

IDAES[®]

Institute for the Design of
Advanced Energy Systems

Advanced Process Control and Dynamic Optimization of Reversible Solid Oxide Cell Systems for Performance and Long-Term Health

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DOE Hydrogen Program 2024 Annual Merit Review

Crystal City, Arlington

May 7, 2024

SOC-based System for Hydrogen and Power Production

- **Key Challenges**

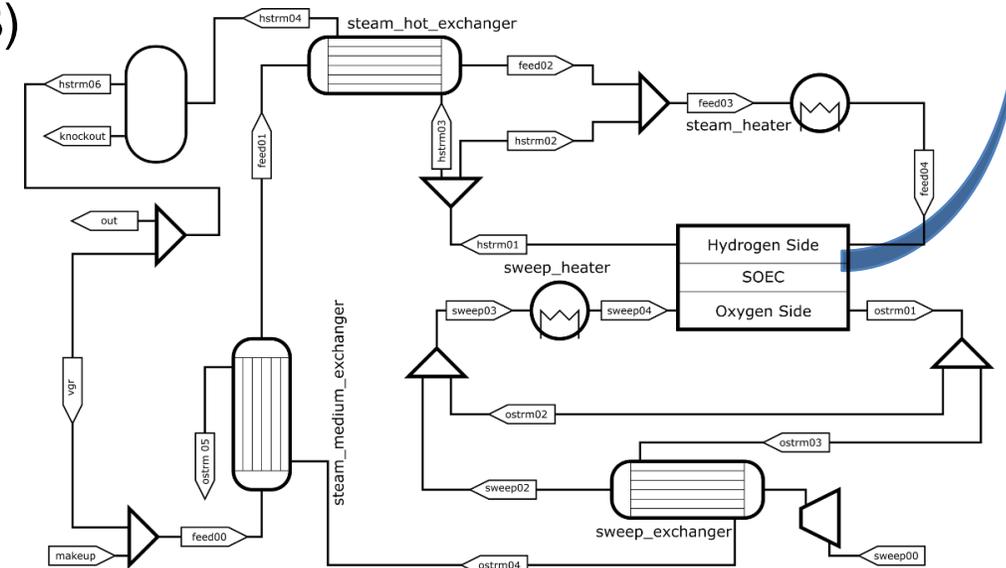
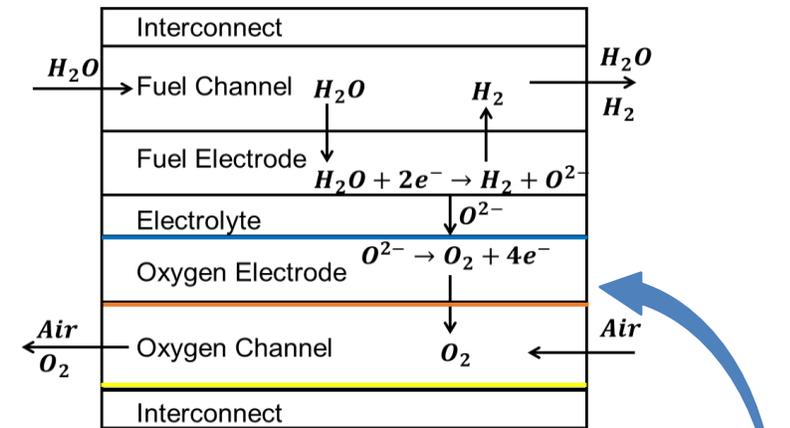
- Solid Oxide Cell (SOC)-based systems for hydrogen and power production **need to operate flexibly** with fluctuations in market electricity prices.
- How can we **best operate and control** SOC-based systems for **mode-switching (H₂/power)**, while **minimizing degradation** over long-term flexible operation?

- **Technical Approach**

- Develop a **first-principles dynamic model** of SOC-based systems
- Develop **classical and advanced process controls** for effective thermal management and mode-switching operation
- Develop first-principles **degradation** sub-models to **quantify the impact of flexible operation** on cell health
- Optimize **long-term performance** and **health** of flexible SOC-based systems

Dynamic Model of SOC-based System for Mode-Switching

- **IDAES** open-source, equation-oriented modeling and optimization framework (Lee et al., 2021)
- **SOC dynamic model** (Bhattacharyya et al., 2007)
 - First-principles, non-isothermal, planar cell
 - 2D electrodes, electrolyte, and interconnect
 - 1D fuel and oxygen channels
 - Operates in fuel cell and electrolysis modes
- **Dynamic SOC-based system model** (Allan et al., 2023)
 - **H₂ fueled** in fuel cell mode
 - **Vent gas recirculation** with purge
 - **Condenser** to remove water from H₂-side off-gas
 - Equipment models for **thermal management**
 - 1D multi-pass crossflow recuperative heat exchangers
 - 1D crossflow trim heaters
 - System **performance constraints**



Block flow diagram of H₂-fueled SOC-based IES for Mode-Switching Operation

- Lee, A., et al., J Adv Manuf Process 2021, 3(3) (2021).
- Bhattacharyya et al., Chem Eng Sci, 62, 4250-4267 (2007).
- Allan, D.A., et al., In Proc. FOCAPO/CPC (2023).

