

Hydrogen Compression Application of the Linear Motor Reciprocating Compressor (LMRC)

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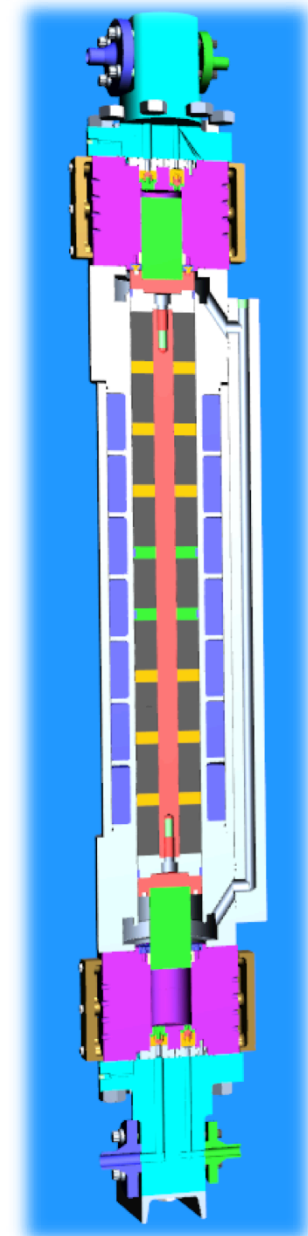
June 7, 2016



SOUTHWEST RESEARCH INSTITUTE



Project ID: PD108



Overview

Timeline

| Description | Date / Timeframe |
|--------------------|------------------|
| Project Start Date | 9/05/14 |
| Project End Date | 10/04/17 |
| Project Duration | 3.0 years |
| Project Progress | 1.5 years |

Budget

- Total Project Budget: \$2,284,553
 - Total Cost Share: \$459,160
 - Total Federal Share: \$1,825,393
 - Total DOE Funds Spent*: \$624,690

* As of 4/6/15, includes ACI's March 2016 charges

Barriers

| Barriers | Targets |
|---------------------------|-----------------------------|
| Low Compressor Efficiency | >73% Isentropic Efficiency* |
| Capital Cost | <\$240,000 per compressor** |
| O&M Costs | <\$4,800 per year** |

* DOE Project Target

** Targets in the 2012 MYRD&D for 2020

Partners

- ACI Services

- Project Objectives:
 - Improve **isentropic efficiency above 95%** by minimizing aerodynamic losses
 - Low speed
 - High valve area ratio
 - **Reduce capital costs** to half that of conventional reciprocating compressors by minimizing part count
 - **Reduce required maintenance** by simplifying the compressor design to eliminate common wear items
- BP1: Analyzed and Designed LMRC to be tested in BP2 & BP3
- This Budget Period (Fiscal Year 2016, BP2):
 - Detailed Mechanical Design
 - Estimated Cost Projection for full-scale version
 - Designed Compressor Test Stand for LP Stage

Approach / Milestones

Fiscal Year 2015 – Design All 3 Stages

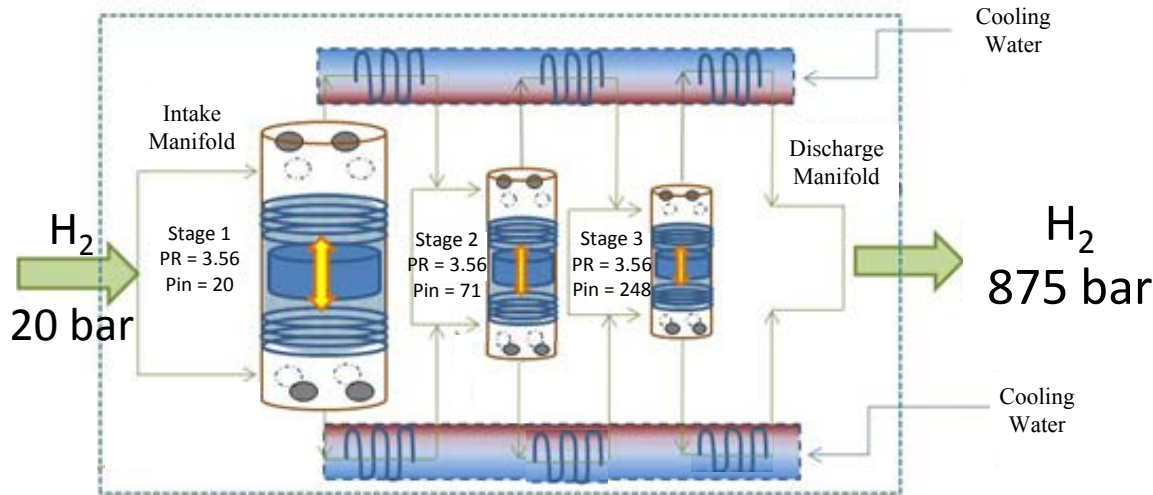
| Task Title | Milestone Description (Go/No-Go Decision Criteria) | % Complete |
|--|---|------------|
| Stage Sizing | Provide cylinder size for each stage and accompanying calculations. | 100 |
| Basic Mechanical Design | Provide FEA results and analysis, basic structural design, and material selection. | 100 |
| Linear Motor Design | Provide linear motor design, including required magnet size and configuration of windings. | 100 |
| Bearing and Seal Design and Analysis | Provide selected bearing and seal technology and supporting calculations. | 100 |
| Valve Selection | Provide the valve type that will be used for the proposed system. | 100 |
| Pulsation Control Design | Provide pulsation control design and/or techniques such that the predicted piping system pulsations are at or below the amplitudes specified in the API Standard 618. | 100 |
| Cooling System Design | Provide cooler sizes and cylinder cooling specifications | 100 |
| Materials and Coatings Selection | Deliver material specifications and manufacturer availability | 100 |
| Performance Predictions and Comparison | Deliver performance predictions and final CFD calculations | 100 |

Approach / Milestones

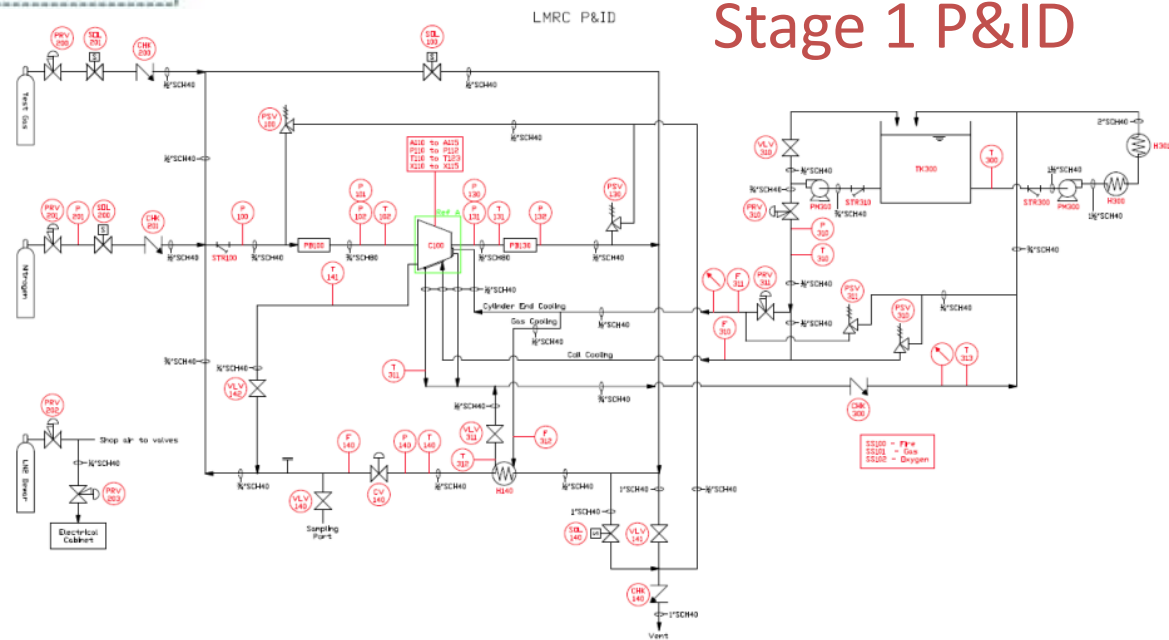
Fiscal Year 2016 – Fabricate and Test LP Stage

