

# Development of Thermal and Water Management System for PEM Fuel Cells

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**Honeywell**

## Honeywell Attendee

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## Agenda

- Overview
- Objectives
- Approach
- Accomplishments and Test Results
- Schedule & Milestones
- Collaborations
- Proposed Future Work

## Overview

### Timeline

- Project start FY03
- Program stopped FY05/06
- Project end date FY10
- 80% complete

### Budget

- Total project funding
  - DOE share - 3,250K
  - Honeywell - \$812K
- DOE funding in FY08 - \$500K
- DOE funding in FY09 - \$500K

### Barriers

- Balance water production and consumption of PEM fuel cell by humidification systems
- Performance of select full-scale humidification system
- Thermal performance of advance radiators to meet fuel cell stack cooling requirements

### Partners

- US Department of Energy
- Argonne National Lab
- FreedomCAR Tech Team

# Objectives

- Improve PEM fuel cell performance and life by maintaining the humidity of inlet air stream at a high level (> 60%)
- Eliminate need for external water source by transferring water from stack exit air stream to inlet stream
  - Validate performance of full-scale humidification devices sized for 80 kW PEM fuel cell
    - Test Emprise enthalpy wheel
    - Test Perma Pure membrane module
  - Evaluate planer membrane humidification devices
  - Performance testing at sub-ambient conditions
- Design, build and test high-performance full-size radiators to meet the 80 kW fuel cell stack cooling requirements
  - Increase performance required to dissipate low-quality heat
  - Optimize the weight, size, and cost

# Approach

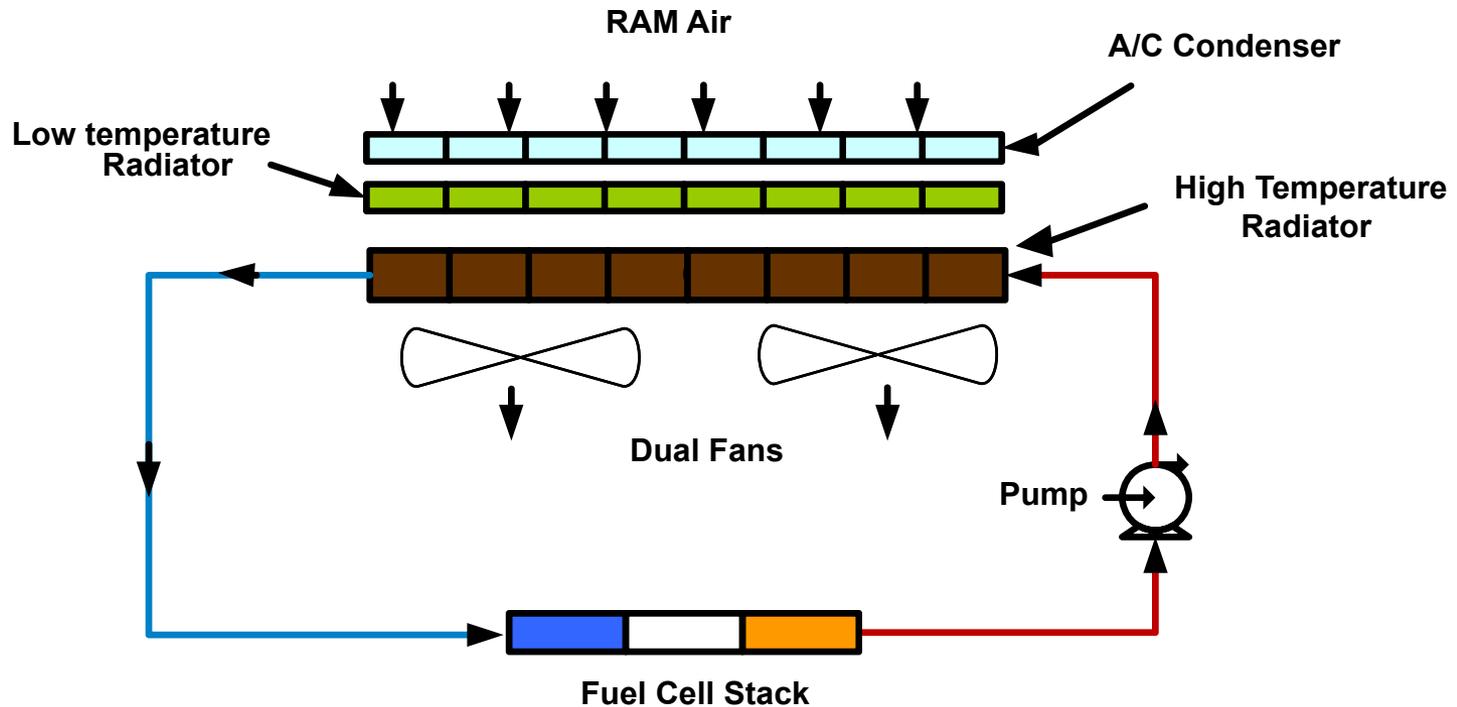
- The inlet air to the PEM fuel cell stack should have a minimum humidity of 60% (at 80 °C) to improve performance and increase stack life
- Two humidification systems were down-selected for the fuel cell application
  - Small-scale systems met the requirements
  - Full-scale units were built to validate the performance
    - Enthalpy Wheel (ceramic honeycomb) rotates while it adsorbs moisture from the fuel cell outlet air and transfers (de-sorbs) it to the inlet air
    - Nafion® membrane transfers moisture from one side of the air stream to the other side. The membrane has upper temperature limit which requires pre-cooler in the inlet air stream
- Planer membrane-based humidification systems are being evaluated
- Value function was developed to compare radiators with different fin geometries
- Two designs were down-selected for full-scale radiator testing