SOEC Microstructure Chemical Degradation Modeling

Fuel electrode nickel (Ni) agglomeration

- Ni particles grow with time under high temperature operation
- Ni₂OH formation drives the process
- Surface-diffusion – Ostwald ripening

$$\frac{d(\overline{d_{Ni}})}{dt} = C \frac{X_{Ni}}{X_{YSZ} A_{YSZ} d_{Ni}^6} \left(\frac{Y_{H_2O}}{Y_{H_2}^{0.5}} \right) \exp\left(-\frac{E_a}{RT}\right)$$

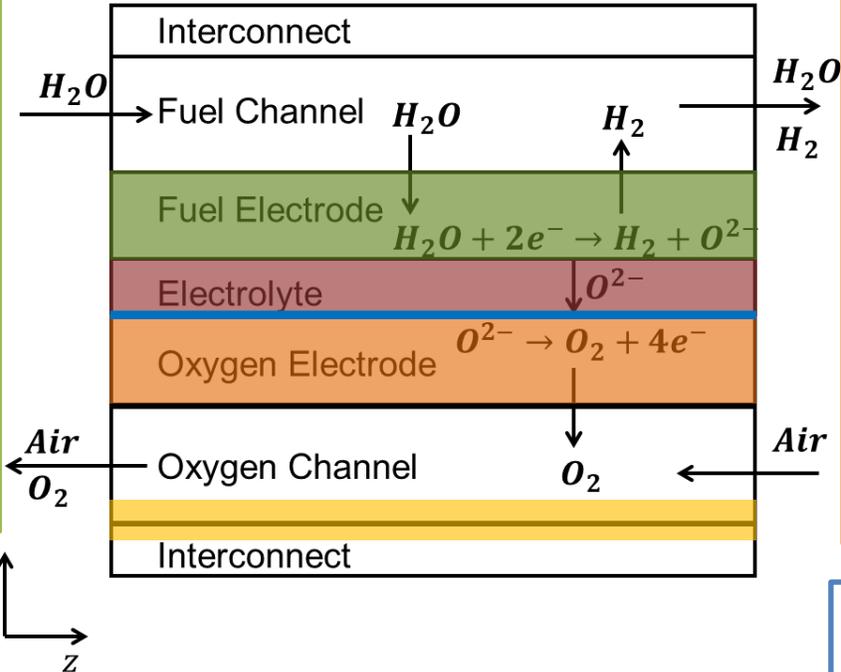
Refs: J. Sehested et al. / *Applied Catalysis A: General* 309 (2006) 237–246

YSZ electrolyte phase transformation

- Phase transformation of YSZ from cubic to tetragonal structure
- Results in decrease in electrolyte conductivity

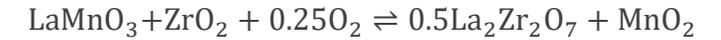
$$\sigma_{El} = \sigma_{El,0} \left[\lambda + (1 - \lambda) \exp\left(-\frac{t}{\tau}\right) \right]$$

Refs: Jiang et al. *Journal of the American Ceramic Society* 82(11):3057 - 3064



Lanthanum zirconate (LZO) scale growth

- At oxygen electrode under oxidizing conditions and high temperatures driven by high P_{O₂}



- Parabolic growth law

$$\frac{dl_{LZO}(t)}{dt} = \frac{K_{g,LZO}}{2l_{LZO}(t)X_{0,LZO}\rho_{LZO}} \exp\left(\frac{E_{LZO}}{RT}\right)$$

Refs: A. Kamkeng, and M. Wang. / *Chemical Engineering Journal* 429 (2022): 132158

Chromium oxide scale growth

- Oxidation of chromium interconnect-oxygen electrode boundary
- Parabolic growth law

$$\frac{dl_{COS}(t)}{dt} = \frac{K_{g,COS}}{2l_{COS}(t)X_{0,COS}\rho_{COS}} \exp\left(\frac{E_{COS}}{RT}\right)$$

Refs: D. Larrain et al. / *Journal of Power Sources* 161 (2006) 392–403

LSM-YSZ phase coarsening

- Driven by Mn²⁺ diffusion from LSM surface toward LSM-YSZ interface
- Results in loss of TPB length
- Model derived by assuming Fick's law diffusion of Mn²⁺

$$\frac{L_{TPB}}{L_{TPB,0}} = 1 - 2 \times \left(\frac{t \times D_{LSM}}{\pi} \right)^{1/2}$$

Refs: A. Kamkeng, and M. Wang. / *Chemical Engineering Journal* 429 (2022): 132158

Impact of Chemical Degradation on Cell Temperatures

Chemical degradation depends on operating strategy

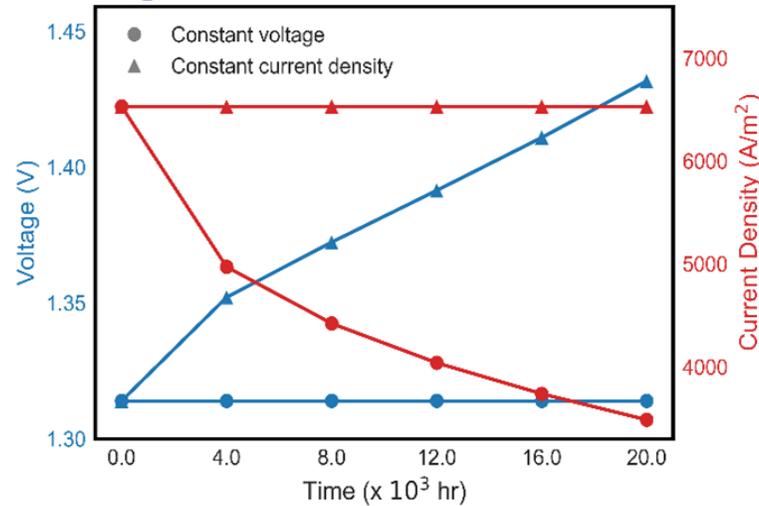
- Constant voltage (potentiostatic)
- Constant current density (galvanostatic)

What happens if the initially optimal cell operating conditions are held constant?

