Targets is **10 to 11 w/o** (with no hydrogen combusted i.e. **$\Delta H < 27$ kJ/mol-H₂**).
- For materials with a higher ΔH (some H₂ combustion required i.e. **$\Delta H > 30$ kJ/mol-H₂**) a minimum material capacity would need to be **15 to 16 w/o**.

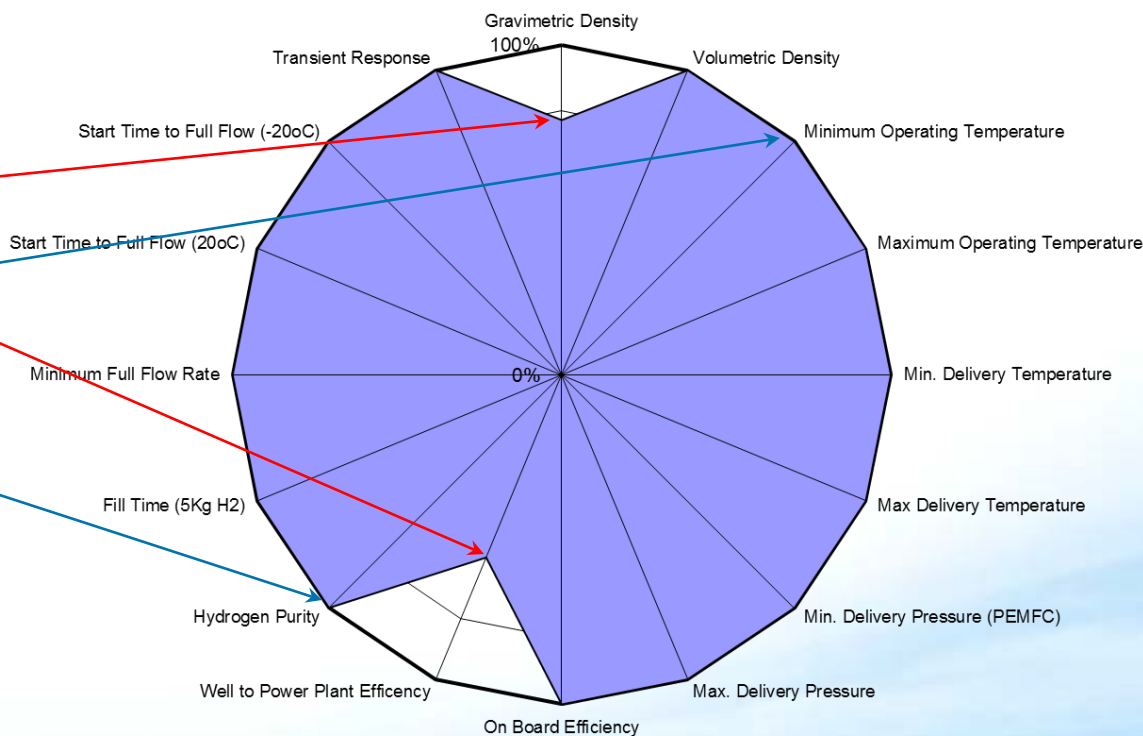
Chemical Hydride System Projection

2017 Targets

- **Media Type: Fluid Phase Ammonia Borane**
- **Composition: 50wt.% AB in BMIMCl**
(1-n-butyl-3-methylimidazolium chloride)
- **Products: Similar rheological properties to reactants**



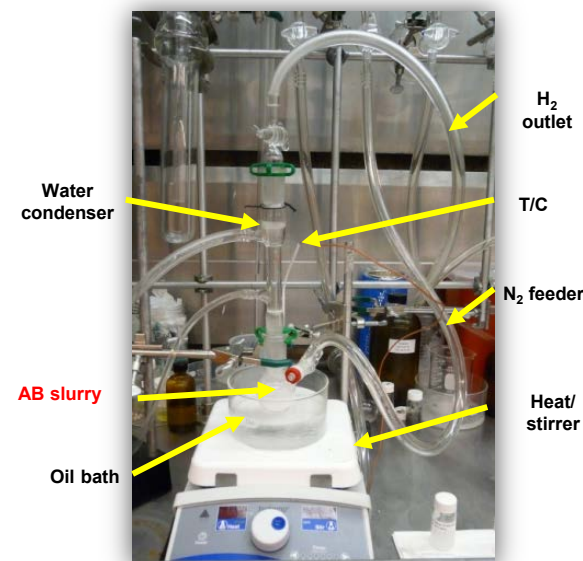
1. Gravimetric Density
2. On-Board Efficiency
3. Min. Op. Temperature?
4. Fuel Cost
5. System Cost
6. H₂ Purity ?



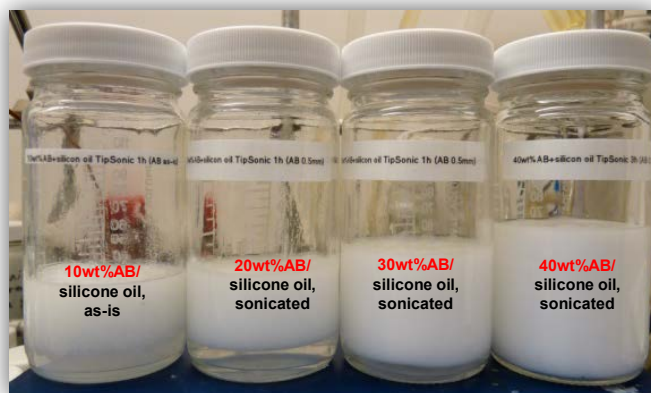
Chemical Hydride Barriers and Approaches

- **Gravimetric Density**
 - Improved Solvent/Slurry to Achieve Higher Density Loading
- **Minimum Operating Temperature**
 - Identify Viscosity vs. Temperature
- **System Cost**
 - Low Cost Solvent/Slurry

Slurry AB Kinetics Measurement



Slurry AB Development



Slurry AB Viscosity Measurement



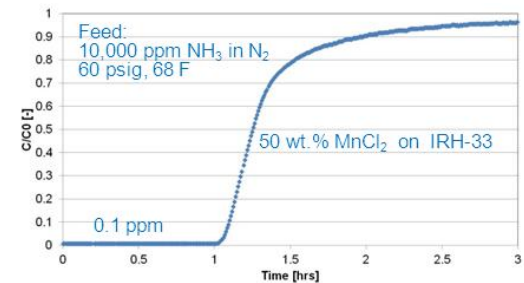
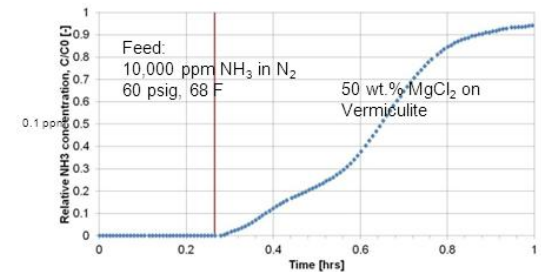
Chemical Hydride Barriers and Approaches

● Hydrogen Purity

- Improved Solvent/Slurry
- Improved Chemical Trapping
- Good Thermal Control

Impurities Trap Development

Metal Chloride on Porous Supports

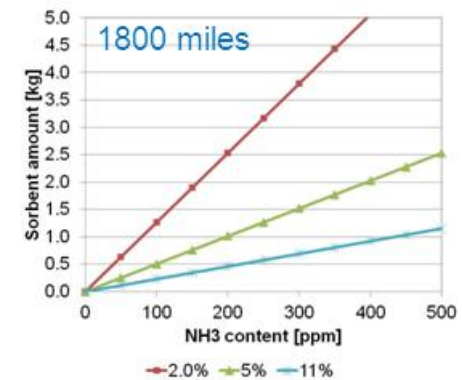


Activated Carbon



Vermiculite

NH₃ Filter Weight



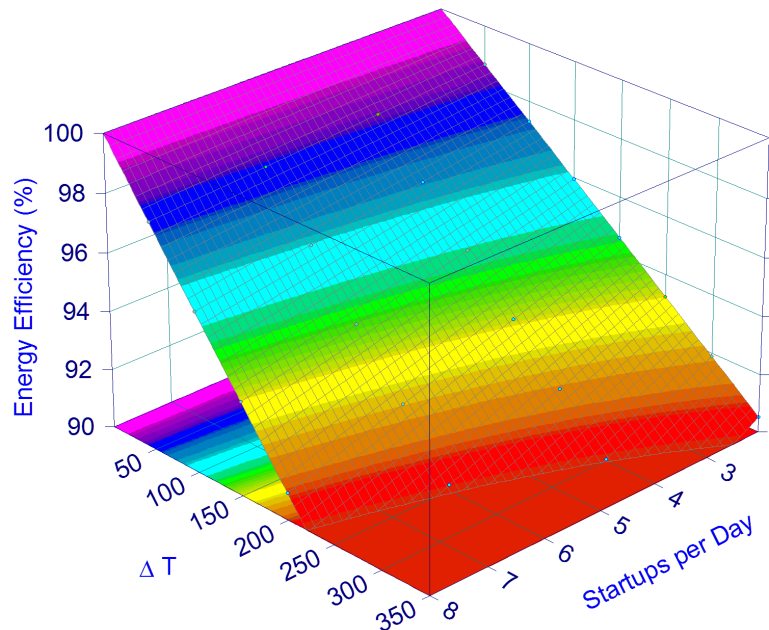
NH₃ filter: 1.2 kg, 1.6 Liter

Chemical Hydride Barriers and Approaches

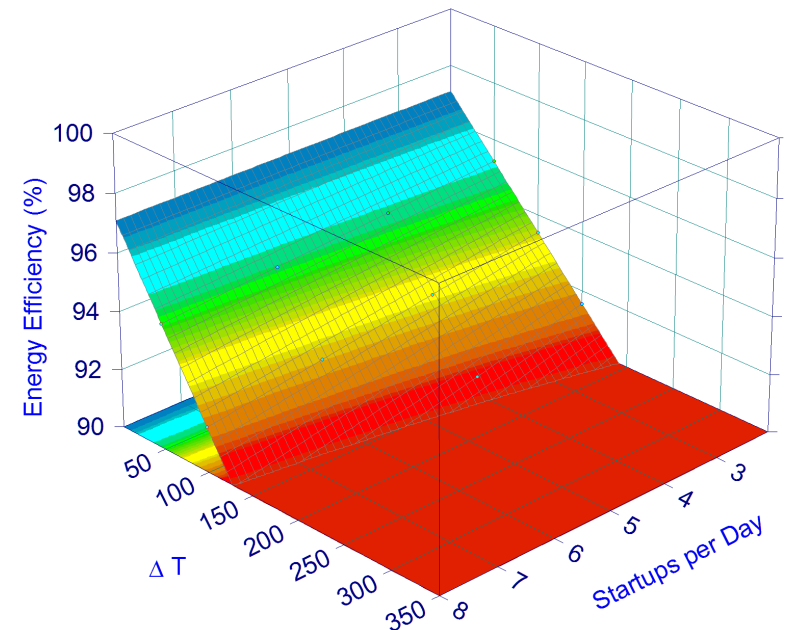
- **On-Board Efficiency**
 - Endothermic vs. Exothermic
 - Daily Utilization



AB Energy Efficiency Calculations as a Function of the Number of Startups and Delta T for a SS Reactor Mass of 5 kg (Total Mass of H₂ = 5.6kg)
Includes Energy for Reactor Startup and Energy to Heat Fluid



Alane Energy Efficiency Calculations as a Function of the Number of Startups and Delta T for a SS Reactor Mass of 5 kg (Total Mass of H₂ = 5.6kg)
Includes Energy for Reactor Startup, Energy to Heat Fluid and ΔH_{rxn}