## Accomplishments for FY08/09

- Fuel stack radiator requirements were established based on Argonne National Lab's PEM fuel cell automotive system model
- Value function was developed for evaluation of various configurations
- Four different fin configuration sub-scale radiators built and tested
- Validated full-scale performance model
- Lesson learned for brazing & assembly for microchannel radiators
- Designed and built full-scale radiators with optimized fin configurations
- Conducted testing of humidity device at low air flow rate
- Enthalpy wheel modified to reduce seal leakage
- Humidification test stand modification underway for higher air flow rate capability and improved measurement accuracy

## Thermal Management System Schematic

High Temp. HX heat load	50 kW	Radiator Area	27.6 X17.7 inch
RAM air inlet temp.	40°C	Max allowable depth	2.8 inch
Radiator 20% larger than ICE radiators			



**Requirements were established based on ANL model**

## Value Function for Radiator

$$VF = a\left(\frac{D}{FE^*}\right)C_F + [bC_{FCS} - c\left(\frac{D}{FE^*}\right)C_F] + C_T$$

(I)                      (II)                      (III)                      (IV)

I: Additional weight -> Lower fuel economy -> Higher fuel cost

II: Higher parasitic power -> Larger fuel cell system -> Higher initial cost

III: Larger stack -> Higher efficiency at part load -> Lower fuel cost

IV: Thermal management system initial cost

$$a = \beta_W \left( \frac{(W_T - W_T^*) + (P_T - P_T^*) / \hat{P}_{FCS}}{W_{GVW}} \right)$$

$$b = \frac{P_T - P_T^*}{P_{FCS}^*}$$

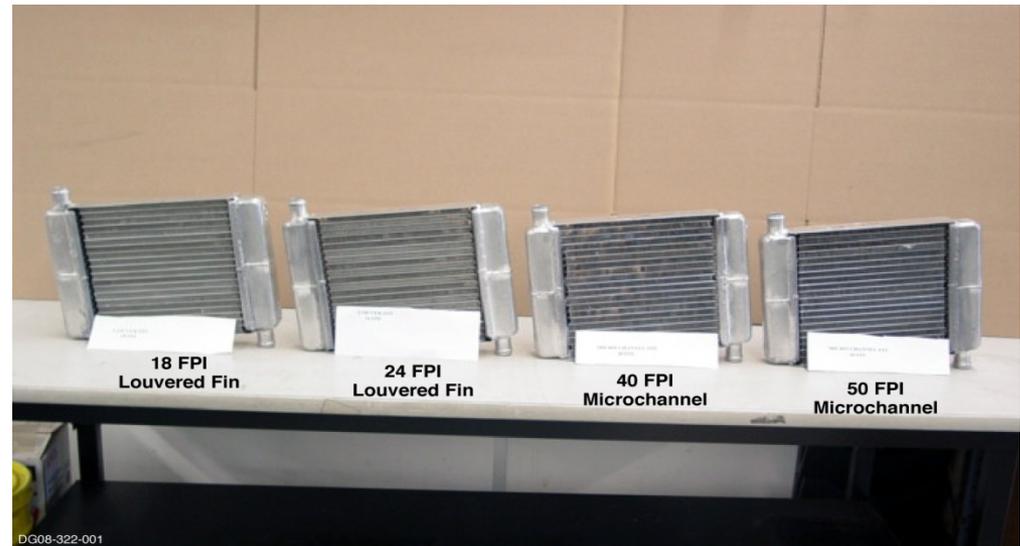
$$c = \beta_P \left( \frac{P_T - P_T^*}{P_{FCS}^*} \right)$$