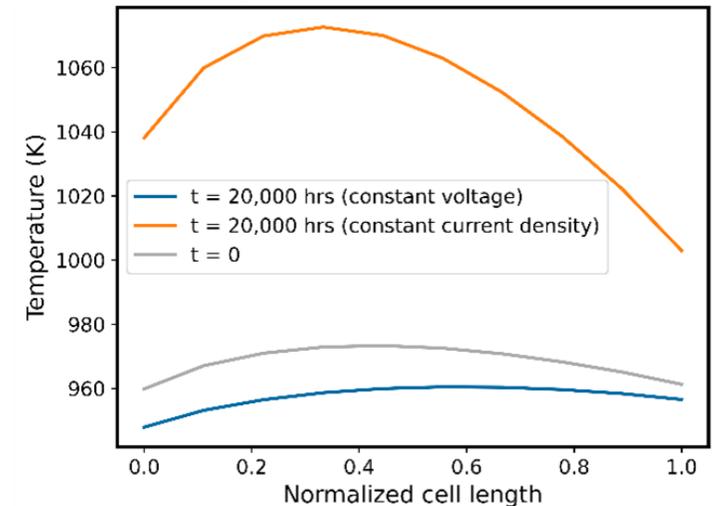
- Initial steady state optimization profiles held constant for 20,000 hours
- Inlet temperatures held constant

Impact on cell performance

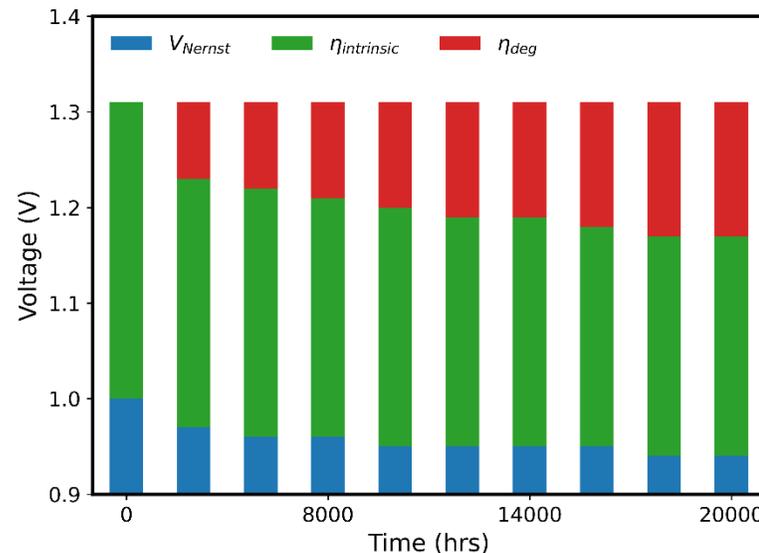
- Potentiostatic operation results in 42% decrease in current density
- Galvanostatic operation results in 8.3% increase in cell terminal voltage



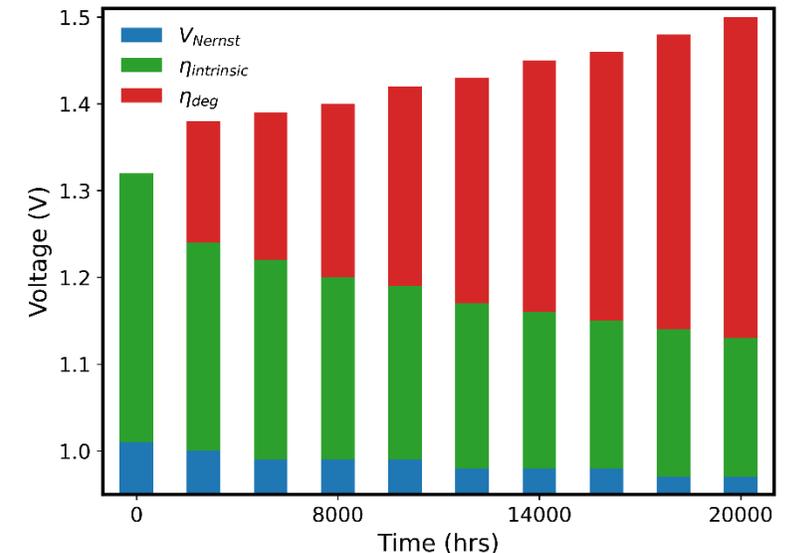
Operating profile of current density and voltage under potentiostatic and galvanostatic operation



Temperature profile under potentiostatic and galvanostatic operation after 20,000 hr of operation



Voltage losses under potentiostatic operation



Voltage losses under galvanostatic operation

Optimizing Long-Term SOEC System Operation

Case 1: Maximize Integral Efficiency

$$\max \frac{1}{t_f - t_0} \int_{t_0}^{t_f} \eta_t dt$$

st.

$$h(x) = 0$$

$$\frac{dR}{dt} = f_R(x, t)$$

$$\eta_t = \frac{HHV(\dot{m}_{H_2,t})}{P_{in,total,t}} \quad \forall t$$

Case 3: Minimize Levelized Cost of Hydrogen (LCOH)

LCOH =

$$\frac{CRF_{BOP} CC_{BOP} + \sum_{i=1}^R CRF_{stack,i} CC_{stack} + OC + EC}{m_{H_2,lifetime}}$$

Case 2: Minimize Final Degradation

$$\min \Delta V(\overline{\theta}_{t_f})$$

st.

$$h(x) = 0$$

$$\frac{dR}{dt} = f_R(x, t)$$

$$\theta_{t_f} = \theta_{t_0} + \int_{t_0}^{t_f} \dot{\theta}(x, \theta) dt$$

Decision variables at each time point:

1. Feed heater duties
2. Sweep heater duties
3. Sweep blower flowrate
4. Feed exchanger flowrate
5. Feed recycle ratio
6. Sweep recycle ratio

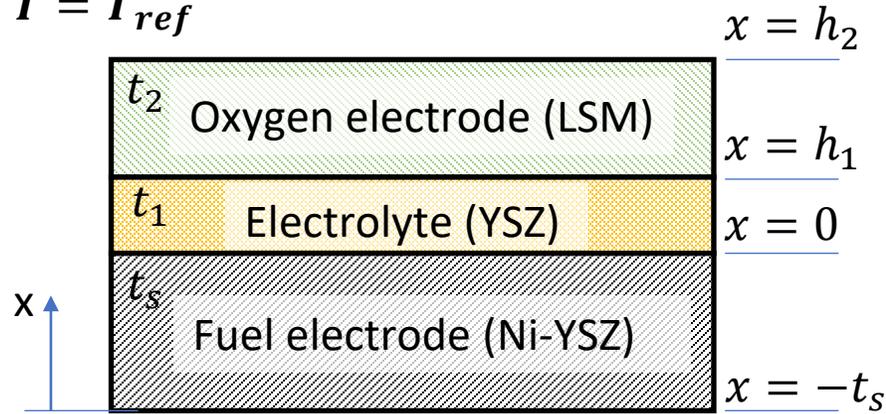
Quasi-Steady State Optimization Results for 3 Objective Functions under Galvanostatic, Potentiostatic, and Flexible Operation for Low- and High-Price Electricity Markets