| Task Title | Milestone Description (Go/No-Go Decision Criteria) | % Complete | Planned Quarter |
|--|---|------------|-----------------|
| Detailed Mechanical Design | Provide final fabrication drawings of each compressor component and manufacturing/assembly drawings of the components <i>(order long-lead items late Q5 or early Q6)</i> | 100 | 5 |
| Estimate Cost Projection for full-scale version | Deliver cost estimate and calculations for a full-scale version | 100 | 6 |
| Design of Compressor Test Stand for LP Stage | Test Matrix for Bench Scale Testing. Plans for Commissioning, Safety, and Operation of Test Stand. Provide final compression system and test stand design. | 90 | 6 |
| Low Pressure (LP) Stage Compressor Parts Fabrication | Order or fabricate the compressor parts in accordance with the detailed design. | 30 | 7 |
| Low Pressure (LP) Stage Compressor Assembly | Complete assembly of the compressor based on the detailed design. | 0 | 7 |
| Test Stand Construction, Compressor Integration | Manufacture the test stand using the drawings and details created in the previous budget period. | 0 | 7 |
| Commissioning & Startup of Demonstration Model | Verify and report the operability of the compressor and test stand. | 0 | 8 |
| Bench Scale Testing | Report on the completion of the single-stage testing. | 0 | 8 |