Chemical Hydride Component Flow Through Reactor Validation Experiments

Fluid AB Flow Through Reactors & Test Facility

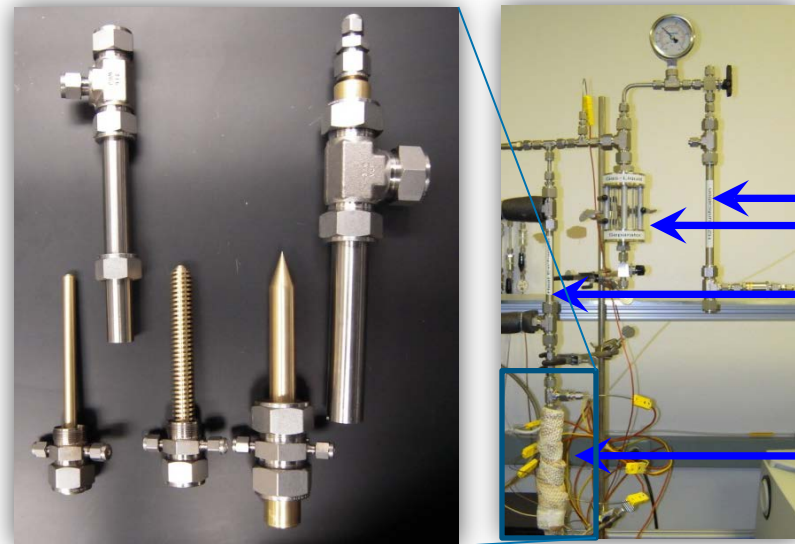


H₂
Purification

Gas-
Liquid
Separator

Heat
Exchanger

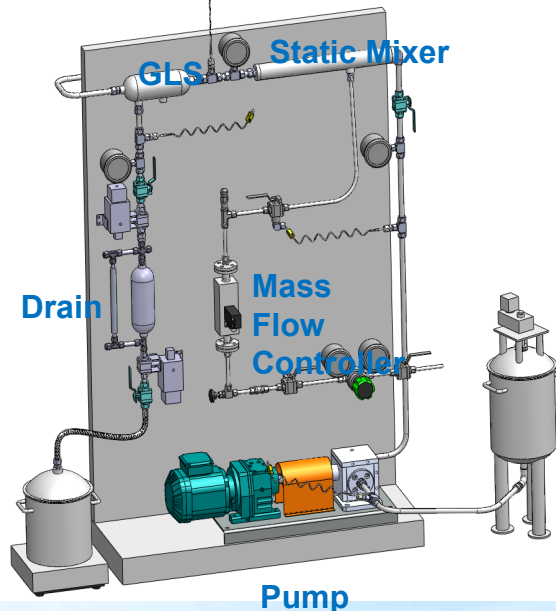
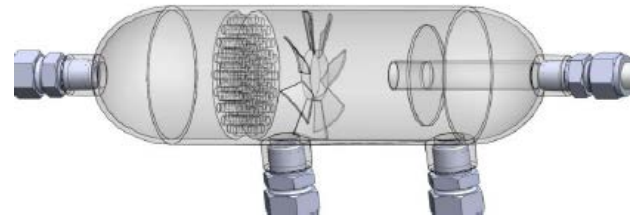
Reactor



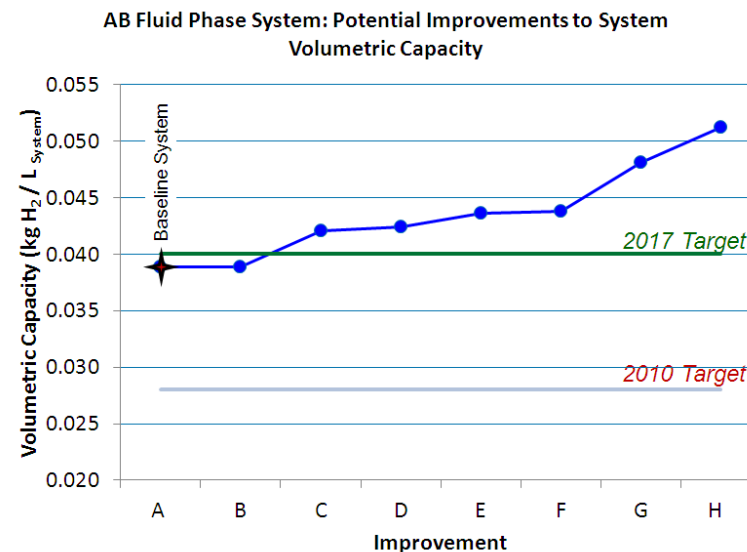
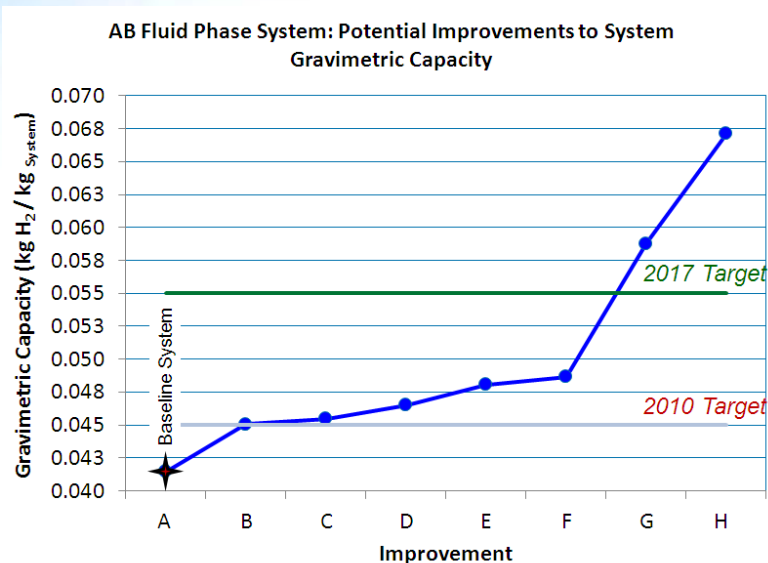
Gas/Liquid Separator Test Facility



Gas/Liquid Separator



CH Projections of Progress

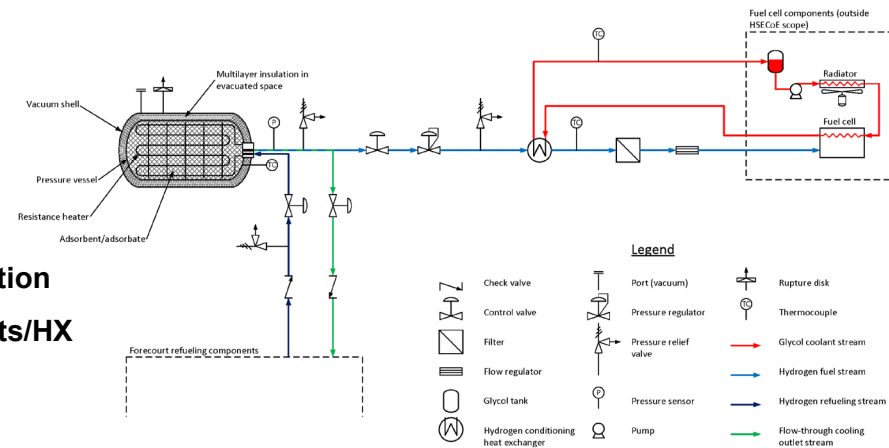


| Step | Description |
|------|--|
| A | Phase 1 Baseline: 50:50 Fluid composition |
| B | Change from steel shell ballast tank to aluminum |
| C | Reduce HX from 76 kW to 38 kW |
| D | Reduce H ₂ Wetted Tubing |
| E | Low Mass Borazine Scrubber |
| F | Low Mass Ammonia Scrubber |
| G | Increase AB loading from 50 to 65 wt. % |
| H | Increase AB loading from 65 to 80 wt. % |

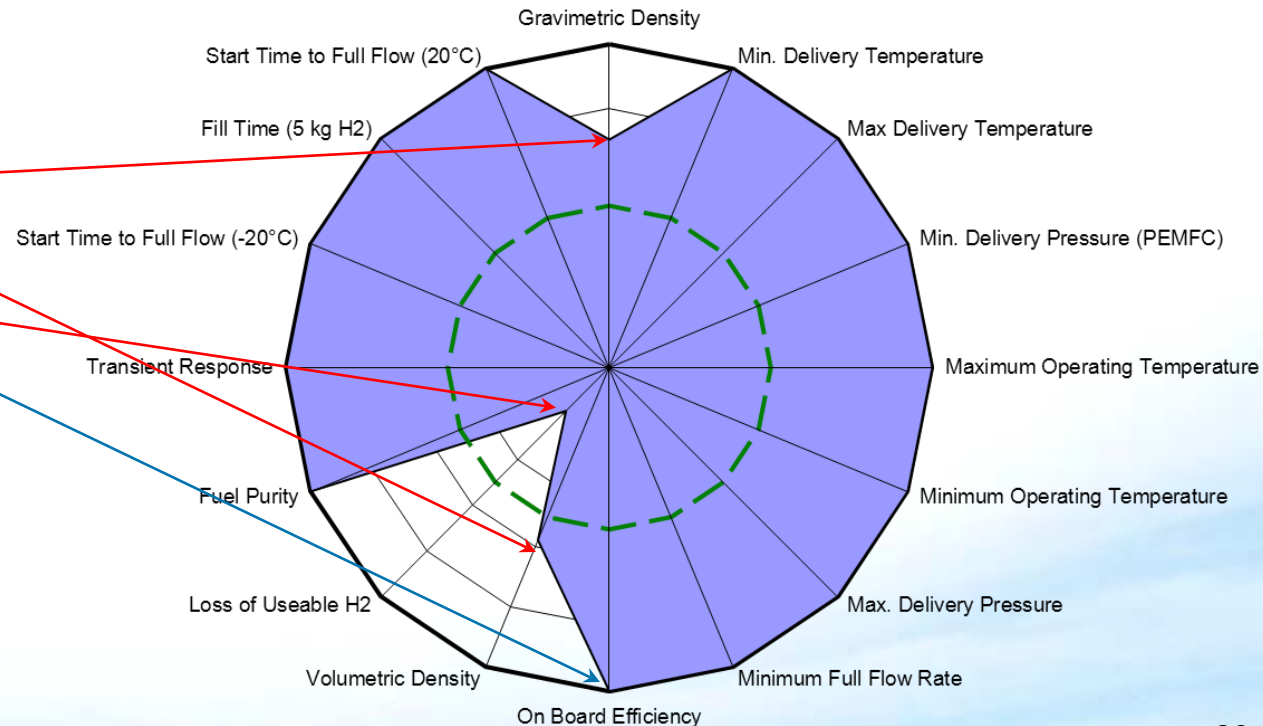
Adsorbent System Projection

2017 Targets

- 2000 bar AX-21, no thermal enhancement, 80 K initial fill
- Type 3 CF/Al lined pressure vessel, 6 mm liner, 200 bar
- Double-wall 60-layer MLVI jacket design, 5W heat leak @ 80 K
- Porous-bed “flow-through” cooling/fueling design for adsorption
- Desorption heat via tank-integral electrical resistance elements/HX



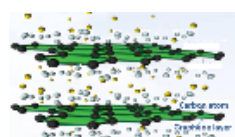
1. Gravimetric Density
2. Volumetric Density
3. System Cost
4. Loss of Usable H_2
5. On-Board Efficiency