Operating Profile	Objective Function	Electricity Price = 0.03 \$/kWh		Electricity Price = 0.3 \$/kWh	
		Replacement Schedule (years)	LCOH (\$/kg H_2)	Replacement Schedule (years)	LCOH (\$/kg H_2)
Galvanostatic Operation	Minimize terminal degradation	5	2.00	5	13.00
	Maximize Integral Efficiency	2	2.29	2	11.92
	Minimize LCOH	5	1.93	2.5	11.84
Potentiostatic Operation	Minimize terminal degradation	3	2.11	3	12.51
	Maximize Integral Efficiency	2	2.30	2.0	11.93
	Minimize LCOH	3	2.05	2.0	11.91
Free Operation	Minimize terminal degradation	5	1.99	5	13.01
	Maximize Integral Efficiency	3	2.02	2.5	11.78
	Minimize LCOH	5	1.92	2.5	11.78

Physical Degradation: Thermal Stress Evolution

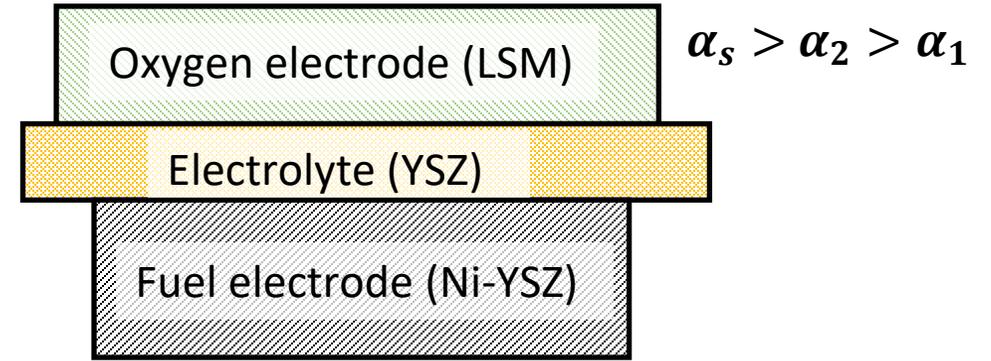
Zero-stress condition

$$T = T_{ref}$$

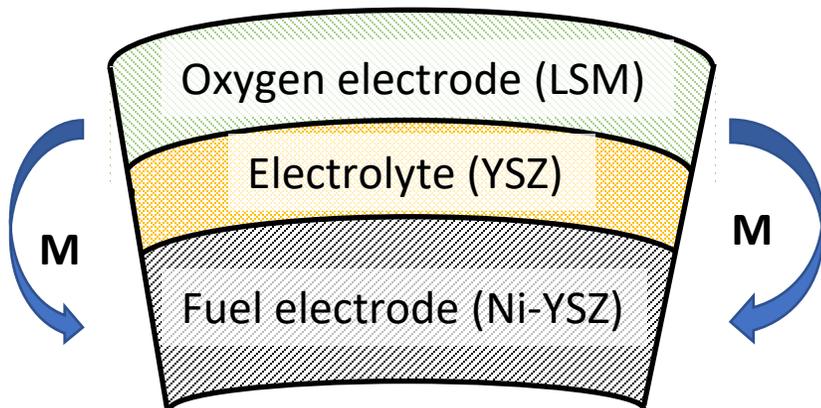


Layers free to expand

$$T = T_{ref} + \Delta T$$

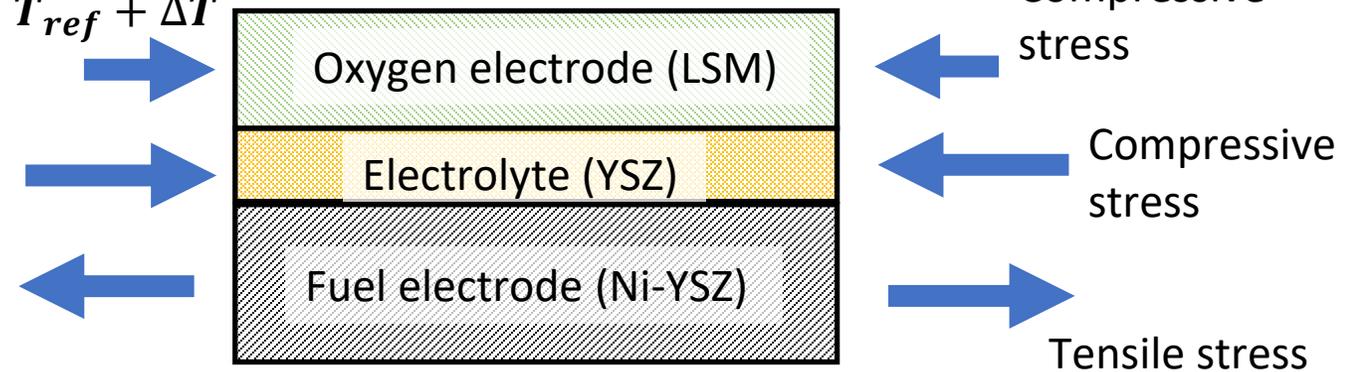


Bending induced by asymmetric stresses

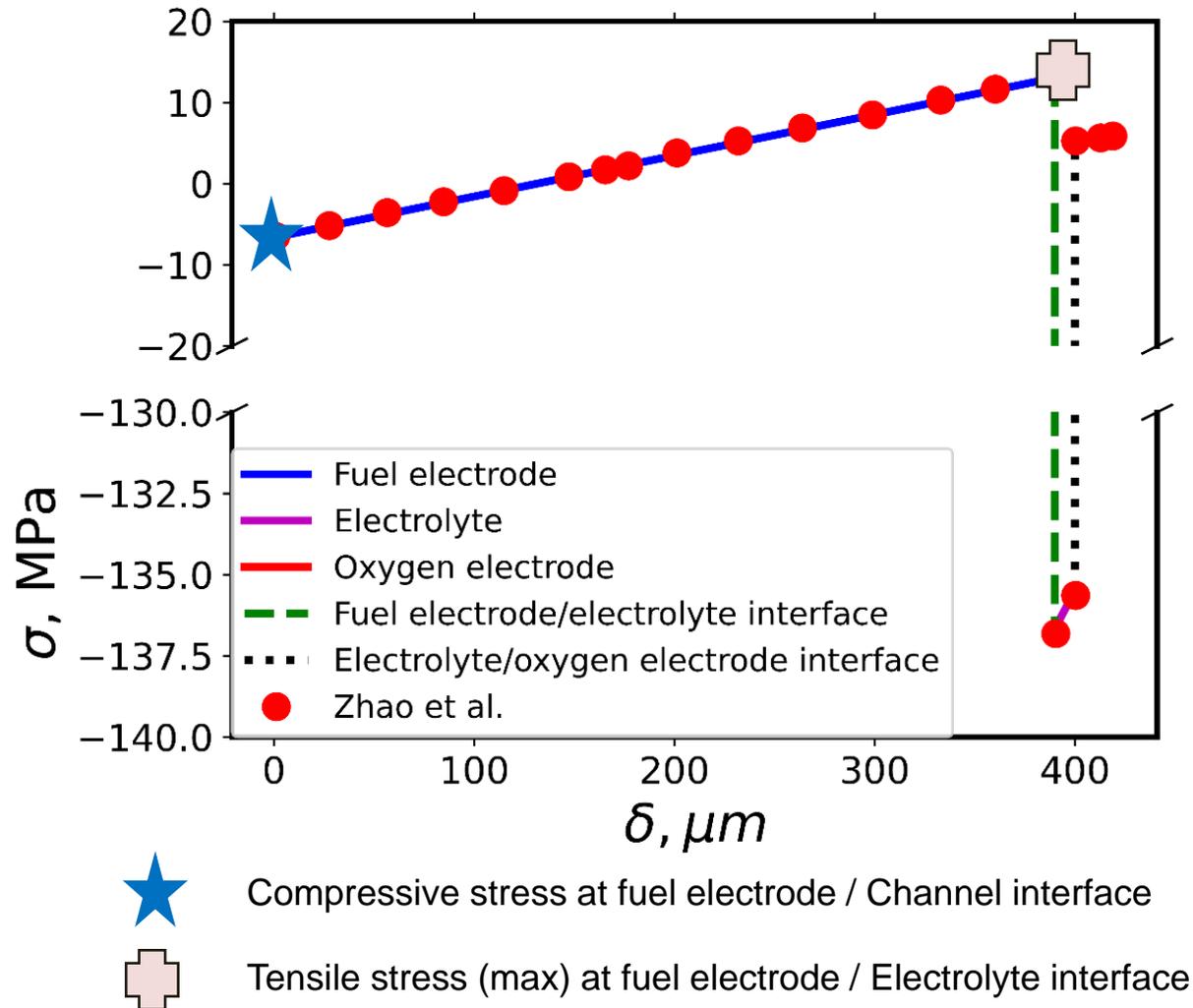


Strain continuity at layer interfaces

$$T = T_{ref} + \Delta T$$



Understanding Thermal Stress Distribution



- Sustained operation at high temperature affects thermal and mechanical properties causing localized **stress build-up**.
- Ceramics are more resilient to compressive stresses than tensile stresses.
- Steep changes in stress profiles and directionality are observed around interfaces.