### Nomenclature Symbol

$C_F$	Fuel cost	3 \$/kg
$C_{FCS}$	FCS initial cost	4800 \$
$C_T$	TMS initial cost	
$D$	Driving Distance	100,000 miles
$FE^*$	Fuel economy	60 miles/kg-H <sub>2</sub>
$P_T$	TMS parasitic power	
$P_T^*$	Reference TMS parasitic power	1.5 kW <sub>e</sub>
$P_{FCS}^*$	FCS power	80 kW <sub>e</sub>
$W_T$	TMS weight	
$W_T^*$	Reference TMS weight	40 kg
$W_{GVW}$	Gross vehicle weight	1920 kg
$\hat{P}_{res}$	FCS specific power	0.65 kW <sub>e</sub> /kg
$\beta_W$	Effect of weight on FE	0.8
$\beta_P$	Effect of parasitic power on FE	0.1

# Sub-scale Radiators Testing

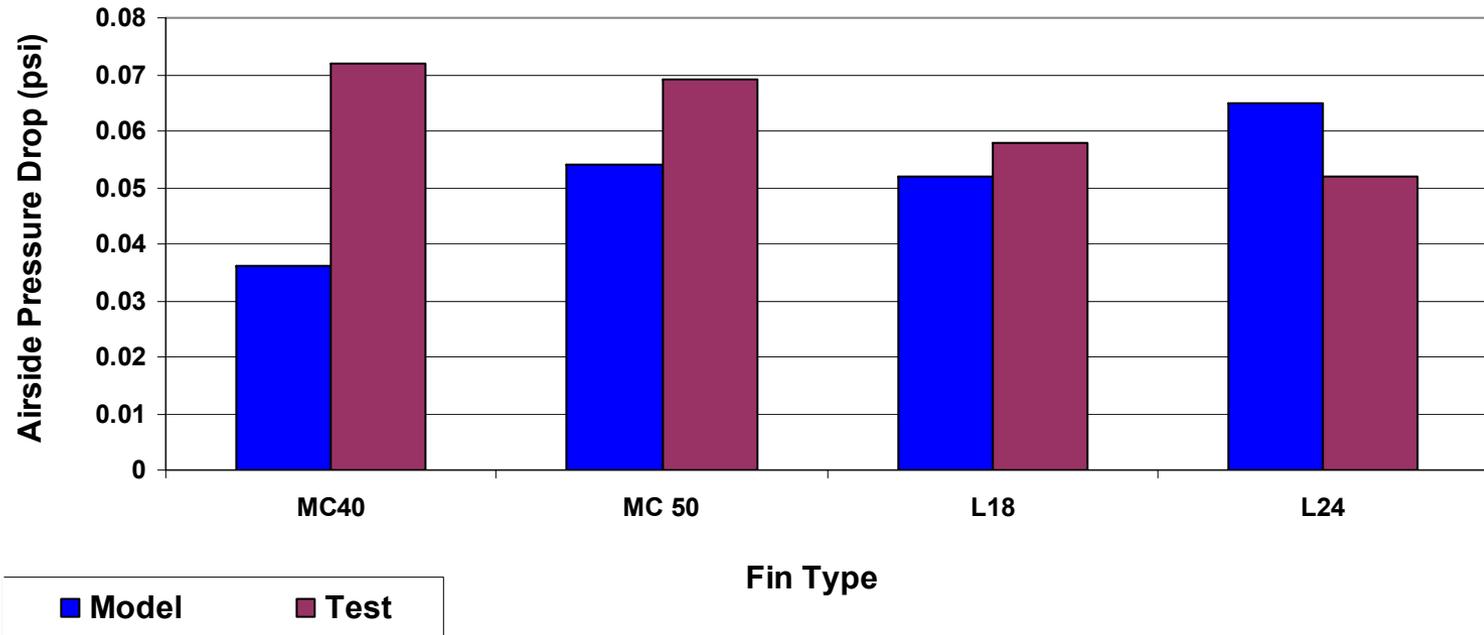
- Sub-scale (9"x 9"x 1.3") radiators were built to validate:
  - Thermal performance
  - Manufacturability of microchannel fin radiators
- Updated full-scale radiator design/performance model
- Four fins were selected:
  - 18 fins/inch (fpi) Louver fins
  - 24 fpi Advance Louver
  - 40 fpi Microchannel fins
  - 50 fpi Microchannel