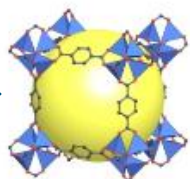
Adsorbent Barriers and Approaches

● Gravimetric Density

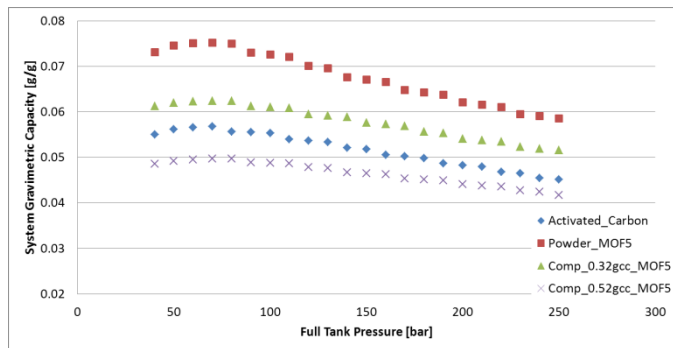
- Media
- Media Compaction
- Type 3 & 4 Tank Development
- Advanced HX Design
 - Modular Tank Insert
 - Flow



Activated Carbon



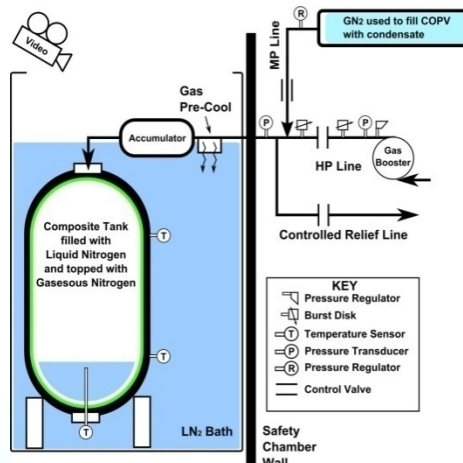
MOF-5



Type IV Cryogenic Pressure Vessel Manufacturing



Cryogenic Tank Burst Facility



Cryogenic Materials Testing



Adsorbent Barriers and Approaches

● Volumetric Density

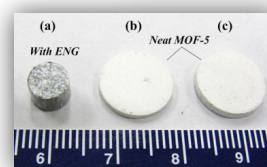
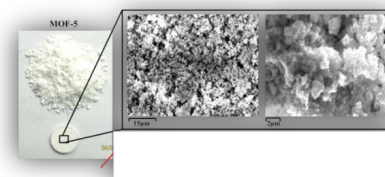
- Media Compaction
- Advanced HX Design
 - Modular Tank Insert
 - Flow Through Cooling
 - Hexagonal Pellet Array



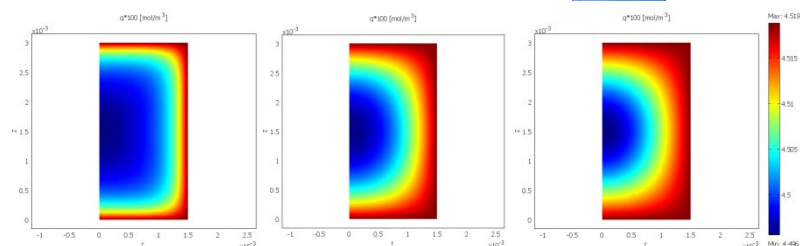
Stacked Pellet Array



Compacted Media Incorporating ENG

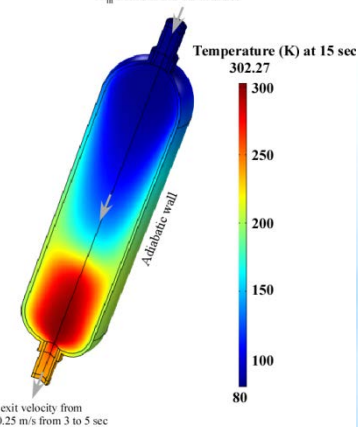


Pellet Thermal Modeling



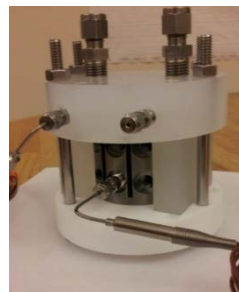
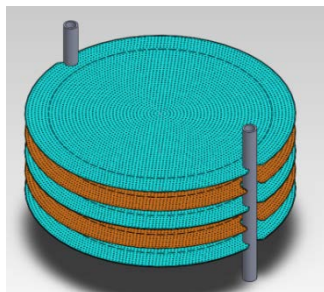
Flow Through Cooling

$T_{in} = 80K$
 P_{in} from 5 to 200 bar in 20 sec



Avg. exit velocity from 0 to 0.25 m/s from 3 to 5 sec

Modular Tank Insert

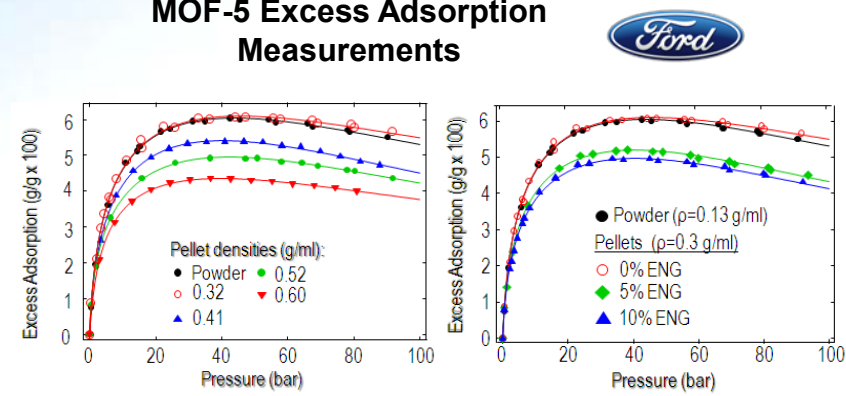


Cryogenic Adsorbent Component Test System

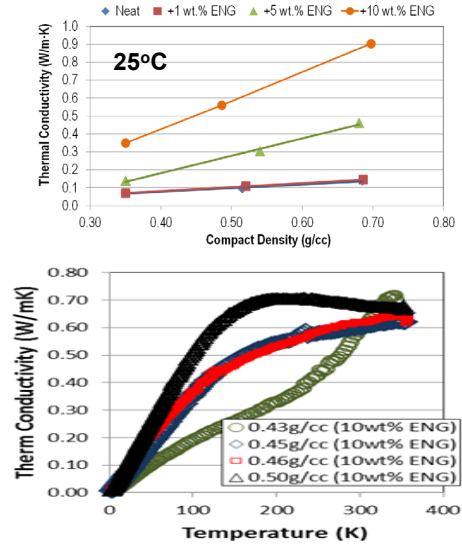


Adsorbent Materials Characterization

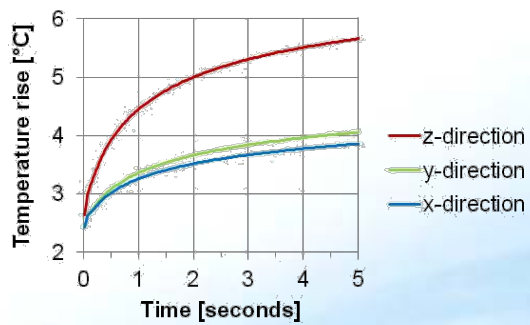
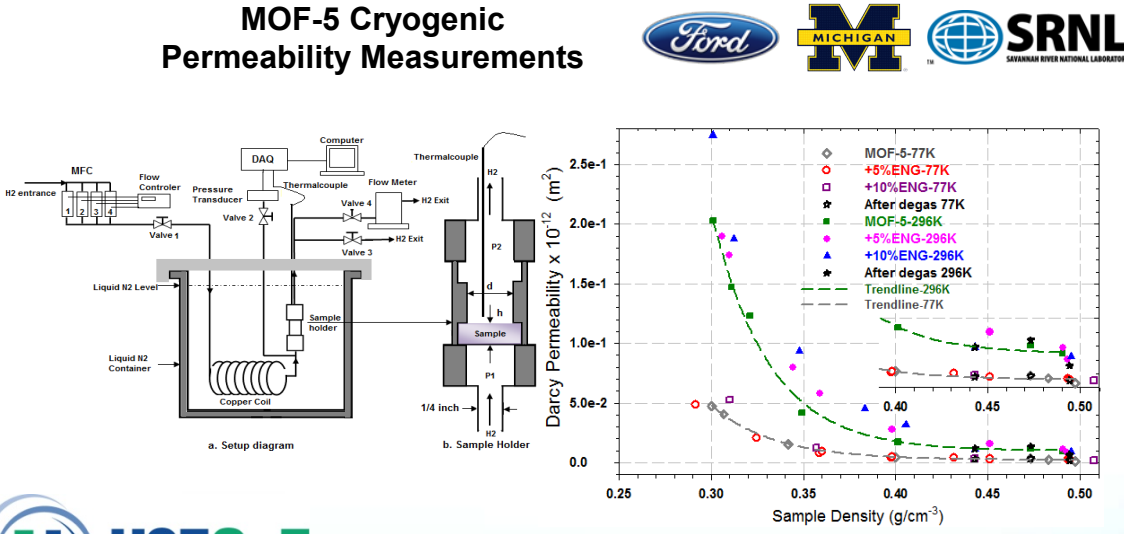
MOF-5 Excess Adsorption Measurements



MOF-5 Thermal Conductivity Measurements



MOF-5 Cryogenic Permeability Measurements

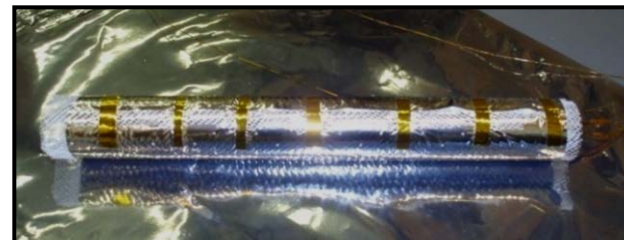


| parameter | 95% confidence interval | Unit |
|----------------|-------------------------|--------|
| kX | 3.32 < 3.45 < 3.58 | W/m/K |
| kY | 1.44 < 1.49 < 1.55 | W/m/K |
| kZ | 0.280 < 0.286 < 0.292 | W/m/K |
| C _p | 1395 < 1438 < 1484 | J/kg/K |

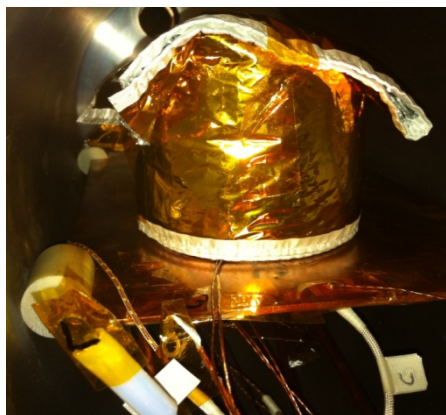
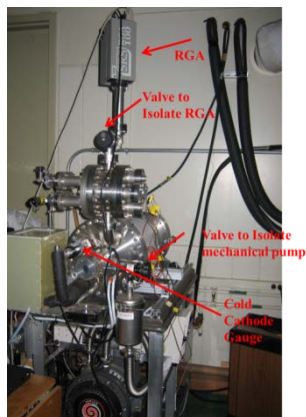
Adsorbent Barriers and Approaches

- **Loss of Usable H₂**
 - **Reducing Parasitic Load**
 - Improved thermal isolation
 - Utilizing Vented Hydrogen