Maximizing Efficiency under Stress Constraint

$$\max \frac{1}{t_f - t_0} \int_{t_0}^{t_f} \eta_t dt$$

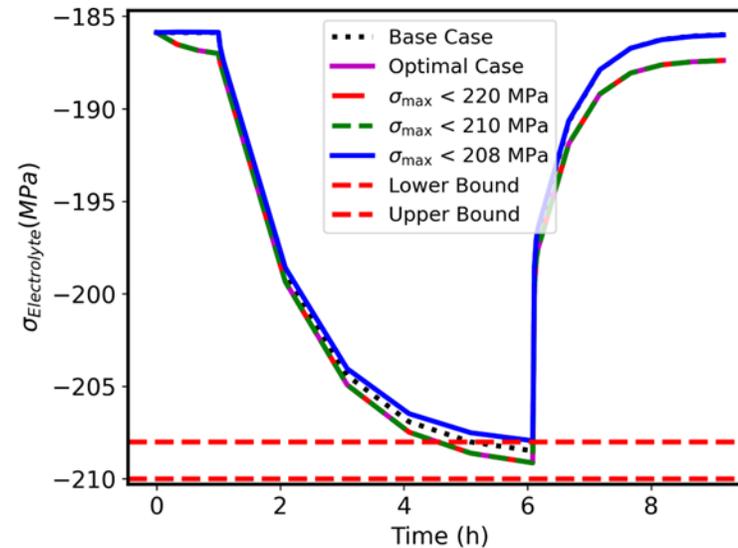
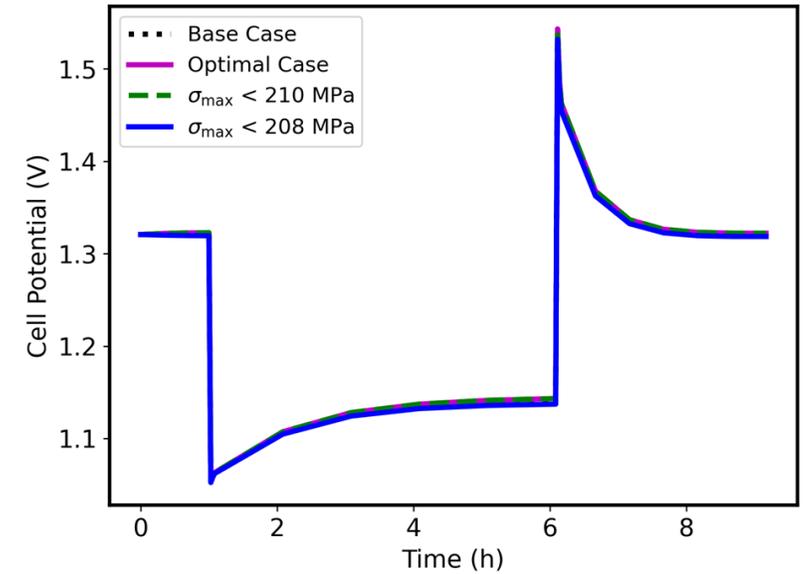
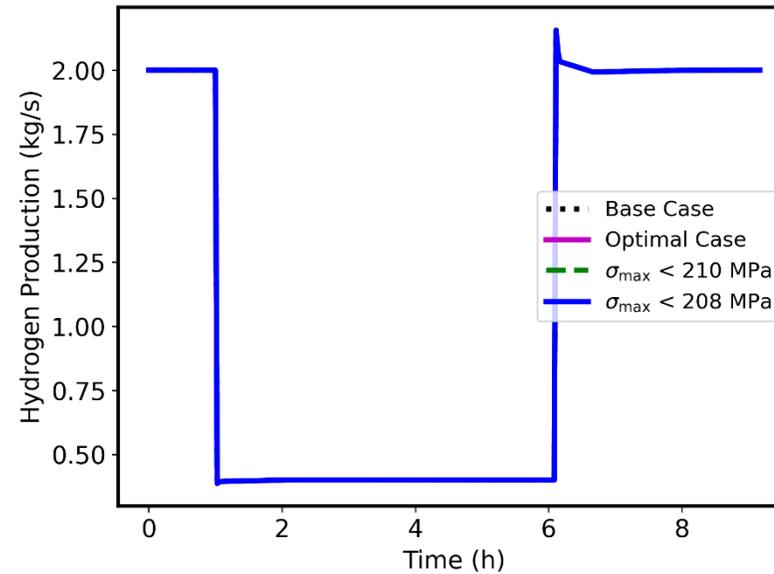
st.

$$h(x) = 0$$

$$\frac{dR}{dt} = f_R(x, t)$$

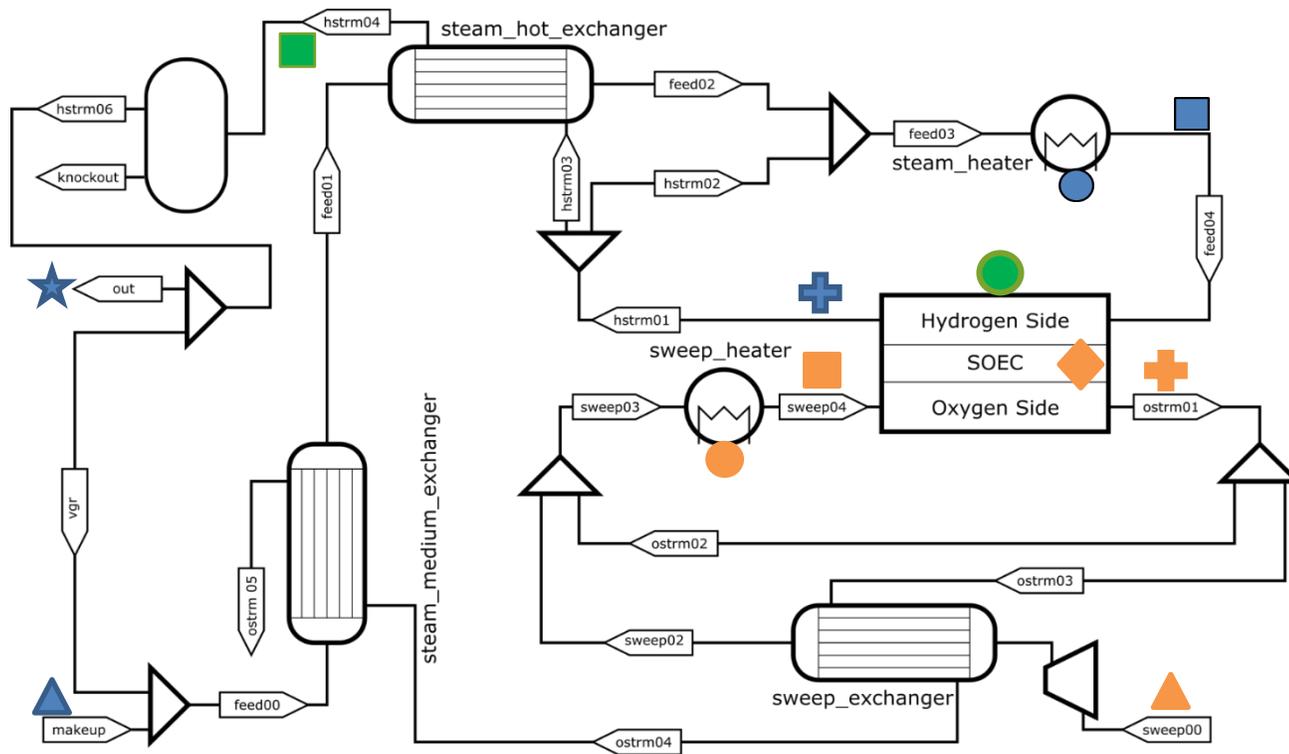
$$\sigma^i \leq \sigma_{max}^i [MPa]$$

$$\eta_t = \frac{HHV(\dot{m}_{H_2,t})}{P_{in,total,t}} \quad \forall t$$



Process Control for SOC-based System Mode-Switching

- **Classical Control: Proportional-Integral-Derivative (PID)**
- **Nonlinear Model Predictive Control (NMPC)**
 - Well-suited to highly interactive manipulated variables and constraint handling



