

Flowing Particle Bed Solarthermal Redox Process to Split Water

PI: Alan W. Weimer

Ibraheam Al-Shankiti, Caitlin Czernik, Hans Funke, Arto Groehn, Amanda Hoskins, Samantha L. Millican, Scott Rowe, Ryan Trottier, Mark Wallace, and Charles B. Musgrave

University of Colorado at Boulder

Judy Netter, NREL

Jennifer Walsh, CoorsTek

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Overview: Year 3 of 3-Year Project



Timeline

Project Start Date: 9/1/2014 Project End Date: 11/30/2017

% Complete: 87%

Paid Partners

National Renewable Energy Laboratory (NREL), Golden, CO

• Solar testing facility and capabilities

Allan Lewandowski Solar Consulting, LLC

• Solar field design consultation and modeling

Musgrave Group*, CU Boulder

 Active materials discovery and DFT modeling (*NSF/DOE Funding – joint FOA)

TRL 2 \rightarrow TRL 3

Technical Barriers Addressed

- S. High-temperature robust materials
- W. Materials and catalysts development
- X. Chemical reactor development and capital costs

Collaborators

Australian National University (ANU), Canberra, AU

• Reactor models and receiver testing at solar simulator facility

Saudi Basic Industries Corporation (SABIC)

- Supplying equipment and materials characterization <u>Coorstek/Ceramatec</u>
- Preparation of large spherical active materials
- High temperature O₂ transport membrane

Budget

Total project funding: \$2,000,000 Sub-contract to NREL: \$450,000 Total recipient cost share: \$6,250 Total funds received FY16: \$687,055 Total planned FY17: \$455,901

Relevance: Renewable Efficient Hydrogen Generation



Project Objective: Design and test individual components of a novel flowing particle solarthermal water splitting system capable of producing 50,000 kg H_2 /day at a cost < \$2/kg H_2

- Identify and develop high-performance active material formulations
- Synthesize flowable, attrition-resistant, long-use spherical particles from low-cost precursors
- > Demonstrate high-temperature tolerant, refractory, non-reactive containment materials
- Construct fluidized bed particle redox test system and test components of system
- Monitor progress toward cost target by incorporating experimental results into frequently updated detailed process model and H2A
- On-sun production for a full solar day
- Move from TRL 2 to TRL 3

This Reporting Period:

- ✓ Performed long-term stability tests of reactive materials showing no loss in reactivity between 100th and 200th cycle and 2X targeted H₂ production rate(Barrier S)
- ✓ Developed ALD barriers that improve high-temperature resistance of SiC to steam by >60%, 2X targeted impact (Barrier S)
- \checkmark Demonstrated on-sun production of 1.91L standard L H₂ in less than 3 hours (Barriers S and X)
- ✓ Assessed economic viability of thermal energy storage to provide electricity for nonintermittent STWS (Barrier X)
- ✓ Completed study on effects of structure and magnetic ordering for 1343 materials (Barrier W)
- \checkmark Continued testing of high temperature O₂ transport membrane for inert gas recycle (Barrier X)
- ✓ Completed construction of high-flux solar simulator to test hybrid reactor concept (Barrier X)

Approach:

Iterative Materials and Reactor Development



Reactive Materials

Produce and characterize reactive materials

- M1.2: Optimize perovskite and spinel material formulations (65% done)
- M1.4: Produce attrition resistant active materials (100% done)
- GNG1: Spray dried particles making ≥150 µmol H₂/g (100% done)
- GNG2: Particles that produce ≥150 μmol H₂/g and lose ≤10% reactivity from 100th to 200th cycle (100% done)

Containment Materials

Efficient, Cost-effective H₂ Production

Ongoing updates to the process model and H2A

Construct particle flow system to test reactor design

Reactor

Design

- M3.2: Evaluate diffusional limitations under inert gas with O₂ membrane (100% done)
- M3.3: Develop diffusional model for oxygen removal (30% done)
- M3.4: Operate reactor as a fluidized bed (80% done)
- GNG4: Operate particle flow redox system with >1g of active material (100% done)

On-Sun Production

Production of H₂ with reactive engineered particles (80% done)

Develop redox compatible containment materials

- M2.1: Synthesis and characterization of coated SiC powders (80% done)
- M2.2: Selection of preferred coating material based on TGA results (80% done)
- M2.4: Coated containment tube system constructed (100% done)
- GNG3: Coated SiC with ≥25% reduction in steam reactivity (100% done)

Accomplishments and Progress: Overall Process R&D





Multiple Fluid Beds in Solar Cavity (near-isothermal)

processing".

