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Investigation of Solid State Hydrides For Autonomous Fuel Cell Vehicles

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Project #ST134



This presentation does not contain any proprietary, confidential, or otherwise restricted information

Timeline and Budget

Project Start Date: 3/1/2015 FY15 DOE Funding: \$100K* FY16 DOE Funding: \$250K* FY 17 DOE Funding: \$250K

Partners

- Naval Undersea Warfare Center (Newport)
- Office of Naval Research
- Ardica Technologies, LLC

*Additional Federal (ONR) Funding: \$50K FY15, \$100K FY16



Relevance

DOE Funded Activities

Objectives:

- Screen H₂ storage systems against DoD targets and requirements that are suitable for vehicle demonstration platforms
- Complete a detailed design of the hydrogen storage system for use in an integrated system design
- Develop a preliminary design of an integrated UUV platform with a non flow through fuel cell

ONR/NUWC Funded Activities

Objectives:

- Design, build, and test a small benchscale, alane hydrogen storage vessel
- Package and ship bench-scale vessel and alane material to the Navy (NUWC)
- Provide technical support to Navy NUWC for their further testing and evaluation

Impact:

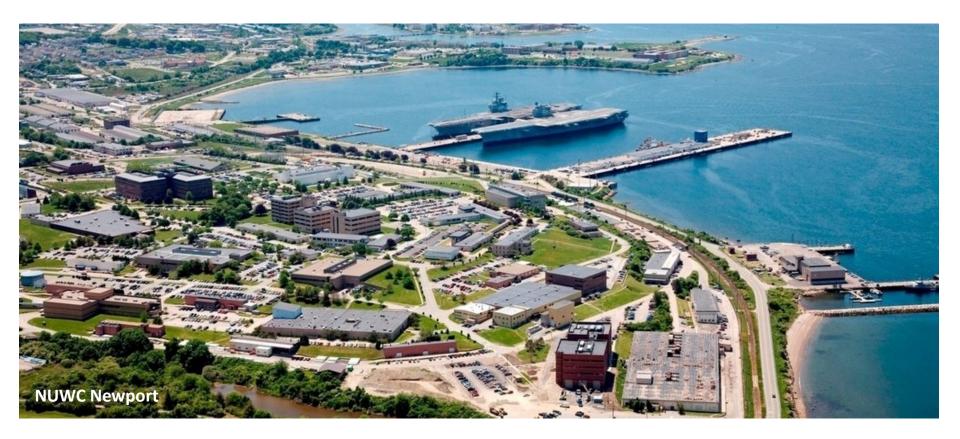
- The experience gained from the HSECoE and the core capabilities of SRNL and DOE were leveraged to develop a unique hydrogen storage system for new fuel cell applications
- Extension of this program to other unmanned and manned platforms is likely
- This project also provides the basis to extend a long-term partnership between DOE and the DOD in hydrogen and renewable energy systems

The overall approach of this research is to develop a methodology that incorporates engineering modeling and analyses to efficiently screen, design and select storage materials and material systems against cost and performance targets leading to an initial system design for an Unmanned Underwater Vehicle (UUV) application.

- This methodology, initially developed by SRNL and applied to light-duty vehicle in the Hydrogen Storage Engineering Center of Excellence (HSECoE), was adapted for other hydrogen and FC applications
- This methodology will be applied to UUVs to reduce design time and lead to a more cost effective and better performing final product
- Maintaining this capability for DOE will attract other opportunities and projects in hydrogen and other gas handling areas



Naval Undersea Warfare Center (NUWC) Division Newport



Naval Undersea Warfare Center, is the Navy's full-spectrum research, development, test and evaluation, engineering, and fleet support center for submarine warfare systems and many other systems associated with the undersea battlespace.

Christian Schumacher and Dr. Joseph Fontaine



REMUS 600

Navy NUWC changes proposed project from 22" UUV to 12.75" Remus Platform

Advantages:

- Smaller, less expensive and readily available commercial platform
- Reduced requirements for alane material
- Ability to break hull to accommodate canister refueling