Controller	Manipulated Variables (MVs)	Controlled Variables (CVs)
PID, NMPC	Cell potential ●	Outlet Water Concentration ■
PID, NMPC	Steam/H ₂ feed rate ▲	H ₂ production rate ★
PID, NMPC	Feed heater duty ●	Feed heater outlet temperature ■
PID, NMPC	Sweep heater duty ●	Sweep heater outlet temperature ■
PID, NMPC	Steam heater outlet temperature setpoint* ■	SOC steam outlet temperature +
PID, NMPC	Sweep heater outlet temperature setpoint* ■	SOC sweep outlet temperature +
PID, NMPC	Sweep feed rate ▲	SOC temperature ◆
NMPC	Feed recycle ratio	
NMPC	Sweep recycle ratio	
NMPC	Vent gas recirculation (VGR) recycle ratio	
NMPC	H ₂ /H ₂ O ratio in make-up	

*artificial control variables

- Allan, D.A., et al., In Proc. FOCAP/CPC (2023).
- Dabadghao, V., Ph.D. Thesis, CMU (2023).

Nonlinear Model Predictive Control (NMPC)

• NMPC Objective Function

- Developed for setpoint transition
- Penalties for cell temperature curvatures related to degradation

$$f_{\text{obj}} = \underbrace{\sum_{i=0}^N \rho_{H_2} (y_i - y_i^R)^2}_{\text{Trajectory tracking of H}_2 \text{ production rate}} + \underbrace{\sum_{i=0}^N \sum_{j \in J} \rho_j (u_{ij} - u_{ij}^R)^2 + \sum_{i=0}^N \sum_{k \in K} \rho_k (x_{ik} - x_{ik}^R)^2}_{\text{Deviations of manipulated } (u_{ij}) \text{ and controlled variables } (x_{ik}) \text{ from reference values}} + \underbrace{\sum_{i=1}^N \rho' (v_i - v_{i-1})^2}_{\text{Rate of change penalties on trim heater duties}} + \underbrace{\sum_{i=0}^N \sum_{z=1}^{z_L} \rho_M \left(\frac{\partial^2 T_{iz}}{\partial z \partial t} \right)^2}_{\text{Penalties for cell temperature curvatures}}$$

Trajectory tracking of H₂ production rate

Deviations of manipulated (u_{ij}) and controlled variables (x_{ik}) from reference values

Rate of change penalties on trim heater duties

Penalties for cell temperature curvatures

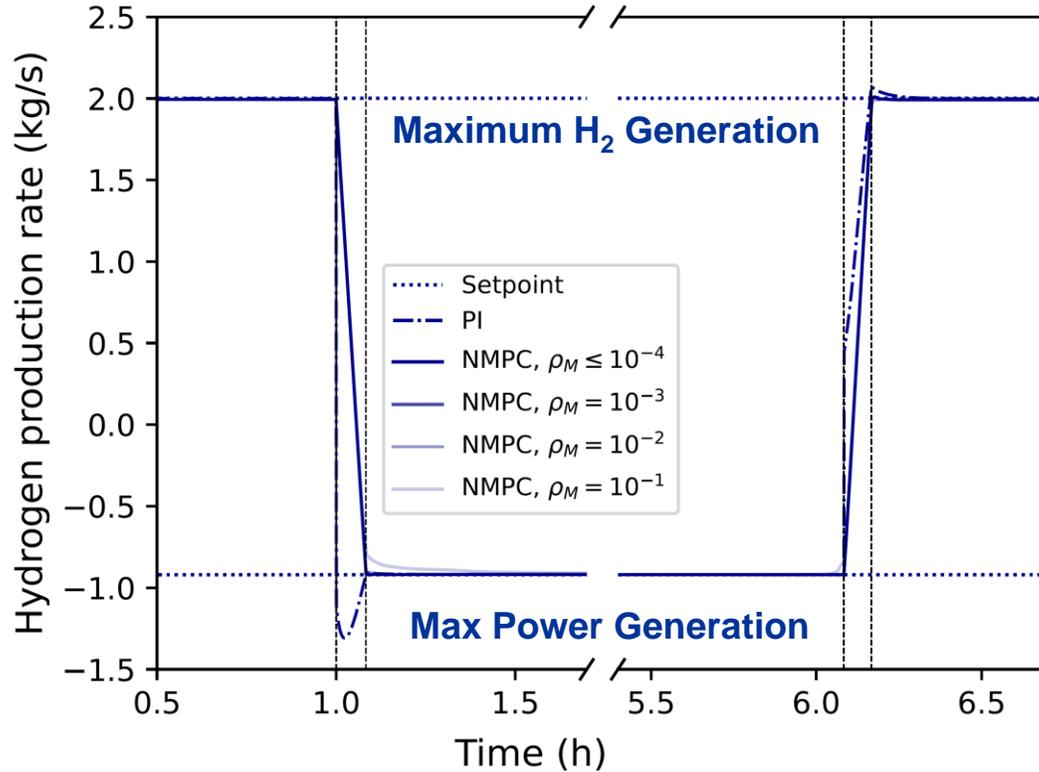
• Solution Approach

- Classical Control: PETSc variable step implicit Euler DAE solver
- NMPC: **Full-discretization** NLP with IPOPT solver