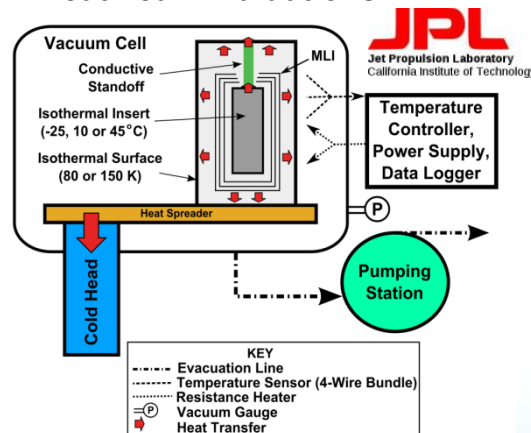
MLVI Development 
Jet Propulsion Laboratory
California Institute of Technology



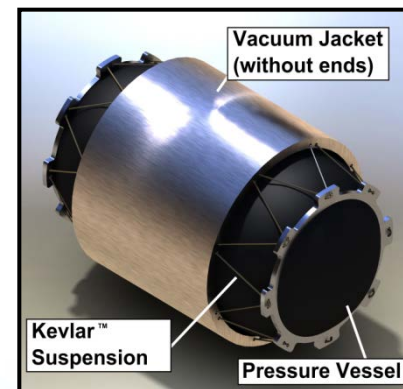
Cryogenic Vacuum Outgassing



Heat Leak Evaluations



Kevlar™-suspended tank
Vacuum shell



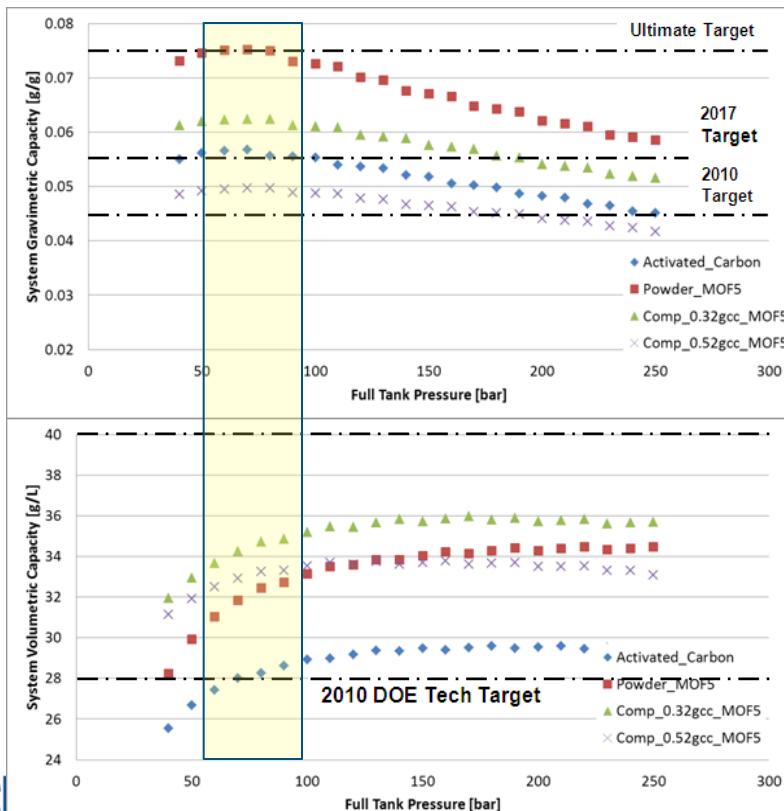
Adsorbent Barriers and Approaches

● On-Board Efficiency

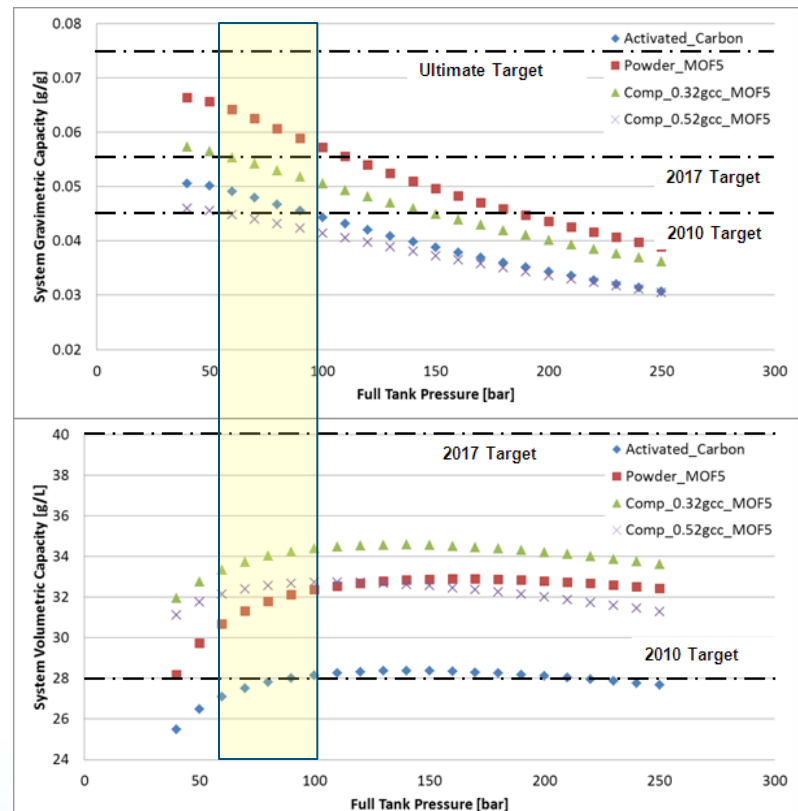
- Low Pressure Design

- Flow-through cooling for refueling
- Resistance heater for desorption
- $40K < T_{\text{operating}} < 120K$

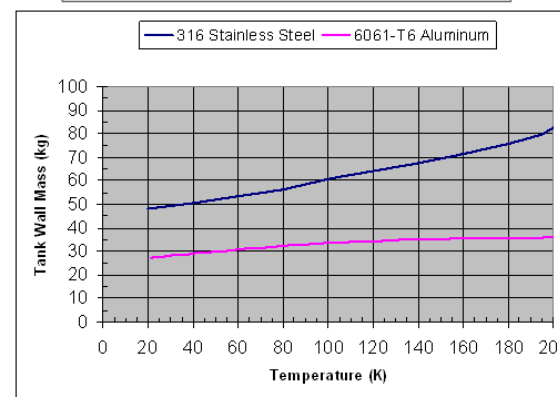
Composite Type III Tank



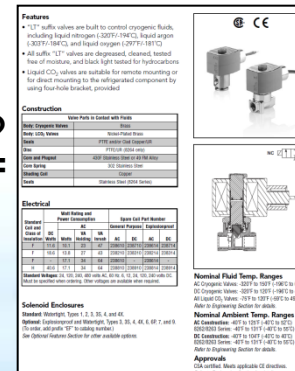
Aluminum Type I Tank



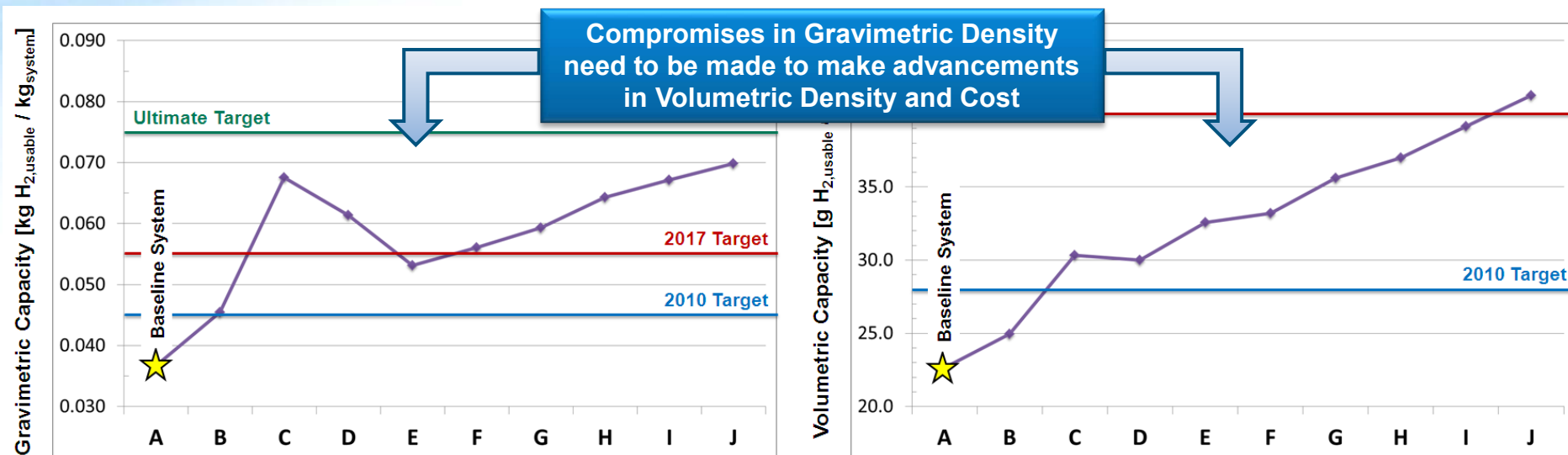
- Low Pressure Type I Tank
- Low cost BoP component identification.



| | Production Amount | | | | | |
|-------------------------|-------------------|---------------|---------------|---------------|----------------|----------------|
| | <u>1,000</u> | <u>10,000</u> | <u>30,000</u> | <u>80,000</u> | <u>130,000</u> | <u>500,000</u> |
| Total Costs | 16,687 | 7,051 | 5,176 | 4,113 | 3,690 | 2,871 |
| \$/kWh | | | | | | 15.4 |
| Item | <u>1,000</u> | <u>10,000</u> | <u>30,000</u> | <u>80,000</u> | <u>130,000</u> | <u>500,000</u> |
| Tanks | 1,837 | 1,578 | 1,470 | 1,381 | 1,340 | 1,308 |
| Media | 6,820 | 1,834 | 1,026 | 642 | 520 | 321 |
| Media Cost/kg | 367 | 99 | 55 | 34 | 28 | 17 |
| Balance of Plant | 5,136 | 2,426 | 1,804 | 1,426 | 1,264 | 980 |
| Assembly | 2,894 | 1,213 | 875 | 664 | 567 | 261 |