Target Mission

Constant Power: 250W

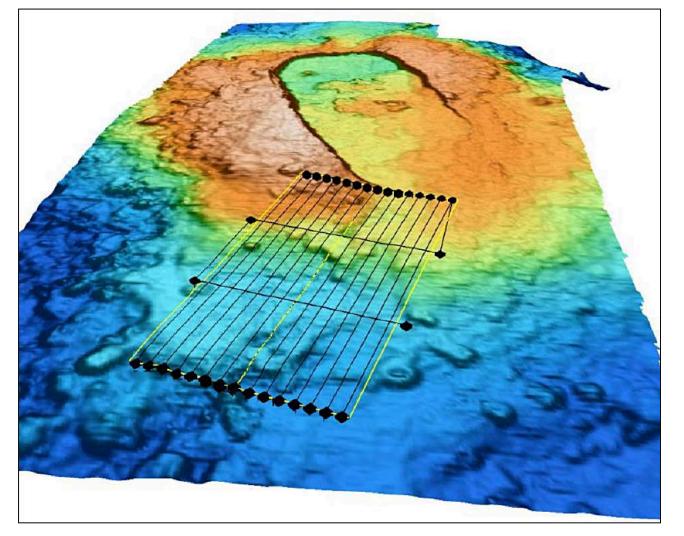
- 100W Propulsion
- 100W Hotel Load
- 50W Sensors

No Transients

• Simple Design

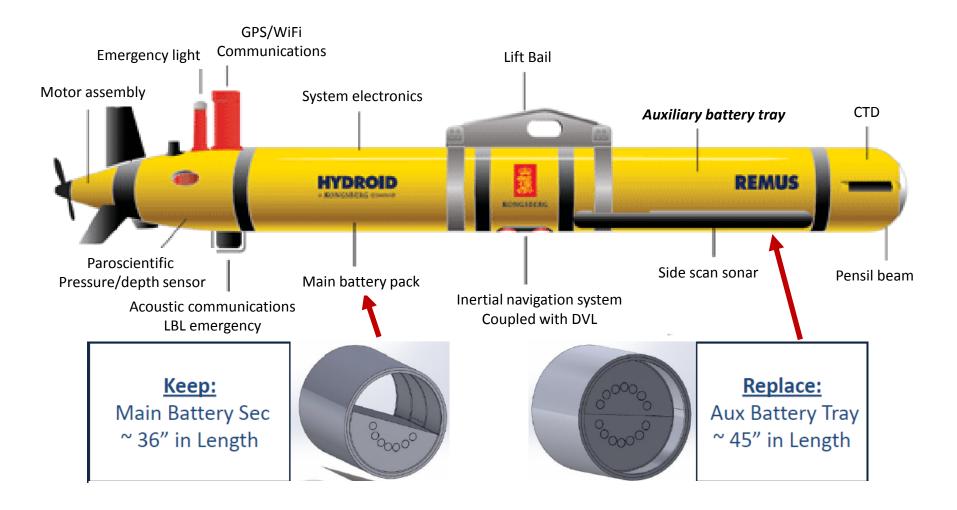
Assume Auxiliary Battery

- Neglect Start-up
- Neglect Shut-down





REMUS 600



Replace auxiliary battery tray with a hydrogen storage material, fuel cell, and oxidant system



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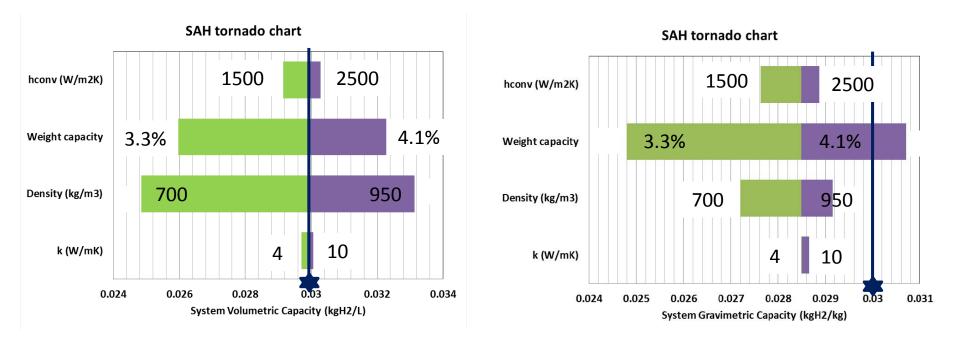
Accomplishments: Material Screening Analysis Criteria

Targets and Data (Gen1 system)	Waste heat available (Gen1 system)
 System volumetric capacity = 3% Usable hydrogen to be stored = 2kg Available volume = 66 L (18.5" x 15") 	Latent heat (average) from H ₂ O ₂ reaction condensing steam = 43.9 MJ • Mission time = 30 hours • Total mass of water available = 29 L • Steam fraction = 0.78
 System gravimetric capacity = 3% Usable hydrogen to be stored = 2kg Storage system weight = 66 kg 	 Steam fraction = 0.76 Temperature = 210 °C Pressure = 18 bar Max (more) water sensible heat = 31.5 MJ
Cost = +1000 \$/kg of hydrogen	Heat (average) from FC byproduct water = 4.08 MJ
H ₂ average flow = 1.1 g/min • Based on FC efficiency of 50%	 Mission time = 30 hours Total mass of water available = 17.7 L Temperature = 80 °C
H ₂ peak flow = 2.1 g/min • Based on FC efficiency of 50%	 Heat (average) from FC cooling water = 60.48 MJ Mission time = 30 hours Total mass of water available = variable
H_2 delivery pressure = 2-20 bar	• Temperature = 80 °C