Accomplishments and Progress: Near-Isothermal **Process Design**

- Hybrid solar/electrical ٠ reactor for nonintermittent heating, 10 hr/d
- Renewable, storable ٠ electricity provided by heated molten salt using • recuperated heat
- Membrane electricity calculated; experimental efficiency of 12%

redox

Bed 1

Fluidized

Solar Cavity Receiver

Heat Recuperation

Inert/O₂

e-

Inert

Blower

ITM

SEOS

02

- Redox reactors operate as fluidized beds within solar cavity
- No solids movement between reactors, simple design
- Reduction and oxidation occur at near 1450°C
- 3L H₂/8hr at NREL HFSF using Hercynite active materials

Make-up

Steam

H₂O

recox Flu dized

Bel 2

 H_2/H_2O

Pump





Accomplishments and Progress: Temperature-Swing Process Design

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- Continuous flowing particle bed hydrogen production process
- Solar radiation on reduction reactor only
- Reduction occurs at 1450°C
- Oxidation occurs at 1000°C
- Experimental implementation underway using 12 kW solar simulator at CU (pictured)
- 3L H₂ in 8 hours using Hercynite





Accomplishments and Progress: H2A Results





\$1.80 \$1.90 \$2.00 \$2.10 \$2.20 \$2.30 \$2.40 \$2.50 \$2.60

Near-Isothermal



Cost Drivers	2015	2020	Ultimate
Heat exchanger effectiveness	85%	90%	95%
SiC material factor	6	5	3
Replacement frequency (years)	2	5	5
Material activity (µmol H_2/g)	354	389	425
Enthalpy of reaction (kJ/mol)	384	346	307
Heliostat cost (\$/m ²)	\$140	\$75	\$75
Hybrid Reactor Mark-up	1.5x	1.5x	1.25x
Cost H ₂ Near-Isothermal (\$/kg)	\$8.79	\$3.51	\$2.00
Cost H ₂ Temperature- Swing (\$/kg)	\$7.42	\$2.61	\$1.98

TEA predicts that NI and TS processes can produce $\rm H_2$ at \$2.00 /kg, and \$1.98/kg, respectively

\$1.80 \$1.90 \$2.00 \$2.10 \$2.20 \$2.30 \$2.40 \$2.50 \$2.60

Go/NoGo: Active Materials Robustness



Temperature [°C]



Accomplishments and Progress: Kinetic Modeling



Diffusion in Hercynite



Impact of Inversion on Local Environment

Increasing Inversion

- Cation distribution in hercynite has a significant impact on the diffusion barrier
- Barrier shows strong correlation to both the oxygen vacancy formation energy, and the number of Fe cations that neighbor the diffusion site

Linear Relationship Between Oxygen Vacancy Formation **Energy and Diffusion Barrier**



Findings show promise for modeling of disordered systems without explicit calculations for every state.

Go/NoGo: SiC Steam Oxidation Resistance





- Particle ALD is being used to study the stabilization effects of nano-scale diffusion barriers with atomic growth control
- Mullite (3Al₂O₃:2SiO₂) and BN have been identified as a promising coating materials
- H₂O exposure at 1000°C for 20 hours
- Increased film thickness improves performance
- Mullite films are able to match performance of alumina
- Preliminary BN films show reduced oxidation similar to alumina

ALD coatings show up to a 64% improvement to the oxidation resistance of SiC.

Accomplishments and Progress: Modeling for Coating Stability Analysis

Energy (eV/atom)





- Key metrics used to compare materials:
 - O/N vacancy formation energy
 - Oxygen hopping energy barriers
- We have performed calculations comparing mullite to bulk alumina, as well as a variety of materials receiving interest in EBC applications
 - 2 materials have been computationally determined to perform better that BN





Computational results match well with experiments and have revealed metrics by which to theoretically screen barrier materials.