Adsorbent System Projection of Progress

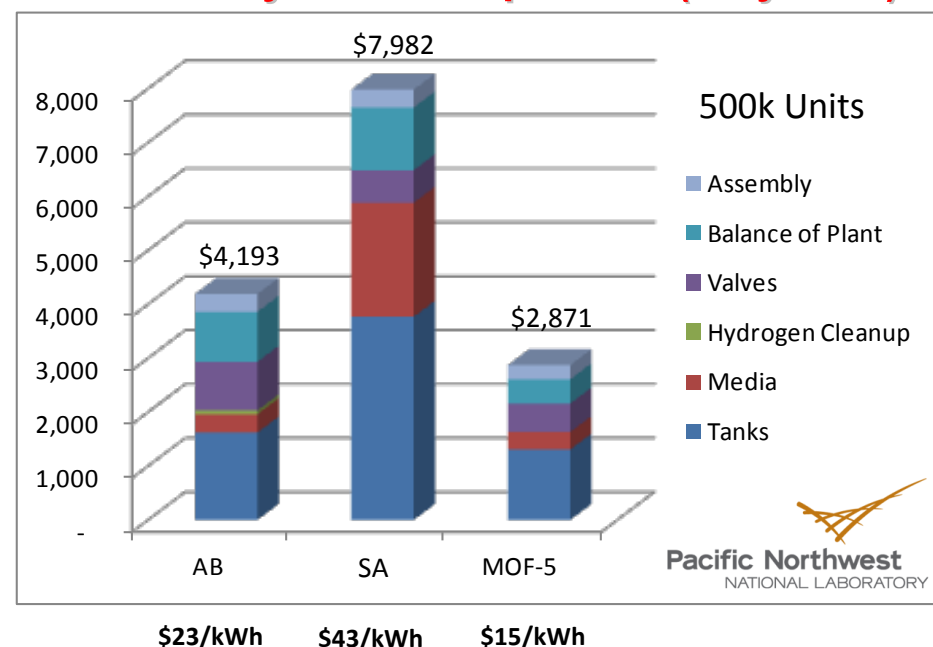


| Step | Description |
|------|--|
| A | Phase 1 Baseline – Activated Carbon in a Composite Tank; Flow-Through Cooling with a Resistance Heater; Full Conditions of 80 K, 200 bar |
| B | Change Material to Powdered MOF-5 |
| C | Change Full Tank Conditions to 40 K, 60 bar |
| D | Change Tank to Type I Aluminum (lower cost) |
| E | Change to Compacted MOF-5 (0.32 g/cc) |
| F | Increase Compacted MOF-5 thermal conductivity by an order of magnitude |
| G | Change from Flow-Through Cooling with a Resistance Heater to the M.A.T.I. |
| H | Reduce mass and volume of BOP components by 25% |
| I | Improve material capacity by 10% |
| J | Improve material capacity by 20% |

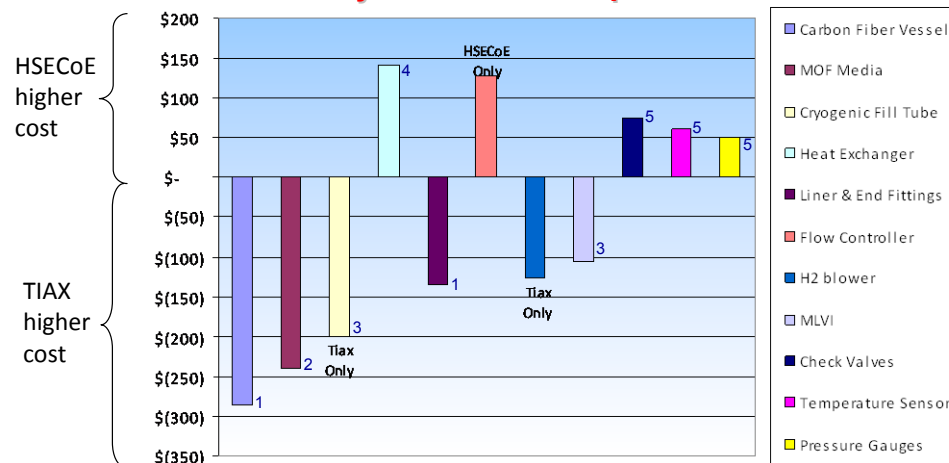
Initial System Cost Projections

- Developing bill-of-materials for various storage systems
- Assessed industry available parts with appropriate capabilities for system conditions
- Reviewed quotes from distributors and manufactures for different quantity levels
- Evaluated progress ratio models based on production level and volume
- Compared costs with direct material models and other benchmarks

HSECoE System Comparison (\$/System)



MOF System Cost Comparison



Comments / Observations

1. Further analysis is required to evaluate pressure vessel cost (fiber and liner)
2. MOF media difference is expected (MOF-177 with TiAx vs MOF-5 with HSECoE)
3. The insulation criteria for the fill tube and MLVI needs confirmation
4. Heat exchanger details needs to be expanded into individual items
5. The main difference is related to the number of parts assumed in the system

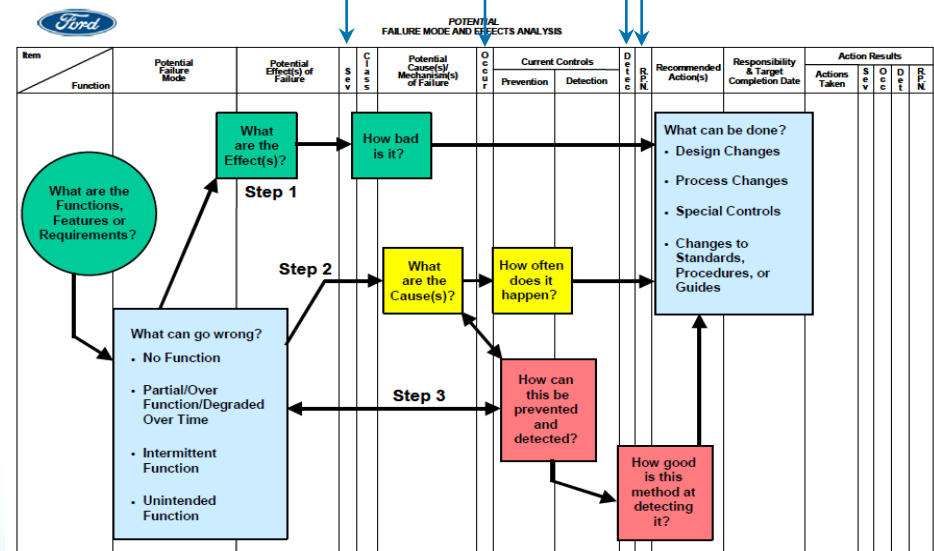
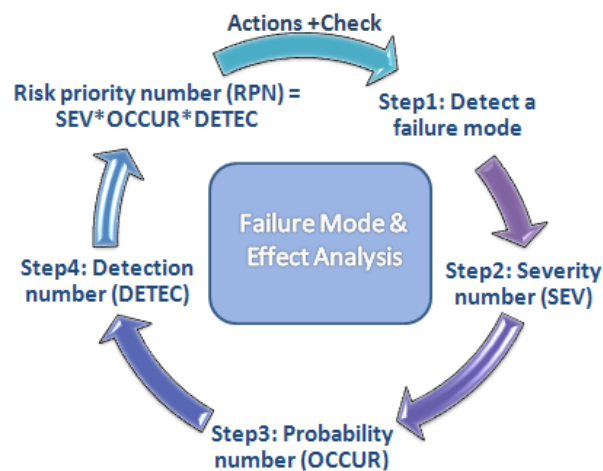
FMEA (Failure Modes and Effects Analysis)

- FMEA Completed for both Adsorbent and Chemical Hydride Systems

- Considered for deployed system

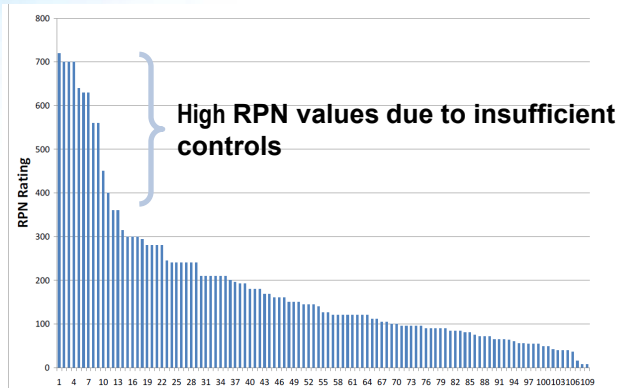
- Severity
- Probability of Occurrence
- Probability of Detection

- Risk Priority Number

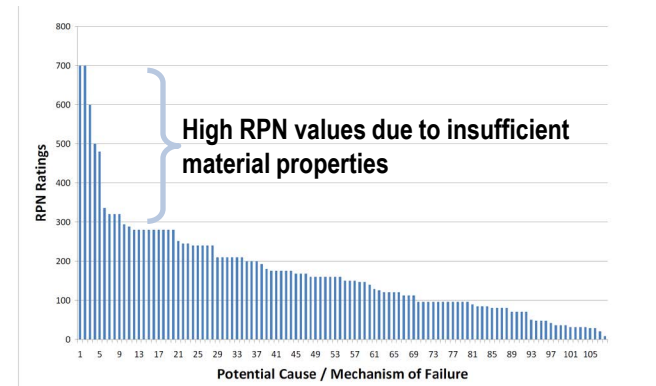


FMEA Results

Adsorbent System



Chemical Hydride System



| Potential Cause | Failure Mode (RPN) | Actions |
|--|--|---|
| Material release rate insufficient due to inhomogeneous materials at end of life | Hydrogen supply unable to achieve full flow rate (720) Storage system only accepts partial fill (630) Storage system on-board efficiency < 90% (560) System only supplies partial capacity (560) Storage system fills in > 3.3 minutes (450) | Consider a vibration test Need to evaluate bed packing Use system models to evaluate sensitivity of contact resistance |
| Type IV tank liner incompatible with adsorbent or in-service activation | System unable to contain hydrogen due to component rupture (700) System exceeds allowable external leak rate limit (700) | Consider in-service process and evaluate the HDPE out-gassing |
| Material release rate insufficient due to impurities | Hydrogen supply unable to achieve full flow rate (640) Storage system only accepts partial fill (560) Storage system fills in > 3.3 minutes (400) | Add a cycle test with spec hydrogen at the limits of J2719 |
| Fuel cell system requires higher delivery pressure | System only supplies partial capacity (560) | Need to confirm with the fuel cell tech team regarding the probability of the min. pressure increase |

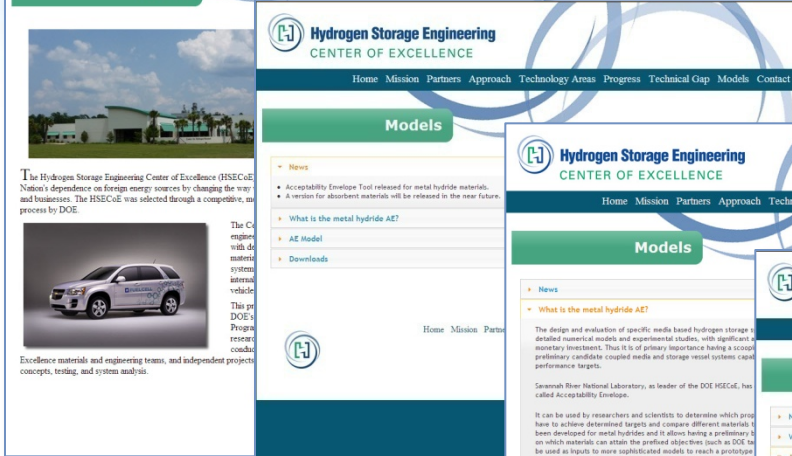
| Potential Cause | Failure Mode (RPN) | Actions |
|--|---|---|
| Not able to charge supply fuel due to the plugged plumbing (8) | System unable to supply hydrogen (320) Hydrogen supply unable to achieve full flow rate (320) Storage system only accepts partial fill (280) Storage system does not accept fuel (280) | Need to evaluate low temperature properties of the media Add settling/flocculation test for evaluating clogging |
| Incomplete phase separation (8) | Hydrogen supply pressure below 5 bar (320) System only supplies partial capacity (280) Storage system on-board efficiency < 90% (280) System only supplies partial capacity (245) | Assess the separator effectiveness and quantify the hydrogen in spent fuel |
| Volume displacement from solids build-up in bladder tank (7) | Storage system only accepts partial fill (294) | Lab scale test of pressurizing the slurry |
| Filling receptacle allows air exposure to fuel (7) | System exceeds allowable external leak rate limit (280) | Need to evaluate the system effects to air exposure |
| Incomplete reaction of the media (7) | Hydrogen supply pressure below 5 bar (320) Storage system on-board efficiency < 90% (245) | Evaluate if material build-up within the reactor can still provide heat transfer |
| BOP components fail to close (7) | System exceeds allowable internal leak rate limit (280) | Include BOP components in bench tests and evaluate cycles |