Targets and Data (Gen2 system)	Waste heat available (Gen2 system)
 System volumetric capacity = 5% Usable hydrogen to be stored = 3.2kg Available volume = 66 L (18.5" x 15") 	Latent heat (average) from H ₂ O ₂ reaction condensing steam = 43.9 MJ • Mission time = 30 hours • Total mass of water available = 29 L • Steam fraction = 0.78
 System gravimetric capacity = 5% Usable hydrogen to be stored = 3.2kg Storage system weight = 66 kg 	 Steam fraction = 0.78 Temperature = 210 °C Pressure = 18 bar Max (more) water sensible heat = 31.5 MJ
Cost = 1000 \$/kg of hydrogen	Heat (average) from FC byproduct water = 4.08 MJ
H ₂ average flow = 1.8 g/min • Based on FC efficiency of 50%	 Mission time = 30 hours Total mass of water available = 17.7 L Temperature = 80 °C
H ₂ peak flow = 3.8 g/min • Based on FC efficiency of 50%	 Heat (average) from FC cooling water = 60.48 MJ Mission time = 30 hours Total mass of water available = variable
H ₂ delivery pressure = 2-20 bar	• Temperature = 80 °C

Using military hydrogen storage targets similar to DOE targets; SRNL evaluated hydrogen materials against nearterm (Gen1) and longterm (Gen2) application performance requirements.

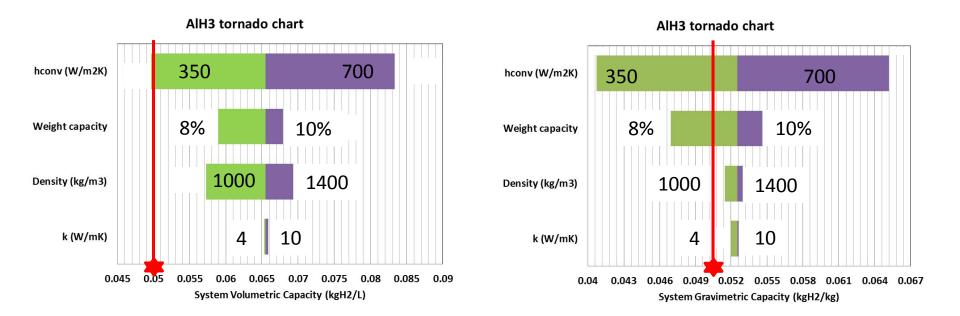
Accomplishments: NaAlH₄ material performance sensitivity analysis (Gen1)



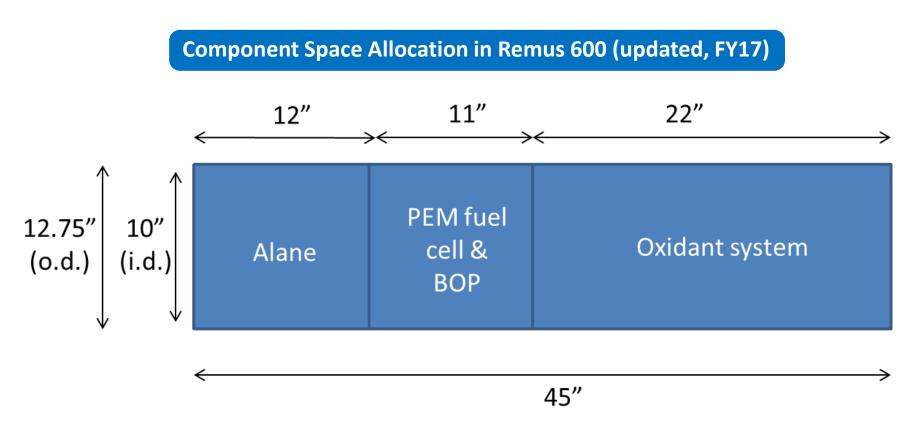
- The Material Shows Good Performance
 - Gen1 target volume capacity (3%) achieved by mini-channel heat exchanger or enhanced heat transfer systems
 - It approaches the Gen1 gravimetric target (3%)
- Significant Influence of the Material Properties on the Performance



Accomplishments: AlH₃ material performance sensitivity analysis (Gen2)