ITM SEOS Membrane Results

- Solar-to-H₂ thermodynamic efficiency calculations showed the separation efficiency (η_{sep}) of inert gas and generated O₂ needs to be at least 10% to have an efficient process.
- Tested a high temperature (850°C) Ion Transport Membrane (ITM) to remove O₂ from inert gas
- Compared energy requirement of separation to thermodynamic separation work to calculate η_{sep}
- Experimental energy requirements are inflated to include thermal-toelectricity conversion (η_{solar-to-electricity})





 O_2 concentration reduced to 15ppm from 1% O_2/N_2 mixture at 1 SLPM using ITM SEOS with 29% η_{sep} (12% including thermal-to-electricity conversion)



Accomplishments and Progress: Hercynite Materials Characterization

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- Hercynite is formed by reacting Al₂O₃ and Fe₃O₄ to form the spinel phase
- $Fe_3O_4 + 3Al_2O_3 \rightarrow 3FeAl_2O_4 + \frac{1}{2}O_2$ (R1)
- Hercynite materials is further reduced under O₂ vacancy mechanism
- $FeAl_2O_4 \rightarrow FeAl_2O_{4-\delta} + \frac{\delta}{2}O_2$ (R2)
- Apparent activation energies for R1 and R2 reactions were experimentally calculated using isoconversional methods
- XRD and TG analysis showed spinel phase is maintained after H₂O and CO₂ oxidation



Undoped hercynite undergoes an O₂ vacancy mechanism up to 1700 °C



Accomplishments and Progress: On-Sun Testing



Data Summary for test on April 13 th , 2017					
	Activity (µmol/g)	Total H ₂ (μmol)	Total H ₂ (L)	Peak Rate (µmol/g/s)	Oxidation Time (s)
Oxidation 1	367	29336	0.66	0.59	1316
Oxidation 2	697	55711	1.25	0.84	2010
Tot	al H_2 for 2	cycles (L)	1.91	Time 2 cycles (h:mm:ss)	2:45:26
Expec	ted H ₂ for	4 cycles (L)	3.81	Expected Time 4 cycles (h:mm:ss)	5:30:52





After producing 1.91L H_2 in less than 3 hours, we are on-target to meet our end-of-project goal of 3L H_2 production in less than 8 hours Summary



- New process models using hybrid solar/electric reactors evaluated
- GNG of H_2 production of 150 μ mol/g/cycle and less than 10% loss in reactivity met (~300 μ mol H_2 /g/cycle and no loss between 100th and 200th cycle)
- Method of kinetic modeling of hercynite systems improved
- ALD coatings show up to 64% improvement in oxidation of SiC in steam environment (target was 25% improvement)
- Computational results for SiC coating stability match experimental results
- O₂ concentration reduced to 15ppm from 1% O₂/N₂ mixture at 1 SLPM using ITM SEOS with 12% η_{sep} including electricity use
- 1.91L H₂ made during 3 hours of testing at NREL's HFSF, showing significant progress toward end-of-project goal



"It is recommended that the researchers improve the kinetics to decrease the cycle time."

Fast kinetics and cycle time is one of many parameters that can have a profound impact on the technology's economic feasibility. We are examining the effect of dopants on kinetics with our NSF sister project, in addition to performing experiments to determine the kinetics of various materials. It is possible, perhaps even likely, that the material with the fastest kinetics will not be the best overall, therefore we must consider productivity, durability and other characteristics in addition to kinetics.

"The H2A analysis in 2015 indicated that heat exchanger effectiveness was by far the most critical factor in the final economics. This technical challenge seems to not have received attention."

Heat exchanger effectiveness was found to have a smaller impact on the overall H₂ cost than any of the other variables presented in the tornado chart. This can be explained by the substantial efficiency advantage conferred by using recycled inert sweep gas and a high-temperature O₂ transport membrane. These two updates to the Aspen simulation make heat exchanger effectiveness a less important factor.

"Given the proposed size of the reactors, they need to present compelling evidence (examples) that atomic layer deposition (ALD) can be economically done on a system of this size, shape, etc."

The process of ALD is independent of line-of-sight, so wherever precursor gas can flow surfaces can be coated. Therefore, one can easily coat the inside of tubes that can be heated. The time and precursor requirements for ALD are largely controlled by the surface area of the substrate making ALD highly scalable. For example approximately 60 m² are loaded into the lab-scale fluidized bed ALD reactor and a commercial tube might have an internal surface area of approximately 30 m². This is not a concern.