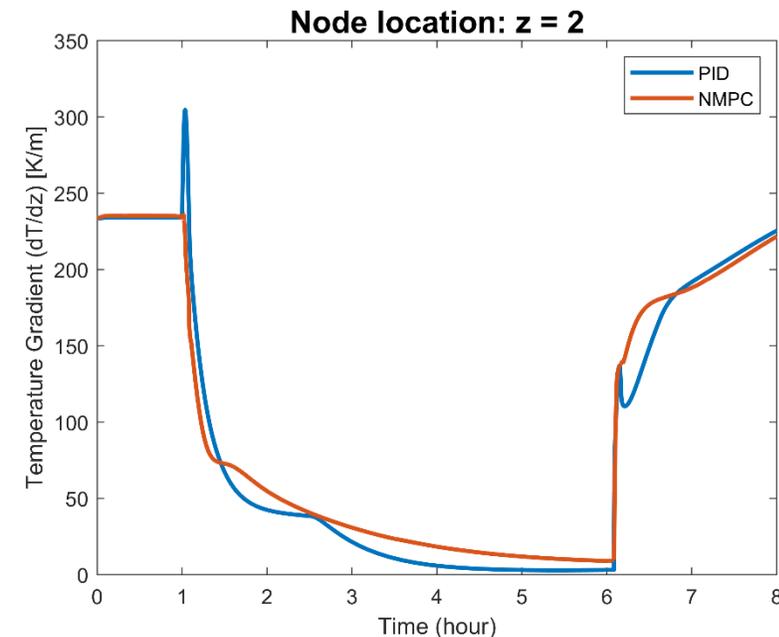
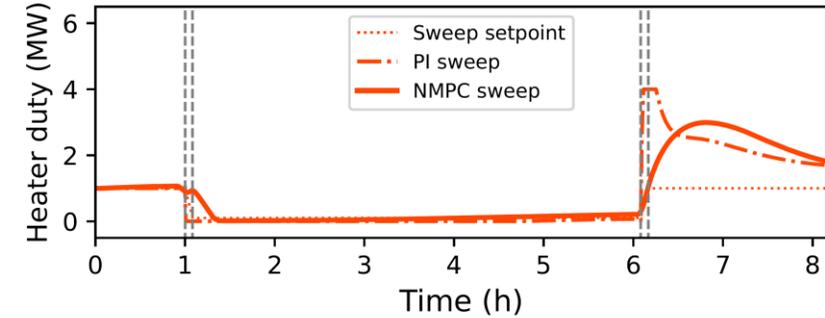
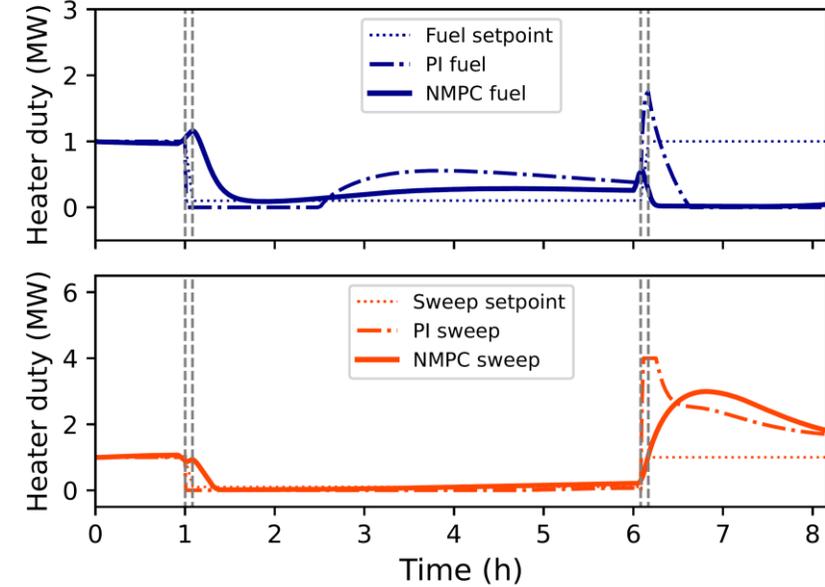
• NMPC Problem Size

- Approximately **16,000** equations and variables
- Average solution time of **35.5s** for a prediction horizon of **750s**
- Horizon size **N=5** with a sampling time of **150s**

Dynamic Simulation and Control Results for Ramping Operation



- **Classical PI control** of H₂ production rate shows **overshoot**, not exhibited by NMPC
- **NMPC** yields **smoother heater duty profiles** than PI control
- **NMPC** yields **smoother SOC temperature gradient** and lower spatial extremum magnitude than PI control



Conclusions

- **Long-term SOEC optimization** considering **chemical degradation** can be used to optimize **stack replacement schedule** and **operating trajectory**.
 - In **high-price** electricity markets, SOEC system **efficiency is maximized** at the expense of **more frequent stack replacements**.
 - In **low-price** electricity markets, SOEC system is operated under **more conservative conditions** to **reduce the frequency of stack replacements**.
- **Dynamic optimization** considering **physical degradation** can be used to optimize SOEC operating trajectories to **satisfy spatio-temporal stress constraints** without much sacrifice in the overall efficiency.
- **NMPC** can explicitly **restrict temperature gradients/curvatures or other constraints** compared to classical control.
- **IDAES** is a powerful modeling and optimization tool for analyzing **how to best operate and control** SOEC-based systems for **mode-switching (H₂/power)**, while **minimizing degradation** over long-term flexible operation.

IDAES Team and Funding Acknowledgements



The IDAES team gratefully acknowledges support from the U.S. DOE's Office of Fossil Energy and Carbon Management through the Simulation-Based Engineering Research Program.

idaes.org
github.com/IDAES/idaes-pse

National Energy Technology Laboratory: David Miller, Tony Burgard, Benjamin Omell, **Steve Zitney**, John Eslick, Andrew Lee, Miguel Zamarripa, Jinliang Ma, Chinedu Okoli, Arun Iyengar, Anca Ostace, Anuja Deshpande, Alex Noring, Naresh Susarla, **Doug Allan**, Radhakrishna Gooty, Ryan Hughes, Andres Calderon, Brandon Paul, Adam Atia, John Brewer, Nadejda Victor, Maojian Wang, Peng Liu, **Eric Liese**

Sandia National Laboratories: John Sirola, Bethany Nicholson, Michael Bynum, Jordan Jalving, Emma Johnson, Katherine Klise, Shawn Martin, Miranda Mundt, Edna Soraya Rawlings, Kyle Skolfield

Lawrence Berkeley National Laboratory: Deb Agarwal, Dan Gunter, Keith Beattie, John Shinn, Hamdy Elgammal, Joshua Boverhof, Karen Whitenack, Oluwamayowa Amusat

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2023 IDAES Technical Team Meeting, Lawrence Berkeley National Lab

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