New Updated WEB Site Launched



List of Models Available

www.HSECoE.org

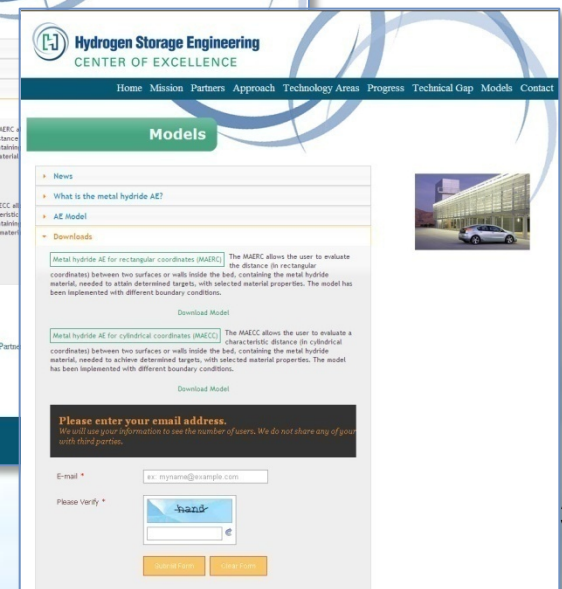
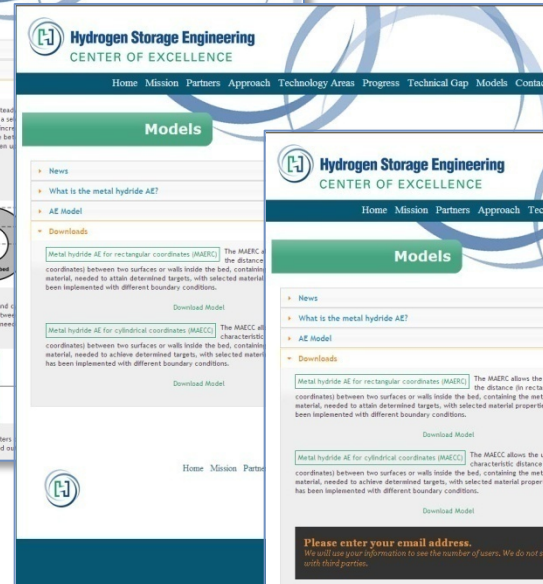
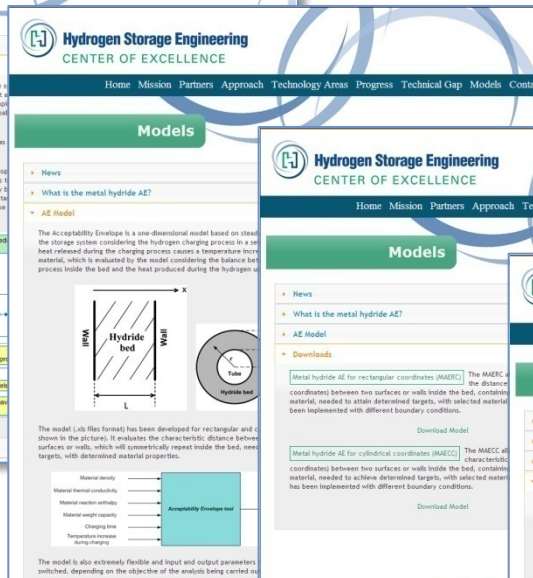


Description of Model

Outline of Analysis

Model Download

Identification of User



- WEB Czar responsible for updating
- Load models on site for public dissemination

Future Work

- **Chemical Hydride System**

- Improved Slurry/Solvent Compositions/Properties
- Improved Chemical Trap Properties
- Flow Through Reactor Design and Evaluation
- Gas/Liquid Separator Evaluation

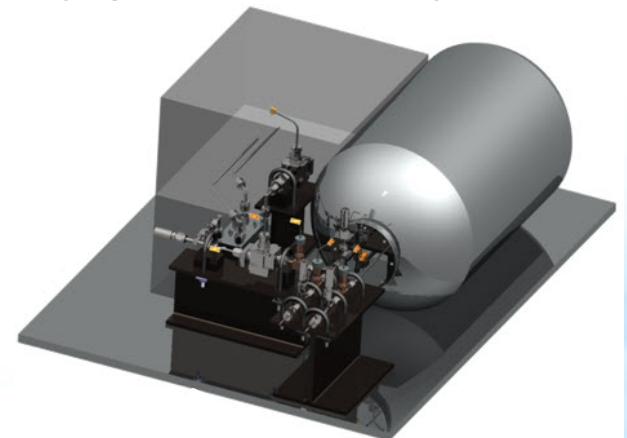
- **Adsorbent System**

- Media Compaction/Characterization
- Advanced HX System Evaluation
- Advanced Insulation Evaluation
- Cryogenic Materials Evaluation

- **Phase 3 Preparations**

- Construct Phase 3 Test Facilities
- Design Phase 3 Test Protocols

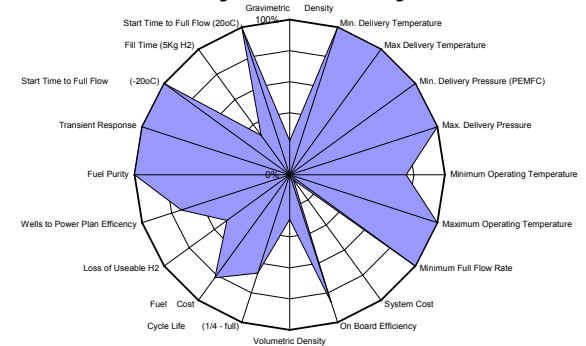
Cryogenic Adsorbent System



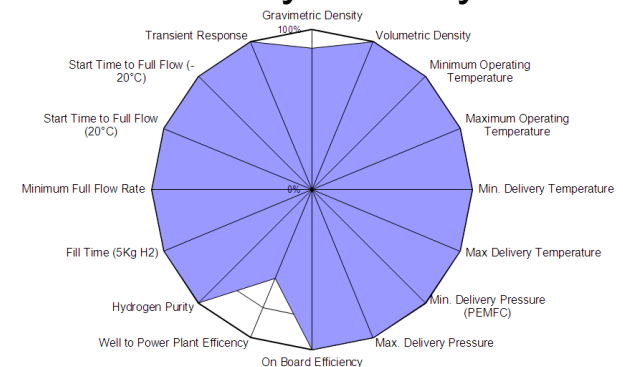
Conclusion

- None of the media considered to date will allow systems to meet all of the DoE technical targets simultaneously but most can be met.
- Chemical Hydrides and Adsorbent Systems hold the highest near term promise of approaching the DoE 2017 Technical Targets.
- Chemical Hydride transport is facilitated by incorporation into a liquid via slurry or dissolution.

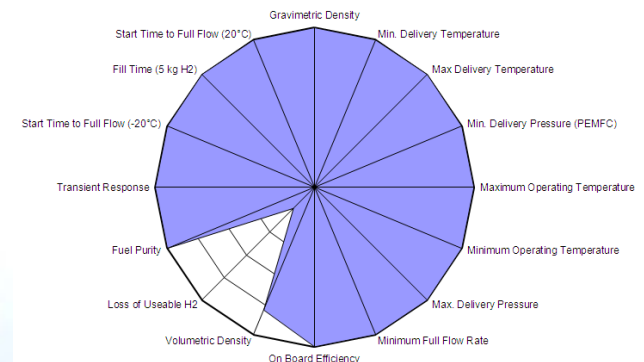
Metal Hydride System



Chemical Hydride System



Adsorbent System





Technical Back-Up Slides

Materials Properties

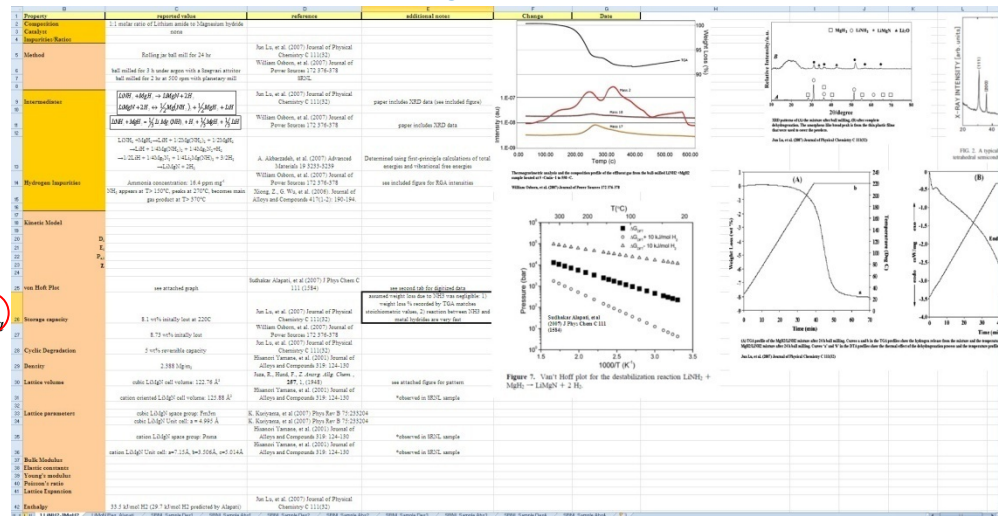
Materials Performance Models

Chemical Hydrides: $\left(\frac{dC}{dt}\right) = A \exp\left(-\frac{E}{RT}\right) (C)^{\frac{1}{2}}$

Metal Hydrides: $\left(\frac{dC}{dt}\right) = A \exp\left(-\frac{E}{RT}\right) \left(\frac{P_e - P}{P_e}\right) (C)^{\frac{1}{2}}$

Adsorbents: $n_{ex} = n_{max} \exp\left[-\left[\frac{RT}{\alpha + \beta T}\right]^2 \ln^2\left(\frac{P_0}{P}\right)\right] - \rho_s V_a$

Materials Catalogue Developed And Deployed on SharePoint®



- **Materials Data:**
 - Kinetics in the entire P & T space anticipated
 - Thermodynamic Properties
 - ΔH , c_p ...
 - Physical Properties
 - ρ_c , ρ_p , κ_p , ...