- The Material With 'Normal' Shell & Tube, Heat Exchangers Shows Good Performance
 - Gen2 target volume capacity (5% kg/L) achieved
 - Gen2 gravimetric capacity (5%) achieved
- Significant Influence of the Heat Exchanger Properties (Mainly Convective Heat Transfer)
- Main Issues → Making a Lower Cost Material



- This system will utilize heat from the oxidant system to drive the thermal desorption of hydrogen from alane to drive a fuel cell
- The ultimate goal is to achieve a 2 x increase in the vehicle operation range/time

Preliminary sizing of the alane reactor

System assumptions and constraints			
Mass of hydrogen	1.13 kg		
Hydrogen flow rate	0.2 g/min for 96 hours		
Start up/shut down	10 min		
Max diameter	10 in		
Length	9.0 - 13.1 in		
Heat transfer fluid	Pressurized water		
Inlet/Outlet T	150/130 °C		
Pressure	10 bar		

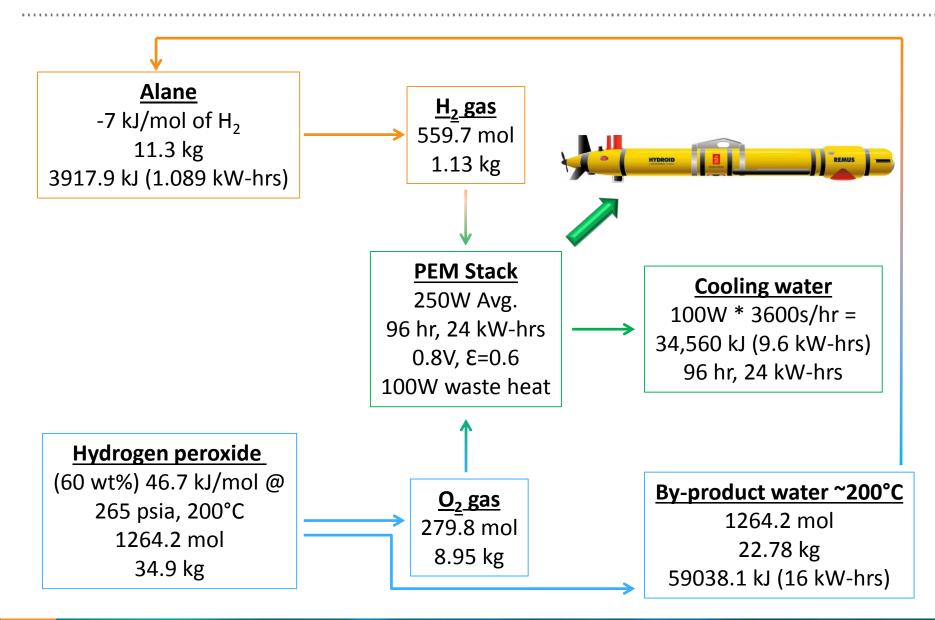


Alane properties		
ΔH	7.6 kJ/mol H₂	
Cp k	1340 J/kgK	
	7 W/mK	
wf	10%	
Bulk density	1000 kg/m ³	

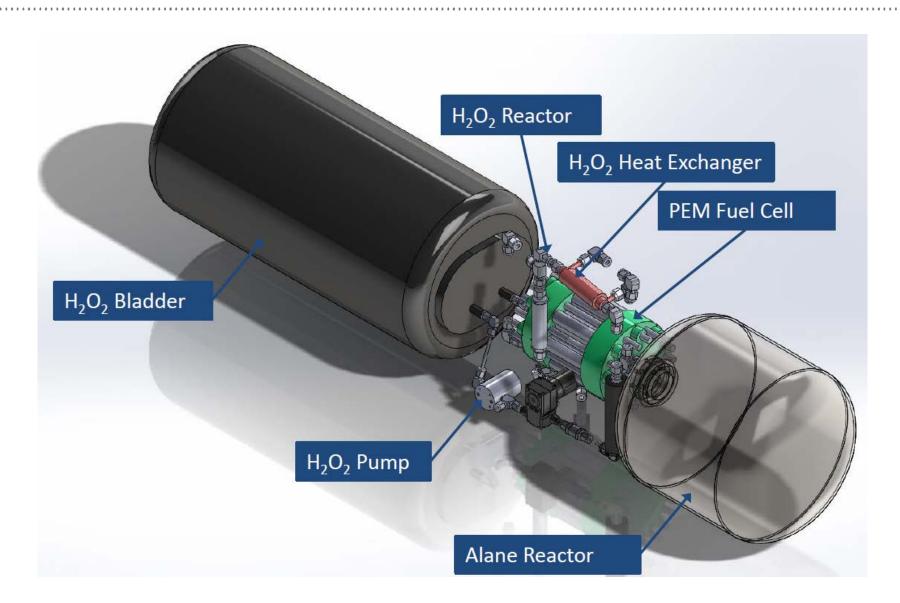
Results		
Reactor Diameter	10 in	
Reactor Length	10.6 in	
Total Power Required	890 W	
Thermal Energy for		
start up/shutdown	146 Wh	
Thermal Energy for		
desorption	1200Wh	
Total Required Power	890 W	
Power required for		
desorption	13 W	