Accomplishments and Progress: Overall Concept & Test Loop

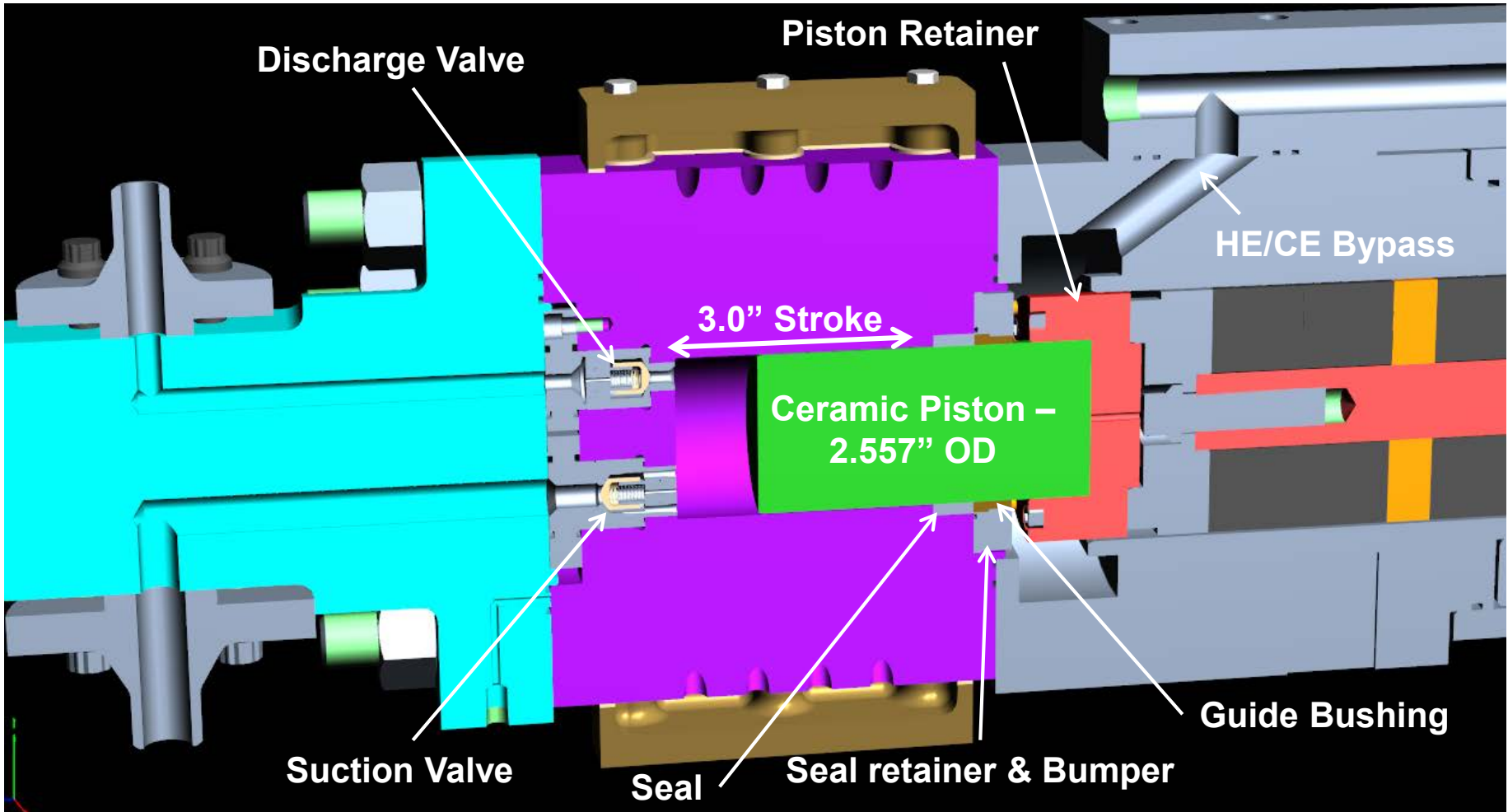


Compress H_2
in 3 stages
with LMRCs

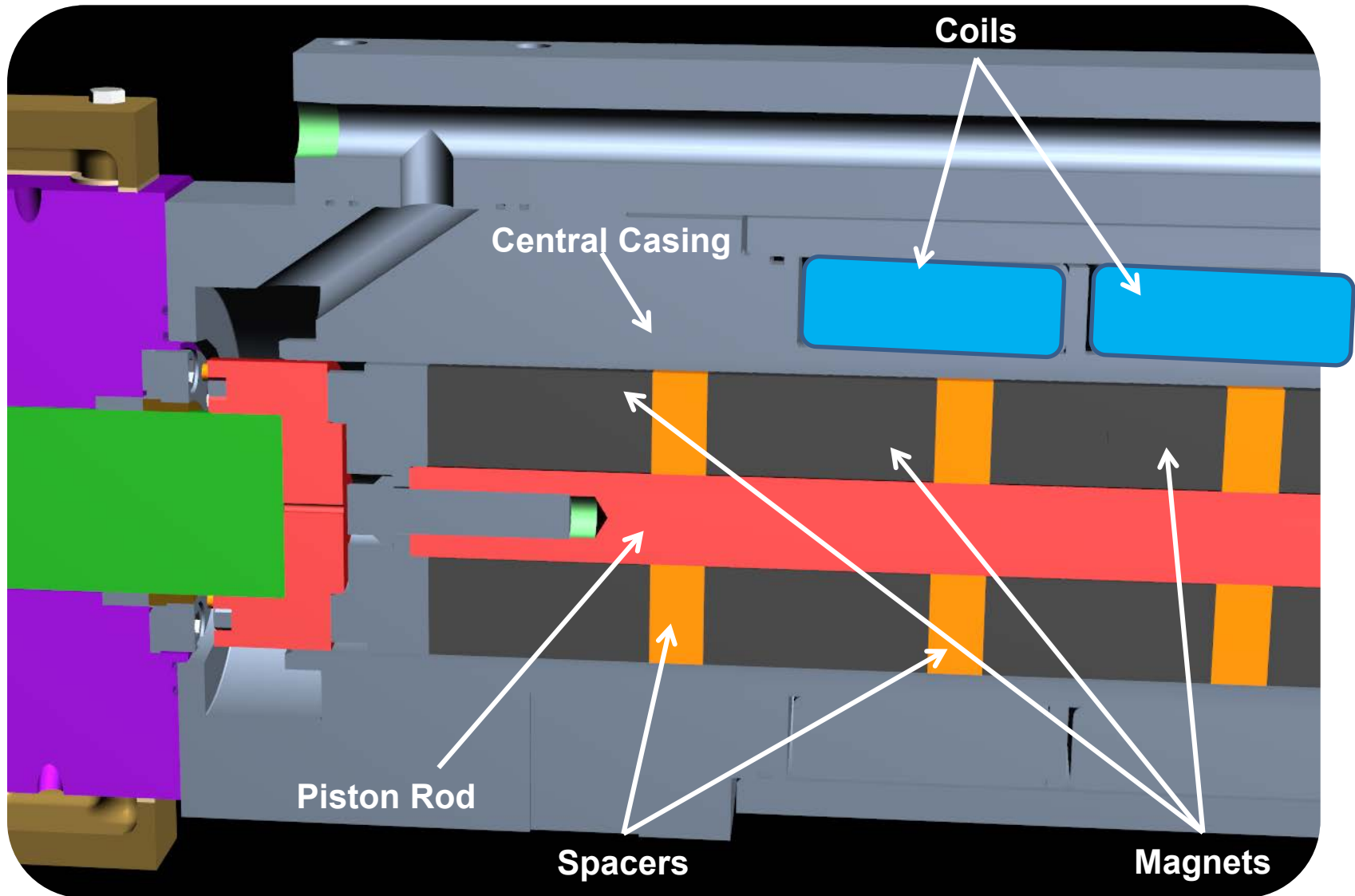


Accomplishments and Progress: 3D Model: Piston Close-up

- Structural design created & FEA performed for each of the 3 stages
- Materials selection is complete



Accomplishments and Progress: 3D Model: Magnet/Coil Close-up

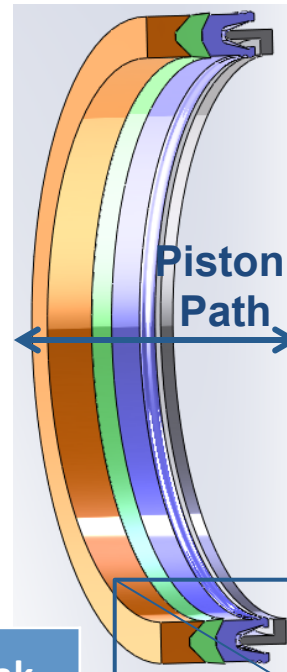


Accomplishments and Progress: Dynamic Seal Design/Analysis

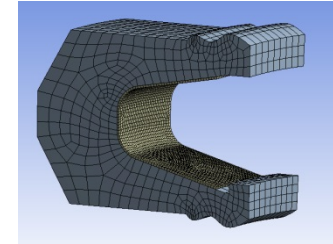
A two step analysis was performed:

1. FE analysis of seal under range of expected pressure conditions to determine how gap size varies & seal deforms
2. Reynold's equation coupled with spring representation of seal to predict the leakage rate

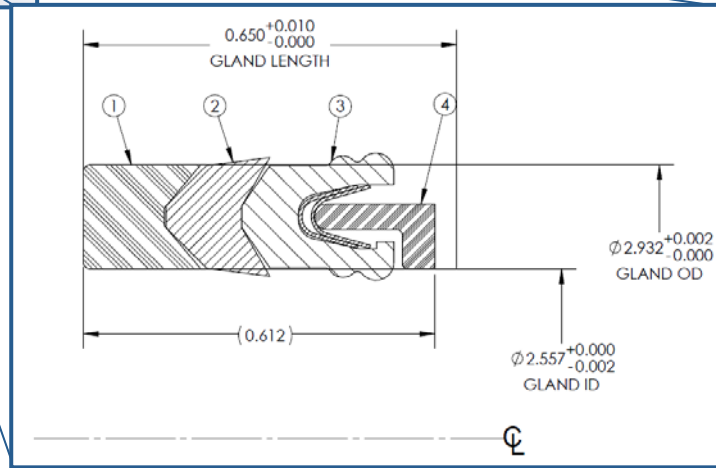
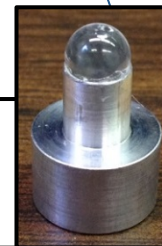
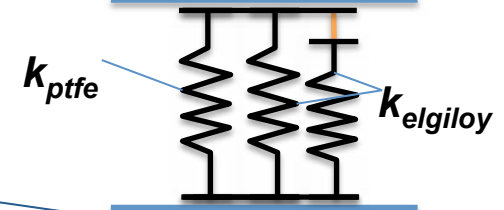
Predicted seal leak rate is acceptable:



Finite-Element Model



Reduced Spring Model

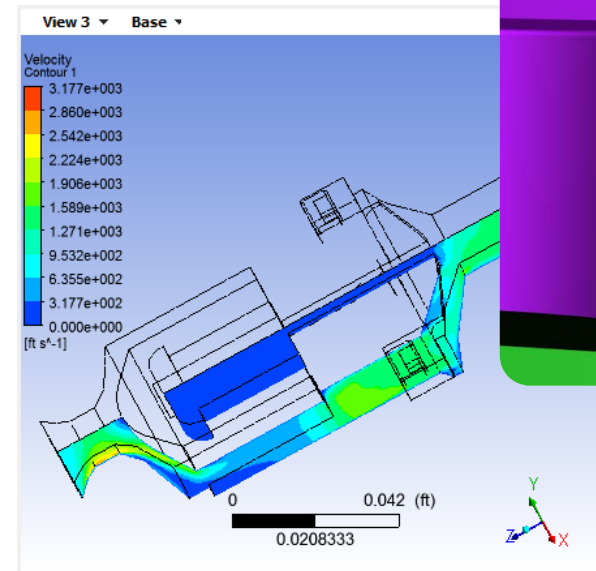
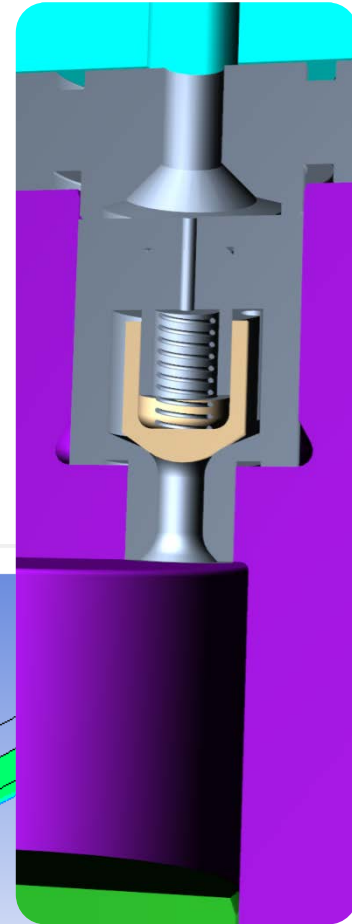
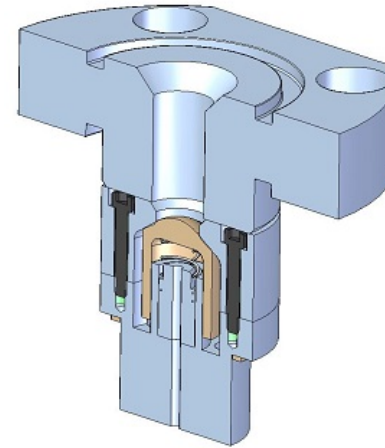


| Stage | Individual Seal Leak Rate (g/hr) | Individual Seal Leak Rate (% of full flow) |
|-------|----------------------------------|--|
| 1 | 1.1 | 0.01 |
| 2 | 8.0 | 0.08 |
| 3 | 35 | 0.35 |