Collaborations



Fund-Receiving Collaborator		Project Roles	
NATIONAL RENEWABLE ENERGY LABORATORY	National Renewable Energy Laboratory (NREL) (sub)	High Flux Solar Furnace (HFSF) user facility for process demonstration	
	Musgrave Group, CU Boulder	Active materials discovery and DFT modeling through "sister" NSF project*	
		* Funds from Joint DOE/NSF FOA	
Leveraged Collaborators (no funds from DOE)		Project Roles	
بیبابک عاداه	Saudi Basic Industries Corporation (SABIC)	Materials characterization support; supplying equipment	
COORSTEK Amazing Solution		Active Materials Preparation; ITM SEOS Membrane	
Harper	Harper International Corporation	Design and construction of pilot high- temperature solar/electric furnace	
Australian National University	Australian National University (ANU)	Reactor models and receiver testing at solar simulator facility	

Proposed Future Work*

- Reactive Materials
 - Perform detailed thermodynamic and kinetic studies of active materials (M1.3 & M1.6)
 - Validate computation work of sister NSF project (M1.1 & M1.2)
 - Poster PD120
- Reactor Design
 - Operate reduction reactor tube under vacuum and evaluate diffusional limitations (M3.2)
 - Develop reactor concept for hybrid solar/electric water splitting
- Containment Materials Development
 - Synthesize ALD films on three SiC tubes having different thicknesses of coating material (M2.3)
 - Test coated tubes for stability in high temperature steam environment, and evaluate tested tubes using SEM, XRD and ICP (M2.5)
- Efficient H₂ production
 - Further refine AspenPlus model and H2A with experimental thermodynamic and kinetic results and optimal operating conditions (M5.1 & M5.2)



Proposed Future Work* – hybrid solar/electric receiver





Non-intermittent chemical processing

CU hybrid receiver (front with sliding CPC)



*Any proposed future work is subject to change based on funding levels



University of Colorado (CU) 10 kW_{th} HFSS



CU hybrid receiver (back showing xyz stand, etc.)

Acknowledgements







Backup Slides



Near-isothermal Single Cavity Dual Fluid Bed System (Easily Made Hybrid by adding Electrical Resistance)

Efficiency is Important for Solar H₂





Does Hybrid Solar/Electric make sense vs. Electrolysis for non-intermittent (10 hr per day) water splitting? Efficiency Comparison:

	η solar collection	η ΡV STWS	η elecrolysis	η overall
PV	100%	20%	70%	14%
STWS	45%	60%		27%
Hybid	η heat recuperation for ITM SEOS	η electric turbine	η electrical resistance	η overall (x 60% STWS
	90%	40%	100%	22%
	80%	40%	100%	19%
	70%	40%	100%	17%

Capital Comparison:

PV electrolysis is capital intensive – half the cost of a plant is PV and half is the electrolyzers;
Branz says cost of adding molten salt is 1/3 best possible cost of adding batteries;

3) Per Harper Int'l, adding electrical resistance with power supply to an already solarthermal receiver increases capital cost for an insulated solar reactor with sliding CPC already installed along with reactor tubes by 25 to 50% (max)

University of Colorado 12 kW_{thermal} HFSS and Hybrid Solar/Electric Receiver

CU hybrid receiver (front with sliding CPC)





CU hybrid receiver (back showing xyz stand, etc.)



Accomplishments and Progress: NSF "Sister" Project for STWS Materials Development





Par -500 -500 0.7 0.75 0.8 0.85 0.9 0.95 1.05 11 1.15 -250 250 750 Tolerance Factor Ferromagnetic Vacancy Formation Energy (kJ/mol)

- Evaluated 1343 materials for the effect of structure and magnetic ordering on STWS behavior
- Found both factors to critically impact accuracy of predicted STWS ability

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Accomplishments and Progress: Modeling of Solar-thermal Reactor Systems





Ray-tracing and finite-volume methods coupled to model heliostat field and reactor

Accomplishments and Progress: H₂ production at different SiC tube radii





For tube radii of 5 cm and 25 cm, the calculated theoretical hydrogen production rates are 7.1*10³ L/hr and 8.3*10⁴ L/hr, respectively

Accomplishments and Progress: GNG: Long Term RedOX Testing



GNG2: Demonstrate the production of robust spray dried active materials that produce at least 150 μ mol H2/g total and do not lose more than 10% of its reactivity between the 100th and 200th RedOx cycle material.