- This study determined the alane reactor size and accounted for the mass and energy balance of the reactive system along with a heat transfer system (shell and tube)
- The alane vessel will fit in the space allotted in the REMUS 600

Alane, oxidant system, and fuel cell interfaces



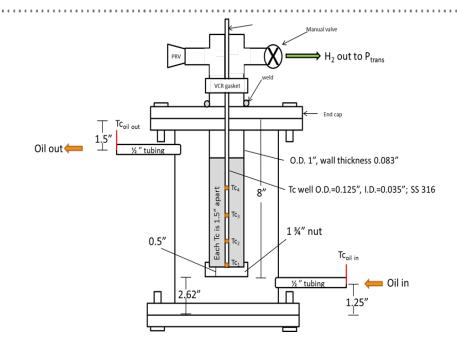
Solid Model of System

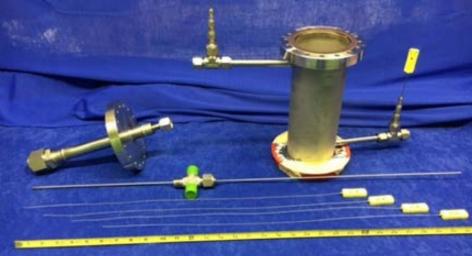




Accomplishments: SRNL Alane Test Vessel Setup

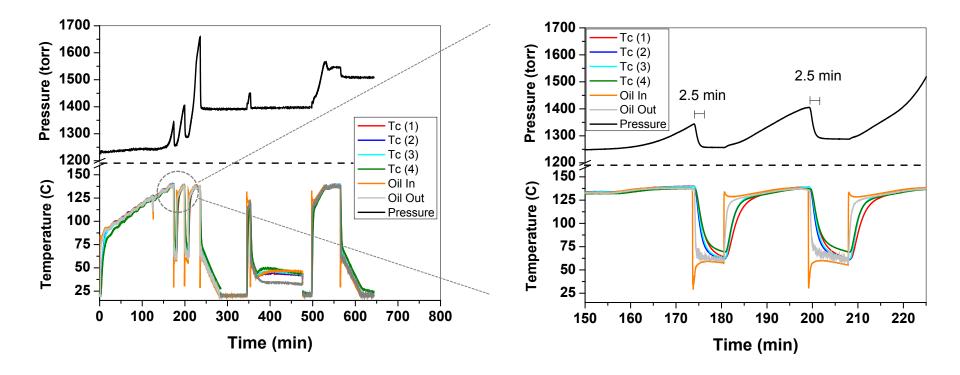






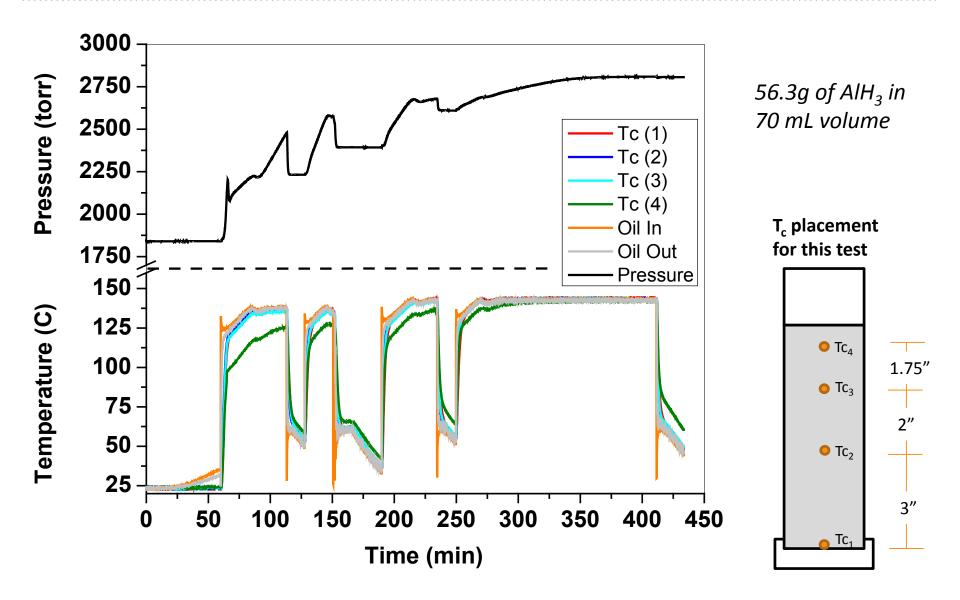


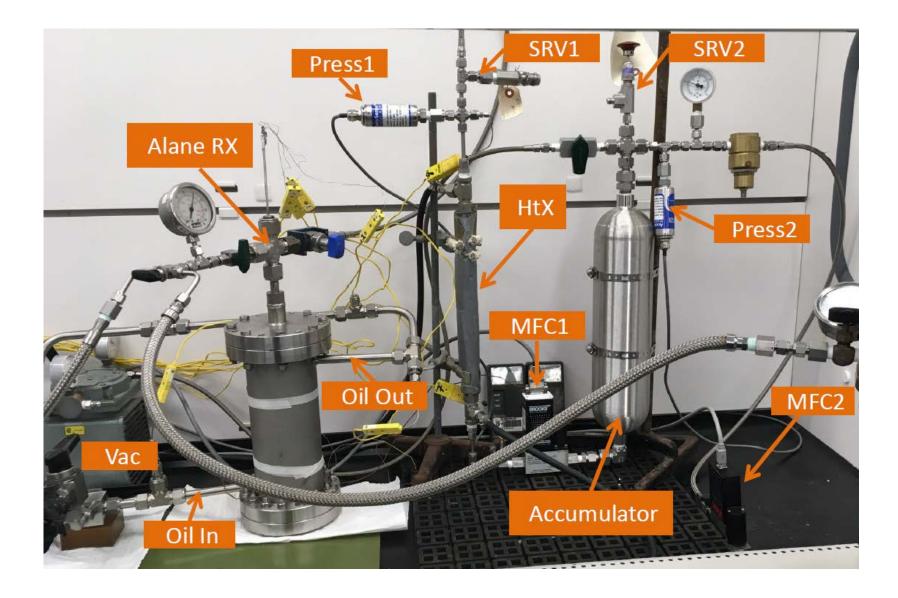
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- H₂ is released at ~133 °C.
- H₂ release can be readily stopped via the cooling loop set at 20 °C.

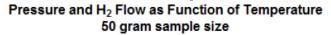
Accomplishments: SRNL Alane Test Vessel Results (Ardica alane)