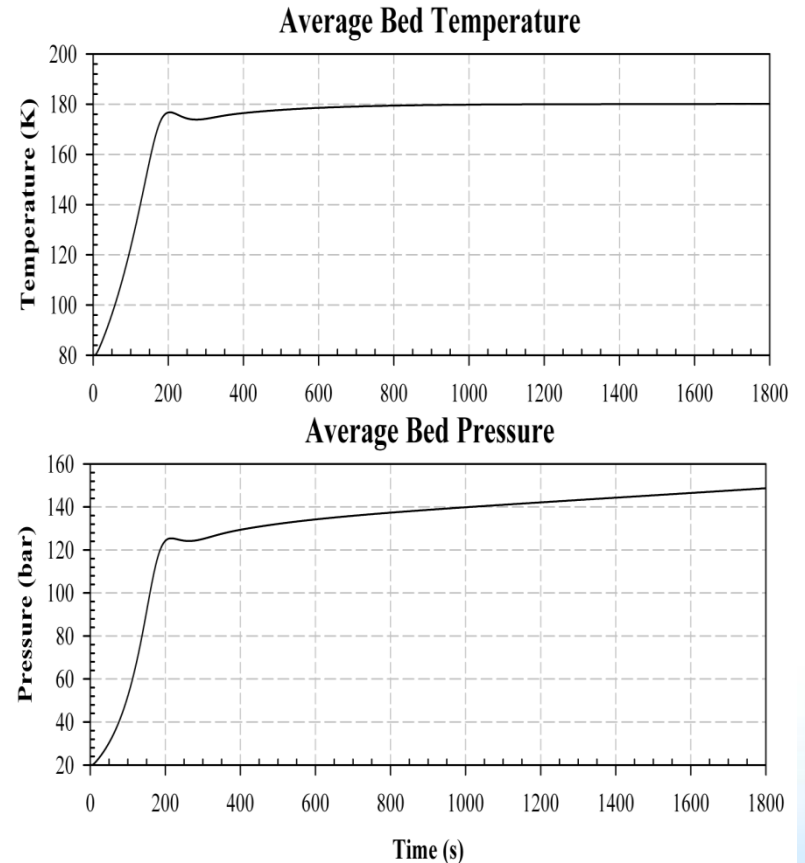
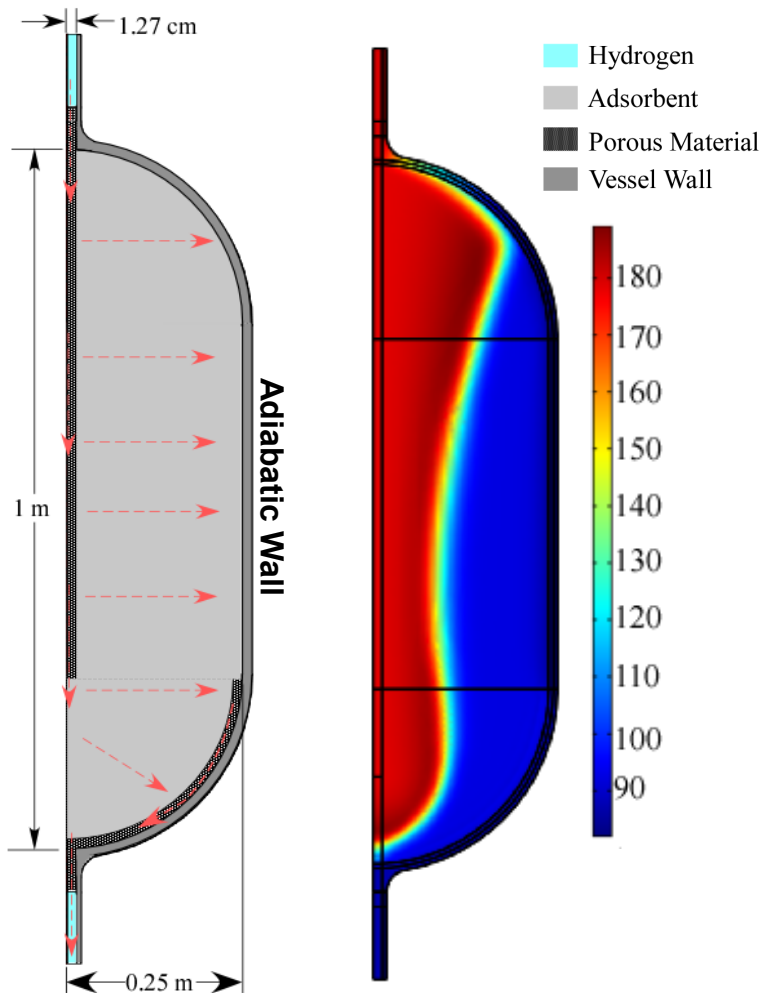
| 120C/160bar/15hrs Abs | | | 100C/1bar Desorption | | | 110C/1bar Desorption | | | 120C/1bar Desorption | | | 80C/1bar Desorption | | |
|-----------------------|--------|----------|----------------------|--------|----------|----------------------|--------|----------|----------------------|--------|----------|---------------------|--------|----------|
| P/h | h/w | wt% | P/h | h/w | wt% | P/h | h/w | wt% | P/h | h/w | wt% | P/h | h/w | wt% |
| 17.28076 | 0.0000 | -1.1485% | 17.78116 | 0.0000 | -2.6114% | 15.92968 | 0.0000 | -2.4216% | 15.84628 | 0.0000 | -2.3089% | 16.64692 | 0.0000 | -1.0579% |
| 17.29744 | 0.0167 | -1.022% | 17.79784 | 0.0167 | -2.5425% | 15.94636 | 0.0167 | -2.3095% | 15.86296 | 0.0167 | -2.1174% | 16.6636 | 0.0167 | -1.0012% |
| 17.31412 | 0.0334 | -1.0592% | 17.81452 | 0.0334 | -2.4875% | 15.96304 | 0.0334 | -2.2010% | 15.87964 | 0.0334 | -1.9457% | 16.68028 | 0.0334 | -1.0004% |
| 17.33080 | 0.0500 | -1.0590% | 17.83120 | 0.0500 | -2.4440% | 15.97972 | 0.0500 | -2.1455% | 15.89632 | 0.0500 | -1.8102% | 16.69696 | 0.0500 | -0.9551% |
| 17.34748 | 0.0667 | -1.0409% | 17.84788 | 0.0667 | -2.3994% | 15.99640 | 0.0667 | -2.0181% | 15.91300 | 0.0667 | -1.6388% | 16.71364 | 0.0667 | -0.9500% |
| 17.36416 | 0.0834 | -1.0438% | 17.86456 | 0.0834 | -2.3523% | 16.01308 | 0.0834 | -1.9218% | 15.92968 | 0.0834 | -1.4835% | 16.73032 | 0.0834 | -0.9389% |
| 17.38084 | 0.1001 | -1.0306% | 17.88124 | 0.1001 | -2.3093% | 16.02976 | 0.1001 | -1.8296% | 15.94636 | 0.1001 | -1.3325% | 16.74700 | 0.1001 | -0.9098% |
| 17.39752 | 0.1168 | -1.0117% | 17.89792 | 0.1168 | -2.2620% | 16.04644 | 0.1168 | -1.7475% | 15.96304 | 0.1168 | -1.1777% | 16.76368 | 0.1168 | -0.9048% |
| 17.41420 | 0.1334 | -1.0288% | 17.91460 | 0.1334 | -2.2319% | 16.06312 | 0.1334 | -1.6805% | 15.97972 | 0.1334 | -1.0350% | 16.78036 | 0.1334 | -0.9000% |
| 17.43088 | 0.1501 | -1.0139% | 17.93128 | 0.1501 | -2.1993% | 16.07980 | 0.1501 | -1.5796% | 15.99640 | 0.1501 | -0.8886% | 16.79704 | 0.1501 | -0.9072% |
| 17.44756 | 0.1668 | -1.0050% | 17.94796 | 0.1668 | -2.1489% | 16.09648 | 0.1668 | -1.4939% | 16.01308 | 0.1668 | -0.7562% | 16.81372 | 0.1668 | -0.8844% |
| 17.46424 | 0.1835 | -1.0123% | 17.96464 | 0.1835 | -2.1144% | 16.11316 | 0.1835 | -1.3983% | 16.02976 | 0.1835 | -0.6140% | 16.83040 | 0.1835 | -0.8758% |
| 17.48092 | 0.2002 | -1.0071% | 17.98132 | 0.2002 | -2.0521% | 16.12984 | 0.2002 | -1.3028% | 16.04644 | 0.2002 | -0.4979% | 16.84708 | 0.2002 | -0.8632% |
| 17.49760 | 0.2168 | -1.0031% | 17.99800 | 0.2168 | -2.0059% | 16.14652 | 0.2168 | -1.2332% | 16.06312 | 0.2168 | -0.3839% | 16.86376 | 0.2168 | -0.8586% |
| 17.51428 | 0.2335 | -1.0065% | 18.01468 | 0.2335 | -1.9735% | 16.16320 | 0.2335 | -1.1418% | 16.07980 | 0.2335 | -0.3059% | 16.88044 | 0.2335 | -0.8382% |
| 17.53096 | 0.2502 | -1.0100% | 18.03136 | 0.2502 | -1.9354% | 16.17988 | 0.2502 | -1.0544% | 16.09648 | 0.2502 | -0.2260% | 16.89712 | 0.2502 | -0.8497% |
| 17.54764 | 0.2669 | -0.9975% | 18.04804 | 0.2669 | -1.8973% | 16.19656 | 0.2669 | -0.9632% | 16.11316 | 0.2669 | -0.1860% | 16.91380 | 0.2669 | -0.8412% |
| 17.56432 | 0.2836 | -0.9769% | 18.06472 | 0.2836 | -1.8353% | 16.21324 | 0.2836 | -0.8898% | 16.12984 | 0.2836 | -0.1681% | 16.93048 | 0.2836 | -0.8108% |
| 17.58100 | 0.3002 | -0.9905% | 18.08140 | 0.3002 | -1.7892% | 16.22992 | 0.3002 | -0.8283% | 16.14652 | 0.3002 | -0.1322% | 16.94716 | 0.3002 | -0.8225% |
| 17.59768 | 0.3169 | -0.9662% | 18.09808 | 0.3169 | -1.7472% | 16.24660 | 0.3169 | -0.7753% | 16.16320 | 0.3169 | -0.1363% | 16.96384 | 0.3169 | -0.8662% |
| 17.61436 | 0.3336 | -0.9797% | 18.11476 | 0.3336 | -1.7272% | 16.26328 | 0.3336 | -0.6837% | 16.17988 | 0.3336 | -0.1363% | 16.98052 | 0.3336 | -0.7899% |
| 17.63104 | 0.3503 | -0.9715% | 18.13144 | 0.3503 | -1.6773% | 16.27996 | 0.3503 | -0.6084% | 16.19656 | 0.3503 | -0.1324% | 16.99720 | 0.3503 | -0.7856% |
| 17.64772 | 0.3670 | -0.9751% | 18.14812 | 0.3670 | -1.6433% | 16.29664 | 0.3670 | -0.5609% | 16.21324 | 0.3670 | -0.1145% | 17.01388 | 0.3670 | -0.7752% |
| 17.66440 | 0.3836 | -0.9699% | 18.16480 | 0.3836 | -1.5775% | 16.31332 | 0.3836 | -0.5055% | 16.22992 | 0.3836 | -0.1069% | 17.03056 | 0.3836 | -0.7710% |
| 17.68108 | 0.4003 | -0.9705% | 18.18148 | 0.4003 | -1.5317% | 16.33000 | 0.4003 | -0.4699% | 16.24660 | 0.4003 | -0.0880% | 17.04724 | 0.4003 | -0.7749% |
| 17.69776 | 0.4170 | -0.9623% | 18.19816 | 0.4170 | -1.4978% | 16.34668 | 0.4170 | -0.4244% | 16.26328 | 0.4170 | -0.1106% | 17.06392 | 0.4170 | -0.7626% |
| 17.71444 | 0.4337 | -0.9600% | 18.21484 | 0.4337 | -1.4659% | 16.36336 | 0.4337 | -0.3750% | 16.27996 | 0.4337 | -0.1026% | 17.08060 | 0.4337 | -0.7384% |
| 17.73112 | 0.4504 | -0.9438% | 18.23152 | 0.4504 | -1.4161% | 16.38004 | 0.4504 | -0.3453% | 16.29664 | 0.4504 | -0.0947% | 17.09728 | 0.4504 | -0.7422% |
| 17.74780 | 0.4670 | -0.9478% | 18.24820 | 0.4670 | -1.3703% | 16.39672 | 0.4670 | -0.3245% | 16.31332 | 0.4670 | -0.1067% | 17.11396 | 0.4670 | -0.7300% |
| 17.76448 | 0.4837 | -0.9553% | 18.26488 | 0.4837 | -1.3166% | 16.41340 | 0.4837 | -0.2920% | 16.33000 | 0.4837 | -0.1207% | 17.13064 | 0.4837 | -0.7160% |
| 17.78116 | 0.5004 | -0.9689% | 18.28156 | 0.5004 | -1.2906% | 16.43008 | 0.5004 | -0.2802% | 16.34668 | 0.5004 | -0.0988% | 17.14732 | 0.5004 | -0.7198% |
| 17.79784 | 0.5171 | -0.9429% | 18.29824 | 0.5171 | -1.2410% | 16.44676 | 0.5171 | -0.2604% | 16.36336 | 0.5171 | -0.1028% | 17.16400 | 0.5171 | -0.7037% |
| 17.81452 | 0.5338 | -0.9348% | 18.31492 | 0.5338 | -1.2012% | 16.46344 | 0.5338 | -0.2467% | 16.38004 | 0.5338 | -0.1028% | 17.18068 | 0.5338 | -0.7035% |
| 17.83120 | 0.5504 | -0.9305% | 18.33160 | 0.5504 | -1.1674% | 16.48012 | 0.5504 | -0.2467% | 16.39672 | 0.5504 | -0.0989% | 17.19736 | 0.5504 | -0.6914% |
| 17.84788 | 0.5671 | -0.9542% | 18.34828 | 0.5671 | -1.1216% | 16.49680 | 0.5671 | -0.2349% | 16.41340 | 0.5671 | -0.0909% | 17.21404 | 0.5671 | -0.6794% |
| 17.86456 | 0.5838 | -0.9460% | 18.36496 | 0.5838 | -1.0839% | 16.51348 | 0.5838 | -0.2270% | 16.43008 | 0.5838 | -0.0929% | 17.23072 | 0.5838 | -0.6653% |
| 17.88124 | 0.6005 | -0.9260% | 18.38164 | 0.6005 | -1.0509% | 16.53016 | 0.6005 | -0.2152% | 16.44676 | 0.6005 | -0.1029% | 17.24740 | 0.6005 | -0.6731% |
| 17.89792 | 0.6172 | -0.9259% | 18.39832 | 0.6172 | -1.0143% | 16.54684 | 0.6172 | -0.2192% | 16.46344 | 0.6172 | -0.1069% | 17.26408 | 0.6172 | -0.6690% |
| 17.91460 | 0.6339 | -0.9256% | 18.41500 | 0.6339 | -0.9726% | 16.56352 | 0.6339 | -0.2192% | 16.48012 | 0.6339 | -0.1090% | 17.28076 | 0.6339 | -0.6529% |
| 17.93128 | 0.6506 | -0.9374% | 18.43168 | 0.6506 | -0.9567% | 16.58020 | 0.6506 | -0.2192% | 16.49680 | 0.6506 | -0.1070% | 17.29744 | 0.6506 | -0.6569% |
| 17.94796 | 0.6672 | -0.9372% | 18.44836 | 0.6672 | -0.9150% | 16.59688 | 0.6672 | -0.2153% | 16.51348 | 0.6672 | -0.1030% | 17.31412 | 0.6672 | -0.6369% |