Ceramic seal and tentatively a DLC poly seal are alternatives

Accomplishments and Progress: Valve Selection/Design

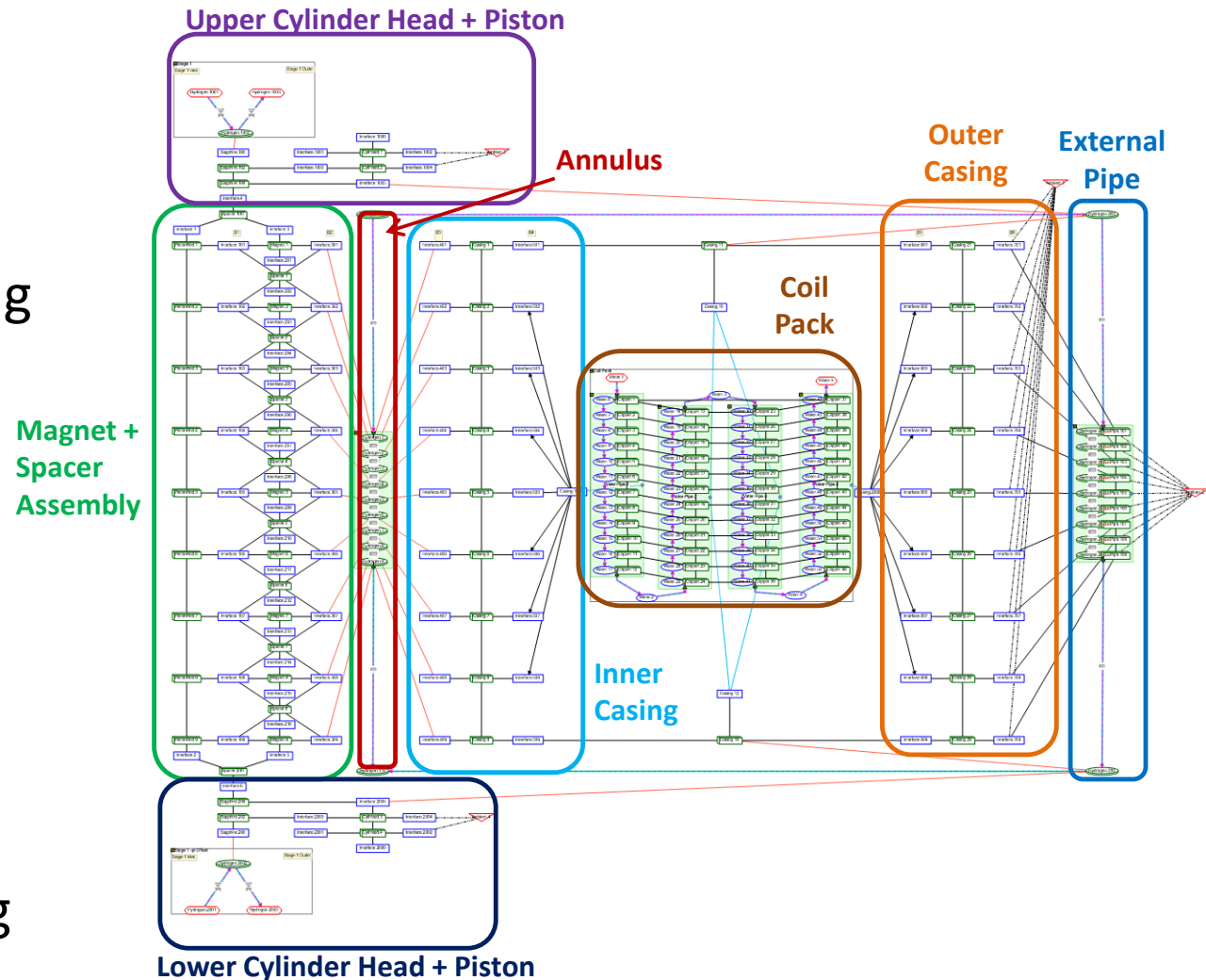
- Market search determined that major manufacturers do not have any products that fit the desired operating conditions
- ACI has experience designing and building replacement and custom compressor valves
- The compressor design has a low throughput & tight space constraints therefore a single poppet valve has been identified as a solution
- Stages 1, 2, and 3 valves are designed and fine-tuned with performance analysis



Accomplishments and Progress: LMRC Cooling System Design

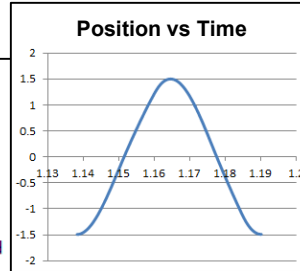
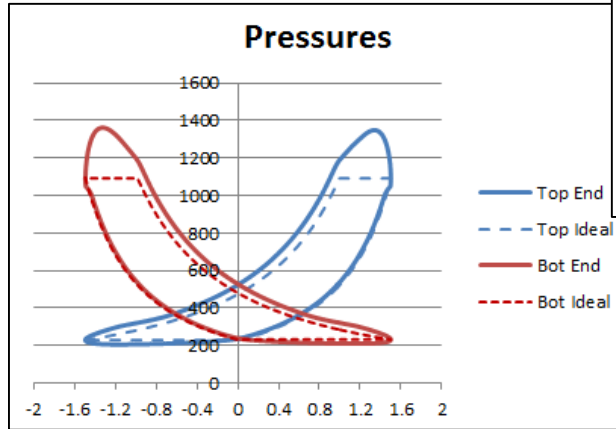
Coil cooling

- Average value of 560A will be traveling through the coils
- Therefore a conjugate heat transfer model (SINDA/FLUINT) was used to determine conditions required for adequate cooling



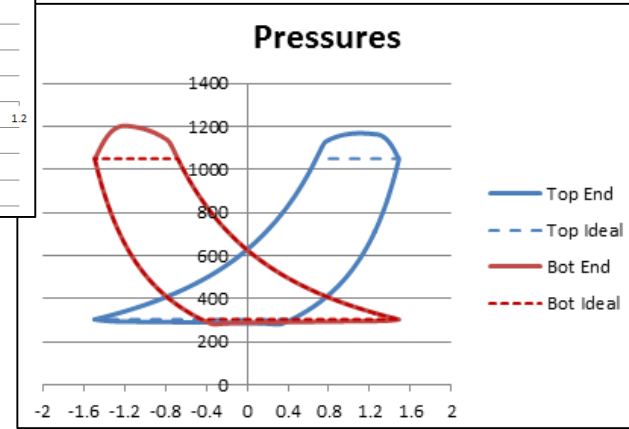
Accomplishments and Progress: Performance Prediction/Control Scheme

Original Valve



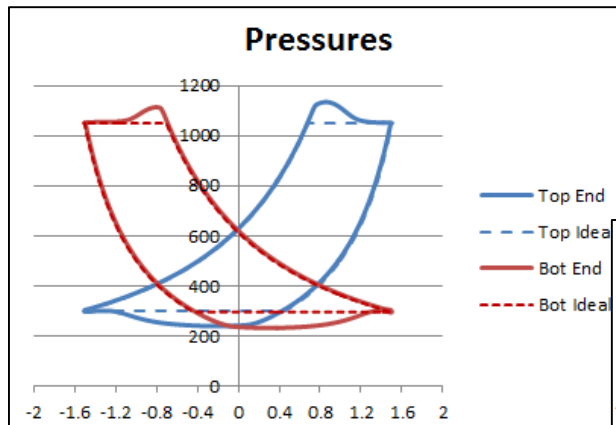
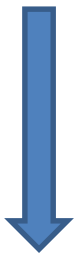
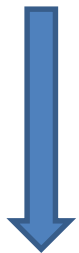
Max Force Scheme (22 cps)

New Valve

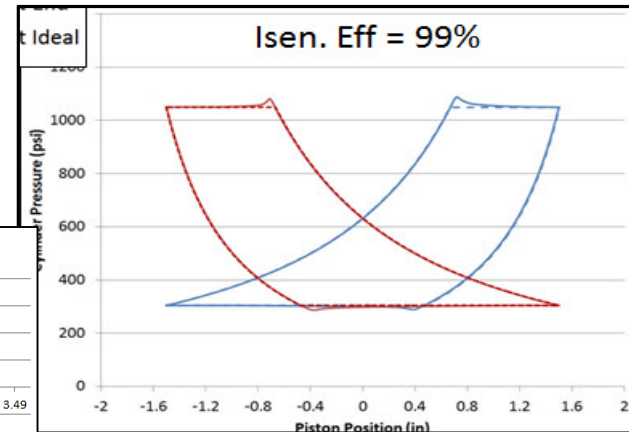
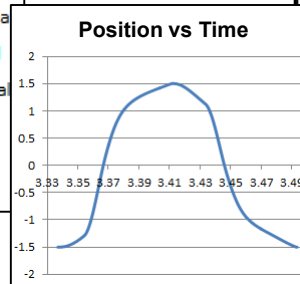