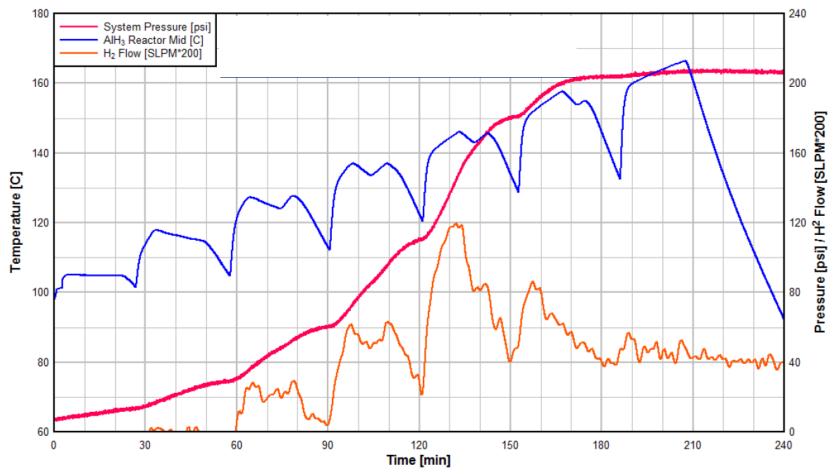




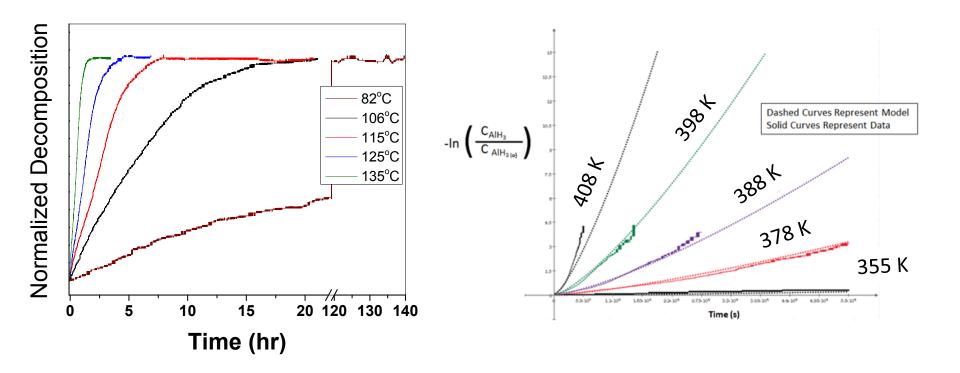


Alane Decomposition



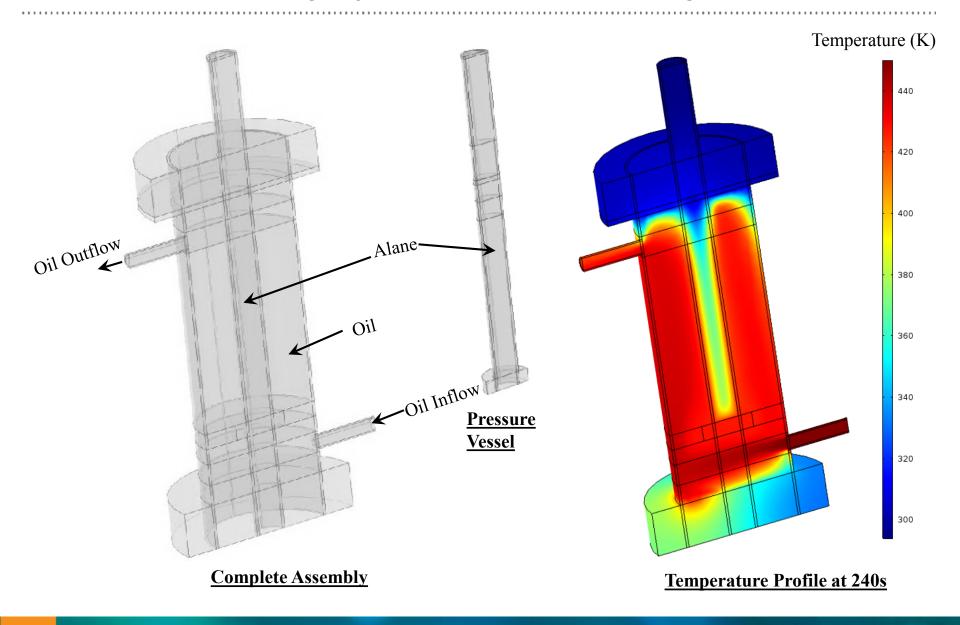


Isothermal Desorption of Alane With 1 bar H₂ Back Pressure



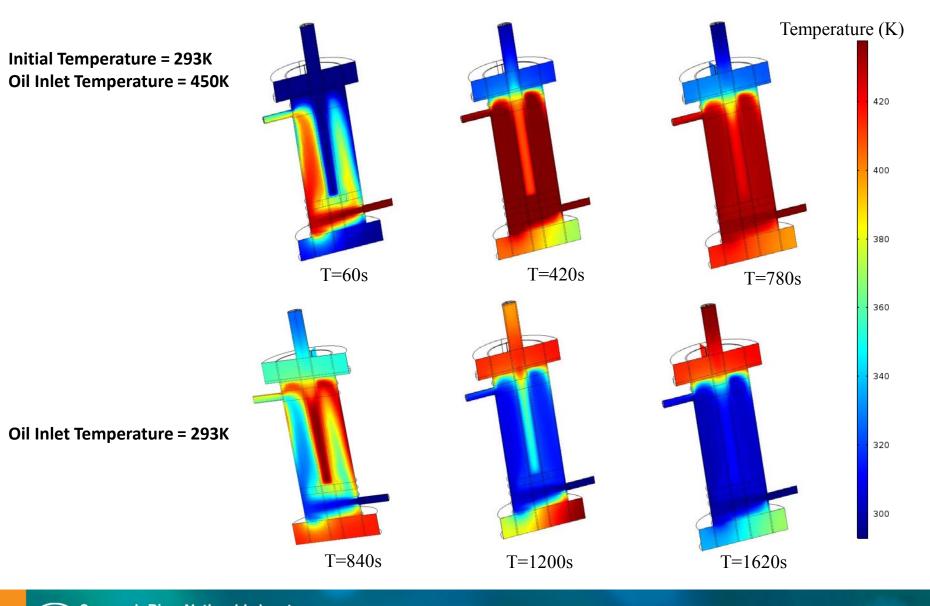


Accomplishments: Storage System Heat Transfer Modeling

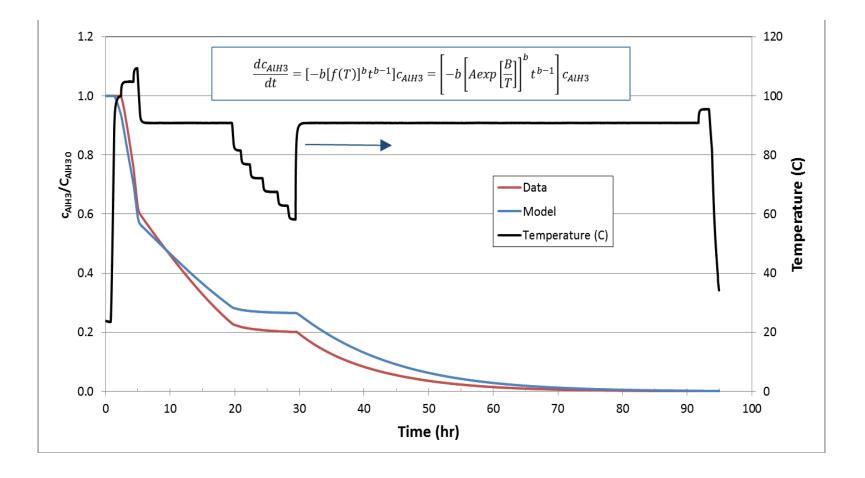


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Accomplishments: Storage System Modeling







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• Project not reviewed in 2016.



- Completed an engineering analysis to screen the most attractive solid-state hydrogen storage materials for UUV applications
- Alane (AlH₃) was selected as the most attractive candidate
- Testing was performed to demonstrate AlH₃ hydrogen storage and delivery performance including steady-state and transient operations
- Delivered AlH₃ material and test module to NUWC for further Navy testing
- Ongoing systems and detailed modeling for UUV platforms are underway along with material safety testing (Ardica Technologies)
- Preliminary analyses indicate 2 times the energy storage compared to battery systems