Storage System Modeling

Detailed FEM Thermal/Mass Analysis

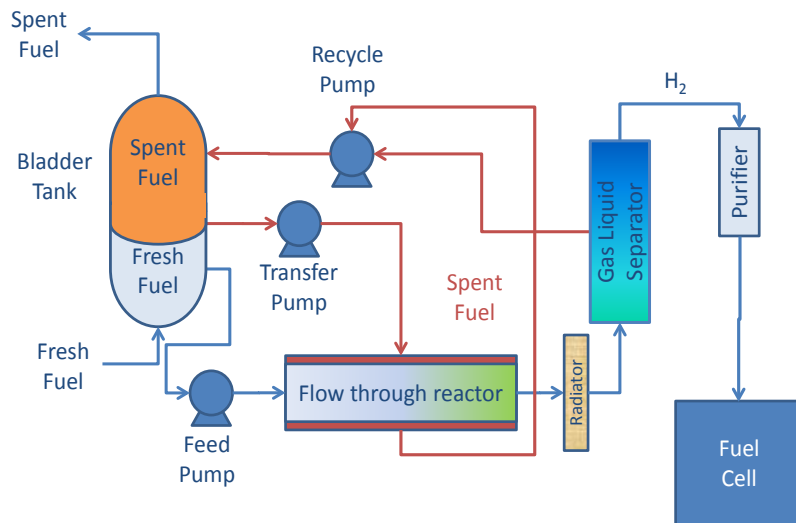


Lumped Parameter Models

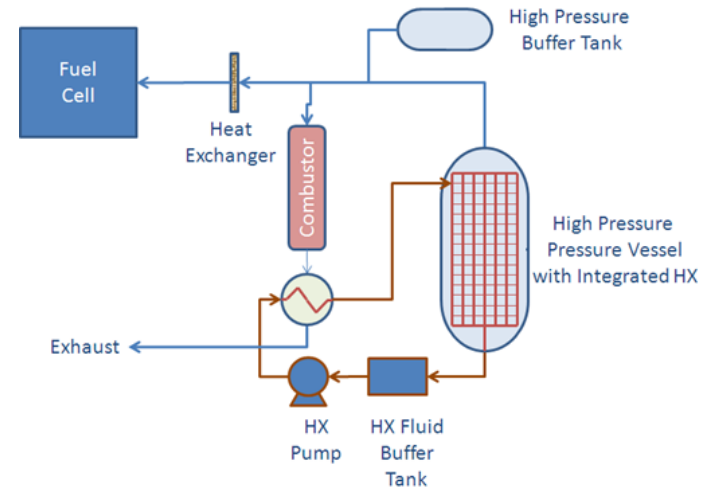


SRNL 200 bar
AX-21
Flow-Through

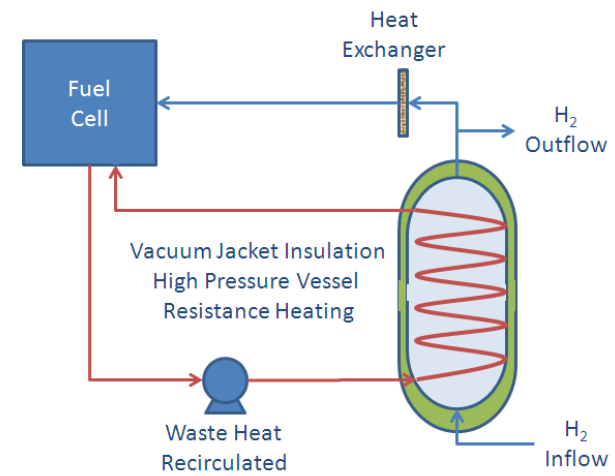
System Concepts



Fluid Chemical Hydride System



Metal Hydride System



Cryo-Adsorbent System

BoP Catalogue Developed

BoP Catalogue on SharePoint

Volume
Weigh
Cost

Microsoft Excel - BOP component library-9-30-2010.xlsx

Category: Ciproadsorb System, MH System, CH System, Electrical, Filtration, Pressure Vessel and Containment, Flow & Level Control, Check Val, Pressure R

| Part # | Description | Pressure psig/bar | Dimensions (cm) LxWxH or L x dia | Wt (g) | Vol (L) | Representative Model | Component Cost |
|--------|-------------|----------------------|-------------------------------------|--------|---------|--|----------------|
| 10 | TNK | | | | | | |
| 11 | THKHX | | | | | | |
| 12 | INS | | | | | | |
| 13 | BOSS | | | | | | |
| 14 | FIB | | | | | | |
| 15 | RES | | | | | | |
| 16 | H2Med | | | | | | |
| 17 | MNT | | | | | | |
| 18 | BLST-TNK | | | | | | |
| 19 | RYNT | | | | | | |
| 20 | CS | 6000/434 | 6.3 x 3.2 x 2.8 | 354 | 0.04 | R220T3-3FP-1450/Circle Seal | |
| 21 | PRV | 2500/173 | 7.1 x 2.54 | 203 | 0.036 | S100-55T1T1/Circle Seal | |
| 22 | PRV | 1450/100 | 10.8 x 2.54 | 437 | 0.055 | M5100T3-MFP-1450/Circle Seal | |
| 23 | MV | | | | | | |
| 24 | AV2 | 3000/205 | 19 x 5 | 1723 | 0.37 | SV30A2NCSF04D/Circle Seal Controls | |
| 25 | AV3 | 3000/205 | 19 x 5 | 1723 | 0.37 | SV30A3ZPF04D/Circle Seal Controls | |
| 26 | PR | 5000/345 | 13 x 6.3 | 1093 | 0.41 | 20-1234-2911/Tescom Industrial Controls | |
| 27 | GA | | | | | | |
| 28 | PT | 7250/500 | 6.9 x 2.23 | 215 | 0.027 | AST2000M-00440-81-F1-417/American Sensors Technology | |
| 29 | FLC | | | | | | |
| 30 | T | 6500/450 | 0.95 OD x 0.16 wall | 0.32 | lg/m | SS-T6-S-065-6ME/Swagelok 316 SS | |
| 31 | HE | | | | | | |
| 32 | HDFD | | | | | | |
| 33 | FLUP | | | | | | |
| 34 | RD | | | | | | |
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| 37 | ELECT | | | | | | |
| 38 | CNTSYS | | | | | | |
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1. This diagram illustrates description cycle - a catalytic heater is necessary to heat the fluid and provide heat of desorption.
2. For refilling, same set of pipelines will carry the cooling.

MH System, CH System, Category Page, Electrical, Filtration, Pressure Vessel and Containment, Flow & Level Control, Check Valves, Pressure Relief Device

Specific System
Design

Metal Hydride System

Pressure Relief Device

Operating Pressure
Burst Pressure
Operating Temperature

Microsoft Excel - BOP component library-9-30-2010.xlsx

Category: Ciproadsorb System, MH System, CH System, Electrical, Filtration, Pressure Vessel and Containment, Flow & Level Control, Check Val, Pressure R

| Category | Ciproadsorb System | MH System | CH System | Electrical | Filtration | Pressure Vessel and Containment | Flow & Level Control | Check Val | Pressure R |
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500 series adjustable, pop-off & inline relief valves

2024-T3/T351 or 6061-T6/T651 Aluminum, 303 or 316 Stainless Steel

Buna N, Ethylene propylene, Neoprene, Silicone, Teflon or Viton

5100 series relief valves

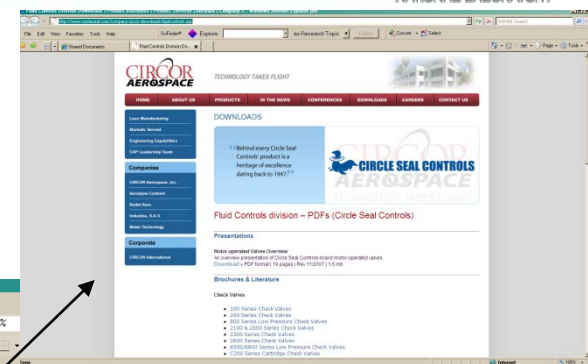
2024-T351 Aluminum, 303 or 316 Stainless Steel

Buna N, EP, Neoprene, Teflon or Viton

5500 & 5775 Series Pilot-operated Relief Valves

2024-T4/T351 Aluminum, or 303 Stainless Steel

Buna N, EP and Viton



Integrated Model Framework

$$n_{ex} = n_{max} \exp \left[- \left[\frac{RT}{\alpha + \beta T} \right]^2 \ln^2 \left(\frac{P_0}{P} \right) \right] - \rho_g V_a$$



SRNL 200 bar
AX-21
Flow-Through