Isen. Eff 89%

Isen. Eff 73%



Custom Scheme (6 cps)



1st Stage Isen. Eff 99%

Target is > 95%

97% 2nd Stage, 97% 3rd Stage

Accomplishments and Progress: System Efficiency and Specific Energy

- LMRC predicted efficiency & specific energy:
 - 20% overall 3 stage (and 20% per stage)
 - 9.2 kWh/kg overall (2.8 to 3.5 kWh/kg per stage)
- Could be > 90% by implementing design improvements
 - Move coils to inside of casing.
 - Locate coils as close as possible to the magnets.
 - Increase # of rows of coils (predictions indicate this is only useful after moving coils closer to magnets)
 - Use superconducting coils. (This may require complex additional system to keep the coils super cold.)
 - Further optimization of control scheme.
- ~1.3 kWh/kg is expected with advanced LMRC actuator design & 100 bar inlet pressure (1.6 is 2015 MYRDD target)

Accomplishments and Progress:

Full Scale (100 kg/hr) Cost and Life Estimates

- 3 LMRCs in parallel per stage = 9 LMRCs total
- operating at ~930 cpm with ceramic seals

| | Conventional Reciprocating Compressor Technologies | LMRC |
|-----------------------|--|--------------------------------|
| Seal Life | 12-18 months | 48 months (ceramic)* |
| Packing Life | 3 years | Infinite (NO PACKING) |
| Valve Life | 1-3 years | 4 years |
| Isentropic Efficiency | 2015 goal > 73%, 2020 goal > 80% | 80% for all 3 stages in series |
| O&M Cost | 2015 goal < \$10,000/year, 2020 goal < \$4,800 | \$3,300 / year |
| Mnfactr Cost | 2015 goal < \$400,000, 2020 goal < \$240,000 | \$284,000** |

2015 and 2020 goals are from the 2012 MYRD&D plan per the goals of the project contract

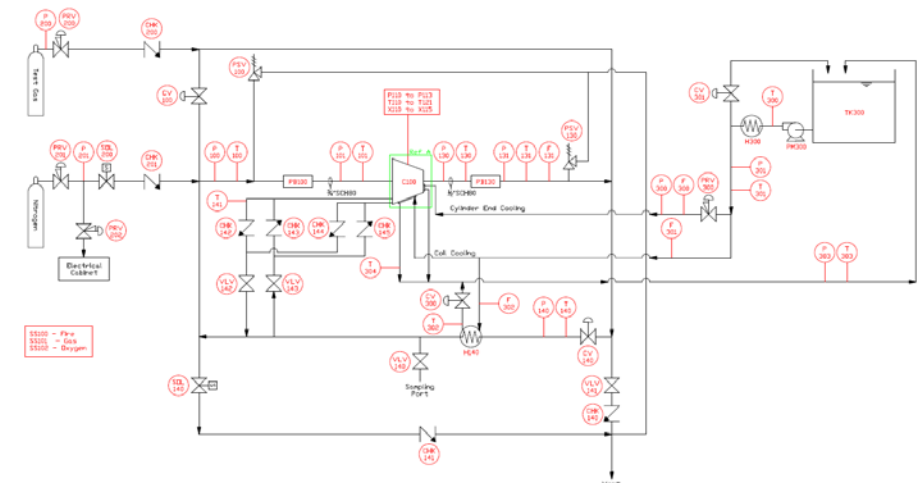
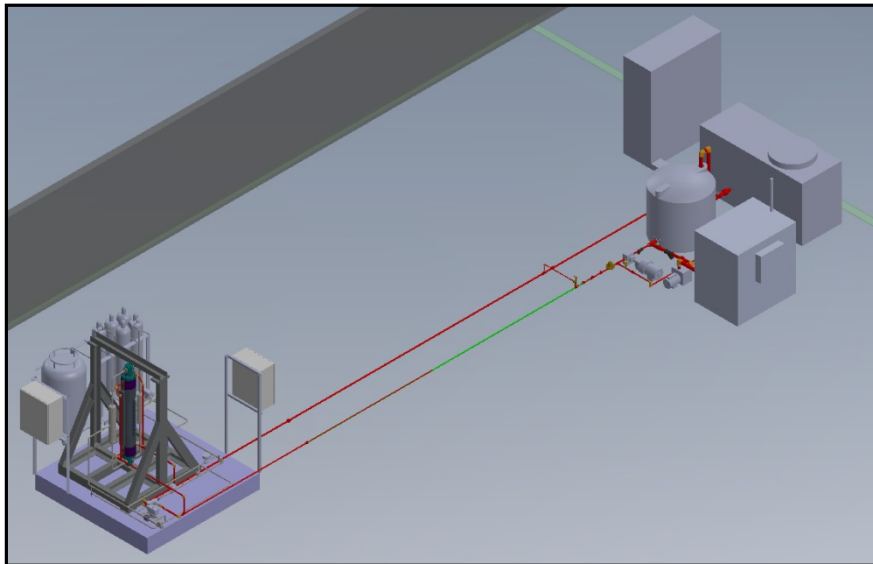
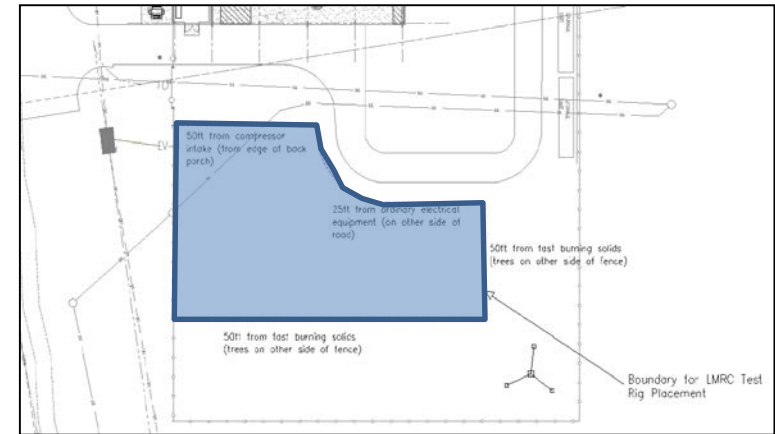
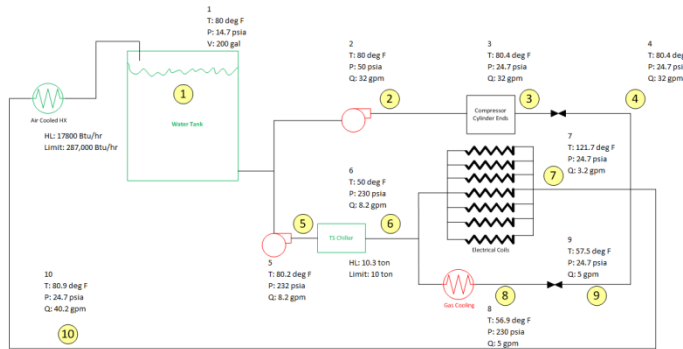
* Assumes operation time is ~1/4 of a 24 hour day

** Includes inter-stage piping and coolers. Assumes ~100 units built per year. 2007\$ like targets

The most understood path to 100 kg/hr was used. Larger may be better, but harder to quantify. Also, overall system efficiency gains (design change) should significantly reduce the cost per LMRC.