- End of year objective is to develop a prototype alane-based UUV system design & system model for potential Navy applications
- Long-term path forward is to work with the Navy to develop a final design, fabrication and testing of a prototype UUV system.





Naval Undersea Warfare Center (Newport)

- UUV Energy System Integrator
- End-user and System Tester/Evaluator



Office of Naval Research

Sponsor



Ardica Technologies, LLC

- Fuel cell Portable Power System Developer and Manufacturer
- Developer for DoD Army Alane-based Soldier Power System
- DOE CRADA Partner with SRNL to Lower the Manufacturing and Recycling Cost of Alane

No new patents to date but SRNL patent # US 8470156 B2 is the basis for the current DOE CRADA between SRNL and Ardica and future IP and/or Tech Transfer is anticipated



Remaining Challenges and Barriers

- Efficiently integrating alane-based hydrogen storage vessel design with fuel cell, hydrogen generator (hydrogen peroxide) and BOP
- Meeting system volume and weight requirements to meet Navy UUV specifications and maintaining neutral buoyancy and achieving all performance objectives
- Demonstrating onboard alane material storage and handling safety
- Supporting the Navy to provide a suitable cost supply of alane to meet future missions and applications



UUV operations off the coast of Bahrain in 2013. Credit: Specialist 2nd Class Michael Scichilone/US Navy/Released



Backup slides



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Material Classes

- 1. Reversible low T MH (AB₅, AB, NaAlH₄)
- 2. Reversible high T MH (Mg family materials)
- 3. Non reversible MH (Alane, Mg alanate, LiMg alanate)

MH material Matl wf Operating Matl cost Matl vf Enthalpy Waste heat Comment $T(^{\circ}C)/P(bar)$ (\$/kq) (kg_{H2}/kg_{MH}) (kq_{H2}/L) (kJ/mol_{H2}) (kJ/mol_{H2}) AB_{5} (MmNi₅) 35 Too low wf 50/12 1.1% 4.4% 30.5 64.1 Too low wf AB (TiFe) 50/10 7 1.8% 4.5% 28 64.1 3.8-4% **NaAlH** 120/45 3.5 3.3-3.5% 40 53.9 Additional H2 75 Mg 360/10 4 6% 5.2% to be burned Additional H2 Mg₂Ni_{0.75}Cu_{0.25} 280/10 8.2 3% 6% 53 to be burned 80-120/25 * 9.5% 12.6% 11 35.3 AlH₃ Currently expensive (Gen1Sc=56.5) $Mg(A|H_4)_2$ 130-170/30 * 8% 8% 1.5 31.4 Inexpensive matl; Step 1 + (Gen1Sc=50.2) Hydrolysis $LiMg(AIH_4)_3$ 150/30 * 8% 8% 13.1 31.4 Two step material + (Gen1Sc=50.2) hvdrolvsis Targets (Gen1) P=2-20 bar +1000 >3% >3% _ _ (Gen2) P=2-20 bar 1000 >5% >5%



Gen1

Gen2