Accomplishments and Progress: Test Loop Design

- After review of OSHA, Occupancy classification letter filed with City of San Antonio, and SwRI requirements, test stand will be located outside building with required electrical supply
- P&ID
- 3D model



Accomplishments and Progress: Responses to Previous Year Reviewers' Comments

- Cost analysis requested – Described in a previous slide
- Flow rate questioned – Calculations described in quarterly reports
- Thermal management questioned – Described in a previous slide
- H₂ inside of magnets chamber? – Yes, intentionally
- Dynamic seal leak rate questioned – predictions acceptable per detailed analysis
- Control system required to manage power delivery questioned – power controller from electric automotive industry

Collaborations

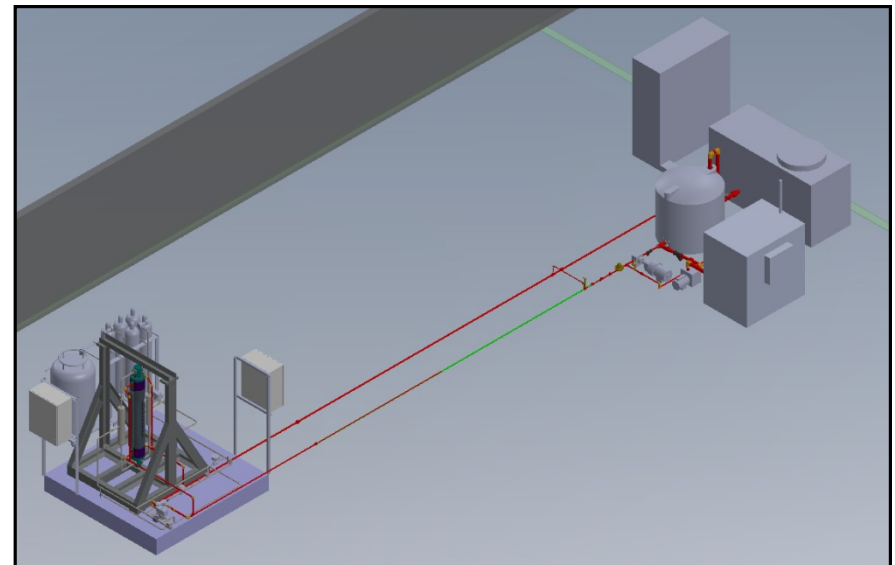
- DOE – Sponsor, Steering
- SwRI – Project lead, design, location for testing
- ACI Services – Overall project partner, lead for mechanical design, fabricator of some parts
- Thar Energy – Project partner, seal and ceramic piston design
- Dexter Magnetic Technologies – Neodymium Iron Magnets
- TechniCoil – Coils and winding
- Enterprise Power Corp. – Power Supply/Controller

All major suppliers/manufacturers are in the USA

- **Challenge:** Seal life
- **Resolution:** Ceramic seal and tentatively a DLC poly seal are alternatives
- **Challenge:** Maintaining budget
- **Resolution:** Weekly budget re-evaluations and borrow test equipment to leverage benefit of large SwRI testing community
- **Challenge:** Full scale production cost target
- **Resolution:** Investigate further the possibilities of increasing the LMRC size instead of speed & numbers

Proposed Future Work

1. Parts Fabrication
2. Test Loop Construction
3. Commissioning
4. Testing
5. Data Analysis
6. BP3 – Fabricate stages 2 and 3 then test stages 2 and 3 in series with stage 1



Summary

- BP1 complete = Stage 1 overall design complete
- Efficiency predictions greater than 95%
- Fabricating and purchasing parts/components
- Currently no technical/commercial off-ramp issues identified

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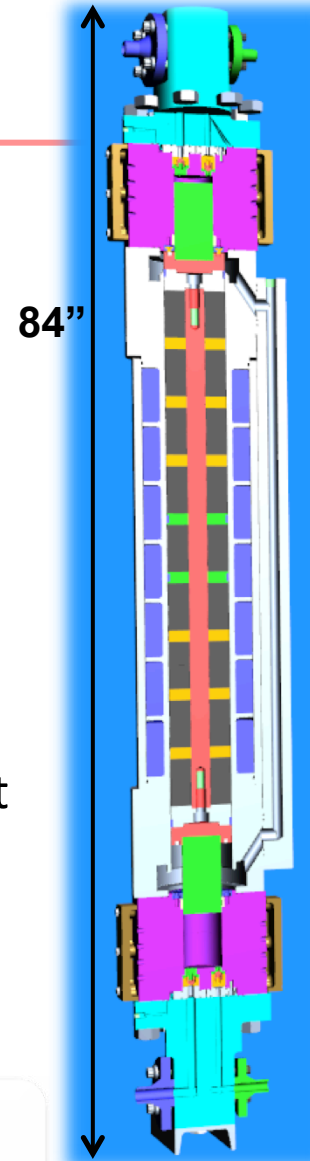
Questions?

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Emeritus

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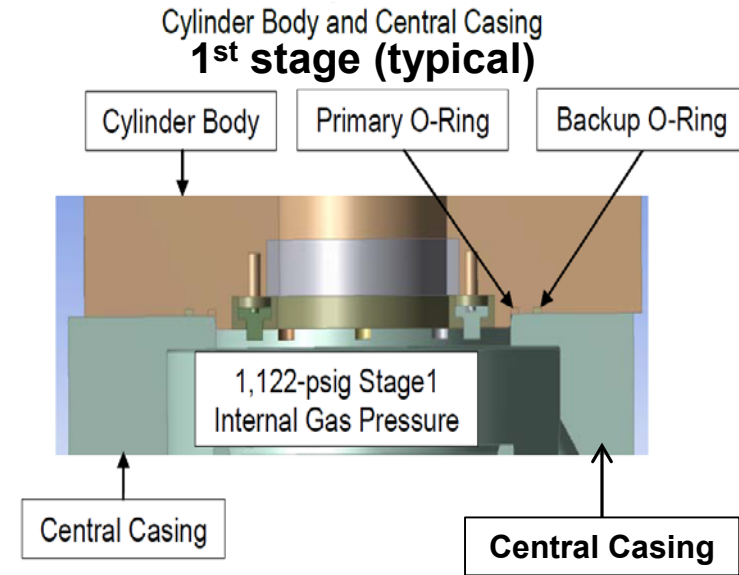
Technical Backup Slide

Seal Selection Criteria:

1. Face seals with zero gap for all primary & secondary (back-up) seal locations
2. Impermeable & resistant to 100% hydrogen gas
3. Explosive decompression resistant

Approved by T. Anderson; Application Engineering
Parker Hannifin O-Ring Division

**** outer seal will be V1238-95 Fluorocarbon due to lower pressures**



| Stage | Max. Internal Operating Press. (psig) | Temp. Range (°F) | | | | |
|-------|---------------------------------------|------------------|------------|--------------------------|-----------------|---------------------|
| | | | Size (in.) | Material | Manufacturer | Durometer (Shore A) |
| 1 | 1,125 | -15 to 400 | 3/32 | V1238-95 Fluorocarbon | Parker Hannifin | 95 |
| 2 | 4,101 | -15 to 400 | 3/32 | V1238-95 Fluorocarbon | Parker Hannifin | 95 |
| 3 | 14,069 (inner seal**) | -15 to 400 | 1/8 | Inconel 718 w/gold plate | Parker Hannifin | NA |

Technical Backup Slide

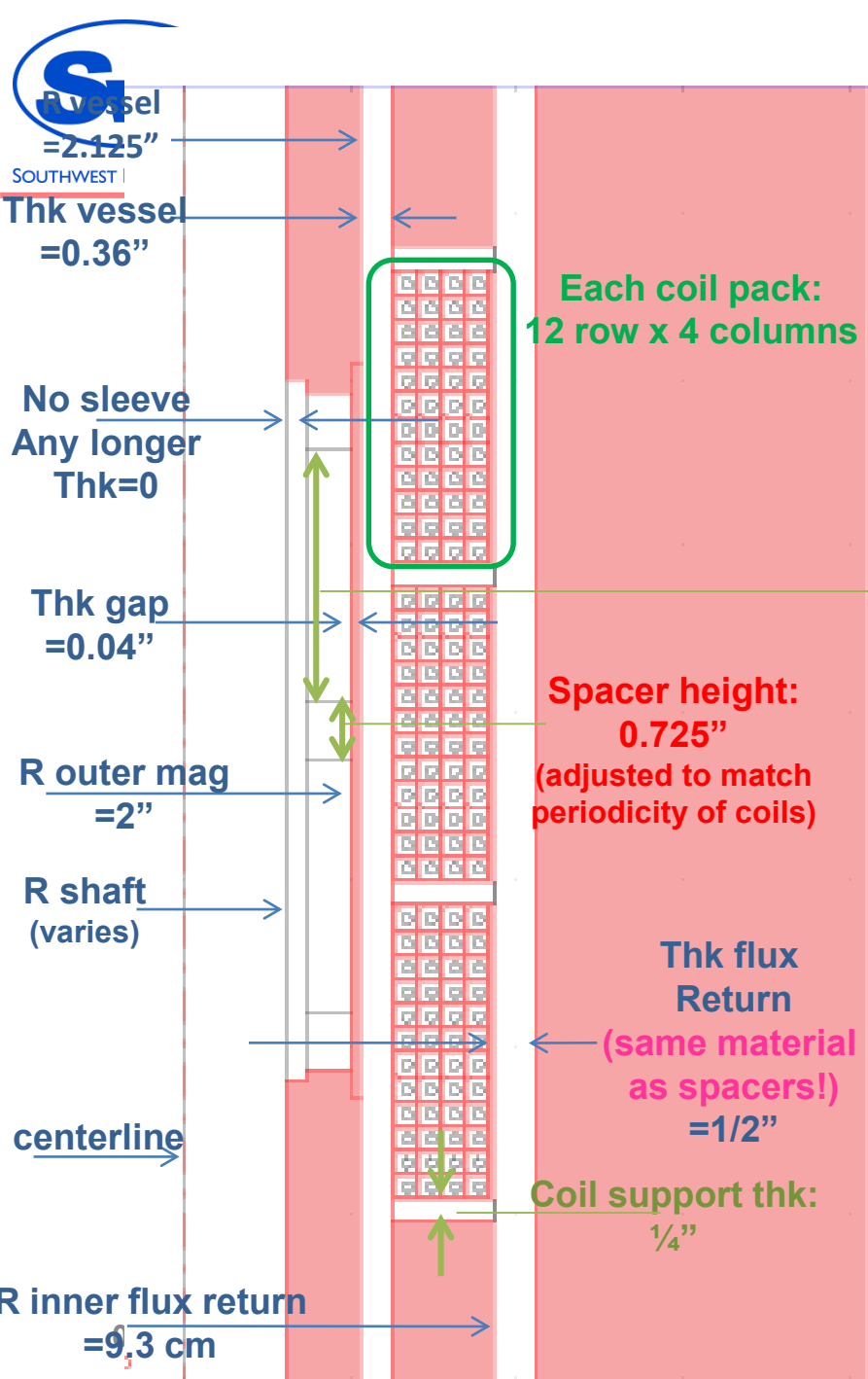
Materials selected for each of the compressor components, and the significant mechanical and physical properties for each

| COMPONENT | MATERIAL | TENSILE STRENGTH | YIELD STRENGTH | ENDURANCE STRENGTH | MAGNETIC PROPERTIES | COEFFICIENT OF EXPANSION (77-212 °F) (IN / IN / °F) | YOUNG'S MODULUS | INFORMATION SOURCE |
|---|---|---|-------------------|----------------------|--|---|--|--------------------|
| Central Casing | A-286 Sol & Age(AMS 5737P) | 145 ksi | 95 ksi | 61 ksi | Non-Magnetic (1.007Mu) | 9.17 x 10 ⁻⁶ | 28.8 x 10 ⁶ psi | 1,2,7 |
| Magnet Spacers | AISI M1010, 1010 hot rolled bar or AISI 1018 hot rolled bar | 47 ksi 69 ksi | 26 ksi 47 ksi | 21 ksi 31 ksi | Magnetic (3290Mu) Magnetic (2540Mu) | 6.78 X 10 ⁻⁶ 6.50 X10 ⁻⁶ | 29 X 10 ⁶ psi 29 X 10 ⁶ psi | 3,4,5,15 |
| Piston Rod | A-286 Sol & Age(AMS 5737P) | 145 ksi | 95 ksi | 61 ksi | Non-Magnetic (1.007Mu) | 9.17 x 10 ⁻⁶ | 28.8 x 10 ⁶ psi | 1,2,7 |
| Magnet Retainer | AISI M1010, 1010 hot rolled bar or AISI 1018 hot rolled bar | 47 ksi 69 ksi | 26 ksi 47 ksi | 21 ksi 31 ksi | Magnetic (3290Mu) Magnetic (2540Mu) | 6.78 X 10 ⁻⁶ 6.50 X 10 ⁻⁶ | 29 X 10 ⁶ psi 29 X 10 ⁶ psi | 3,4,5,15 |
| Piston Holder | Incoloy 903 Sol & Age or Carpenter CTX-1 | 190 ksi | 160 ksi | 68 ksi | Magnetic | 4.0 x 10 ⁻⁶ 4.19 X 10 ⁻⁶ | 21.35 x 10 ⁶ psi | 6,14 1 |
| Piston Holder Alternate Mat'l | Kovar K-Alloy K94610 ASTM F-15 Temper A | 75 ksi | 40 ksi | NA | Magnetic | 3.3 X 10 ⁻⁶ | 20.0 X 10 ⁶ psi | 1,6 |
| Piston | Ceramic (95% Zirconia, 5%Yttria) | 36 ksi | NA | NA | NA | 5.8 x 10 ⁻⁶ | 30 x 10 ⁶ psi | 16 |
| Cylinder | A-286 Sol & Age(AMS 5737P) | 145 ksi | 95 ksi | 61 ksi | Non-Magnetic (1.007Mu) | 9.17 x 10 ⁻⁶ | 28.8 x 10 ⁶ psi | 1,2,7 |
| Head | AISI 316 Annealed | 85 ksi | 36 ksi | 29 ksi | Non-Magnetic (1.008Mu) | 8.89 x 10 ⁻⁶ | 28 x 10 ⁶ psi | 3,18 |
| Suction/Discharge Valves | A-286 Sol & Age(AMS 5737P) | 145 ksi | 95 ksi | 61 ksi | Non-Magnetic (1.007Mu) | 9.17 x 10 ⁻⁶ | 28.8 x 10 ⁶ psi | 1,2,7 |
| Rider Bands | PEEK (PTFE filled) | | | | | | | |
| Thar Seal Rings | Filled PTFE | | | | | | | |
| Thar Seal Springs | Elgiloy (Cold Drawn & aged) | 350/220 ksi | NA | NA | Non-Magnetic | NA | 29.5 x 10 ⁶ psi | 8 |
| Seal Retainer Bolting | AISI 316 ASTM F593 Gr 2 Cond.CW | 100 ksi | 65 ksi | 34 ksi | Non-Magnetic (1.008Mu) | 8.89 x 10 ⁻⁶ | 28 x 10 ⁶ | 22 |
| Valve Springs or Piston Travel Stop Springs | Elgiloy (Cold Drawn & aged) or MP35N (Cold Drawn & aged) or AISI 316 (Cold Drawn) | 350/220 ksi 330/230 ksi 245/110 ksi | NA NA NA | NA NA NA | Non-Magnetic Non-Magnetic Non-Magnetic (1.008Mu) | NA NA NA | 29.5 x 10 ⁶ psi 34 x 10 ⁶ psi 28 x 10 ⁶ psi | 8 8 8,3 |
| Valve Poppets | PEEK (Unfilled) | 13-15 ksi | NA | NA | NA | 26.7 x 10 ⁻⁶ | NA | 20,21 |
| Valve Nose Gasket | Cooper (OFHC)C10200/C10100 | 31.9 ksi | 10 ksi | NA | Non-Magnetic (0.999Mu) | NA | NA | 3,17 |
| Valve Retainer | A-286 Sol & Age(AMS 5737P) | 145 ksi | 95 ksi | 61 ksi | Non-Magnetic (1.007Mu) | 9.17 x 10 ⁻⁶ | 28.8 x 10 ⁶ psi | 1,2,7 |
| Cylinder Cooling Jacket | Aluminum 6061-T6 | 40 ksi | 35 ksi | 12.4 ksi | Non-Magnetic (1.000 Mu) | 13.1 x 10 ⁻⁶ | 10.0 x 10 ⁶ psi | 9,10,17 |
| Coil Housing | Ferritic Ductile Iron Casting ASTM A536 Gr. 60-40-18 | 60 ksi | 40 ksi | 27 ksi | Magnetic (1500Mu) | 6.5 x 10 ⁻⁶ | 24.5 x 10 ⁶ psi | 11,12 |
| External Bolting | Alloy Steel A193-B7 | 125 ksi | 105 ksi | 61.2 ksi | Magnetic | 6.78 X 10 ⁻⁶ | 29.7 x 10 ⁶ psi | 14,3 |
| Bolting for Piston Holder & Magnet Retainer | 17-4PH H1150-D or 17-4PH H1150-M | 125 ksi 115 ksi | 105 ksi 75 ksi | 62.5 ksi 57.5 ksi | Magnetic Magnetic | 6.6 X 10 ⁻⁶ 6.6 X 10 ⁻⁶ | 28.5 X 10 ⁶ psi 28.5 X 10 ⁶ psi | 1,3 1,3 |

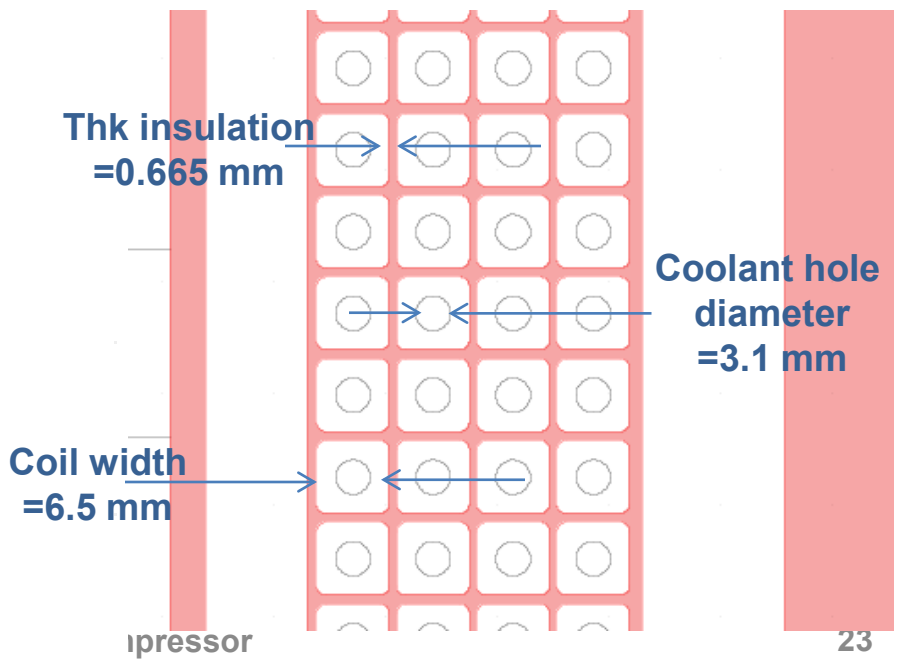
- 1 - Carpenter Steel Corp. Data Sheet
- 2 - AMS 5737P Standard for A-286
- 3 - MatWeb
- 4 - Ryerson Data Book
- 5 - ASM Metals Handbook
- 6 - Special Metals Co. Data Sheet
- 7 - "Physical Properties Data Compilations Relevant to Energy Storage - V Mechanical Properties Data", HM Ledbetter, NSRDS, Jan. 1982
- 8 - Suhm Spring Works Data Book
- 9 - AMS 4027N Standard (Aluminum Alloy Sheet and Plate)
- 10 - Alcoa Aluminum Handbook
- 11 - Iron Castings Handbook (Iron Castings Society)
- 12 - ASTM A536 Standard (Specifications for Ductile Iron Castings)
- 13 - ASTM B152 Standard (Copper Sheet, Strip, and Plate)
- 14 - ASTM A193 B7 Standard (Alloy Steel & Stainless Steel Bolting)
- 15 - Yeadon Handbook of Small Electrical Motors (Soft Magnetic Materials Properties)
- 16 - Thar and <https://www.ceramicindustry.com/ext/resources/pdfs/>
- 17 - Clark, R. "Magnetic Properties of Materials"
- 18 - AZO Materials Web Site
- 19 - "A Silicon - Containing, Low-Expansion Alloy with Improved Properties", DF Smith and JS Smith, Huntington Alloys
- 20 - MakeltFrom.com, Materials Properties
- 21 - Victrex - PEEK Data Sheet
- 22 - ASTM F593 Standard Gr.2 Cond. CW (Specification for Stainless Steel Bolts)

Technical Backup

Slide: Actuator Design

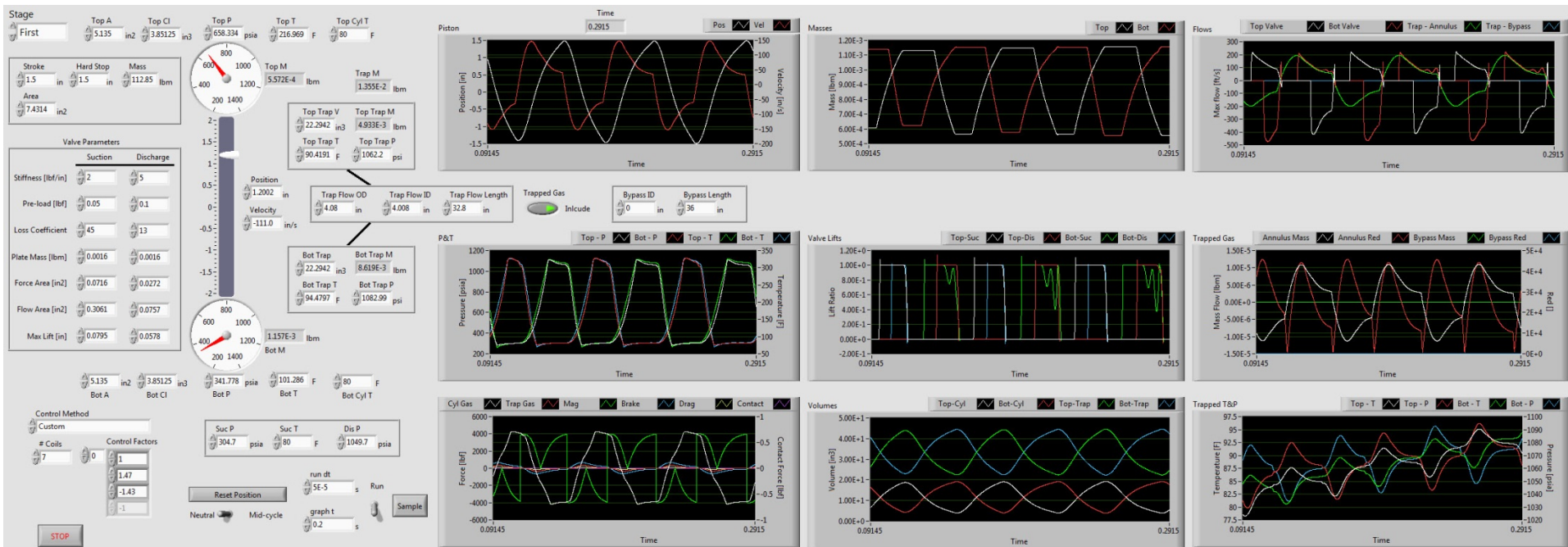


Magnet height:
3"



Technical Backup Slide

Control panel for developing control schemes while simulating LMRC motion and predicting performance (+ many other system characteristics)



Seal-Sapphire COF Determination

- It was determined through pin-on-disk testing that the coefficient of friction (COF) for sapphire on PEEK is 0.15
- Due to the higher than expected COF, two other seal options are planned for testing
 - Poly seal with DLC
 - Sapphire or ceramic seal (~0.0001"-0.0005" clearance)