***Manufacturability with advance fins demonstrated***

## Sub-scale Radiator Test Data & Model Prediction

Coolant flow of 19.4 gpm at 50 kW design condition

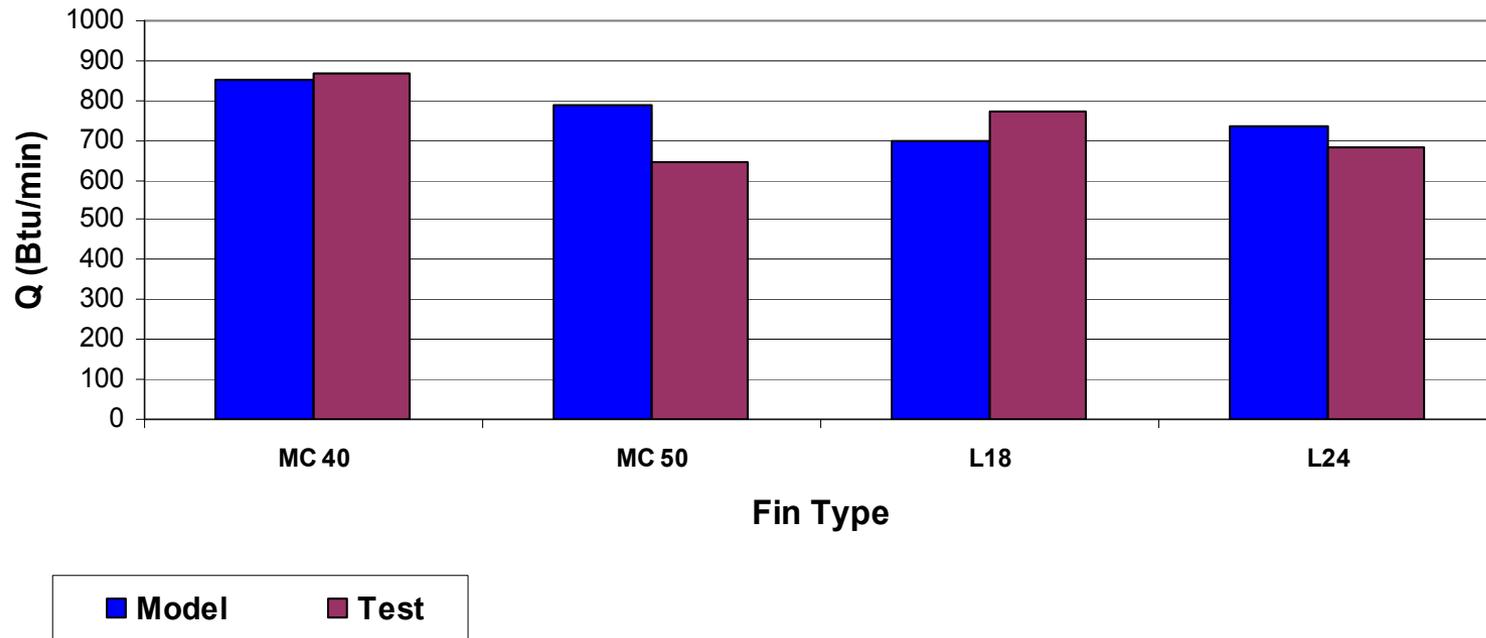


MC – Microchannel fins    L – Louver fins

***40 fpi MC pressure drop test data being verified***

## Sub-scale Radiator Test Data & Model Prediction

Coolant flow of 19.4 gpm at 50 kW design condition



MC – Microchannel fins    L – Louver fins

***Test data validated model predictions***

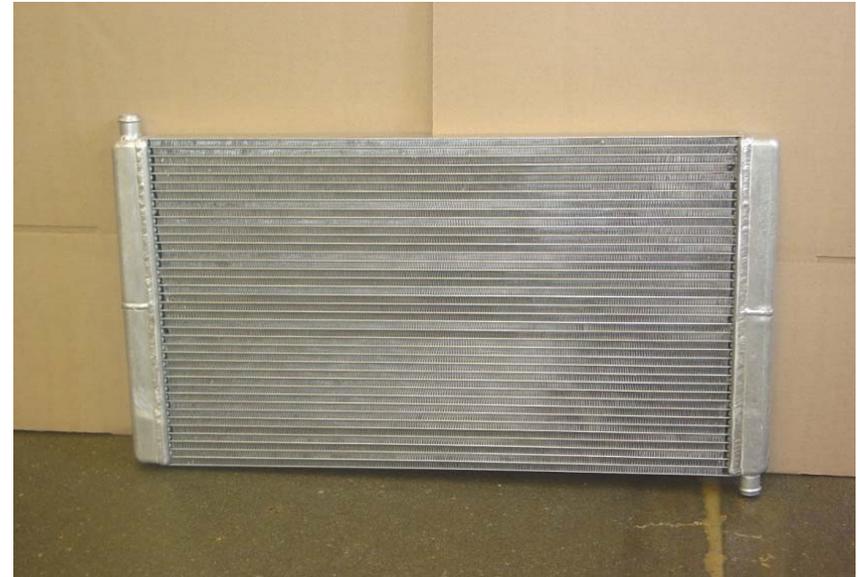
## Full-Scale Radiators

**Size of the radiator 27.6"W, 17.7"H & 1.3"Depth**

**Estimated weight of full-scale louver and microchannel radiator (with plastic tanks) will be 10 and 13 lbs respectively**



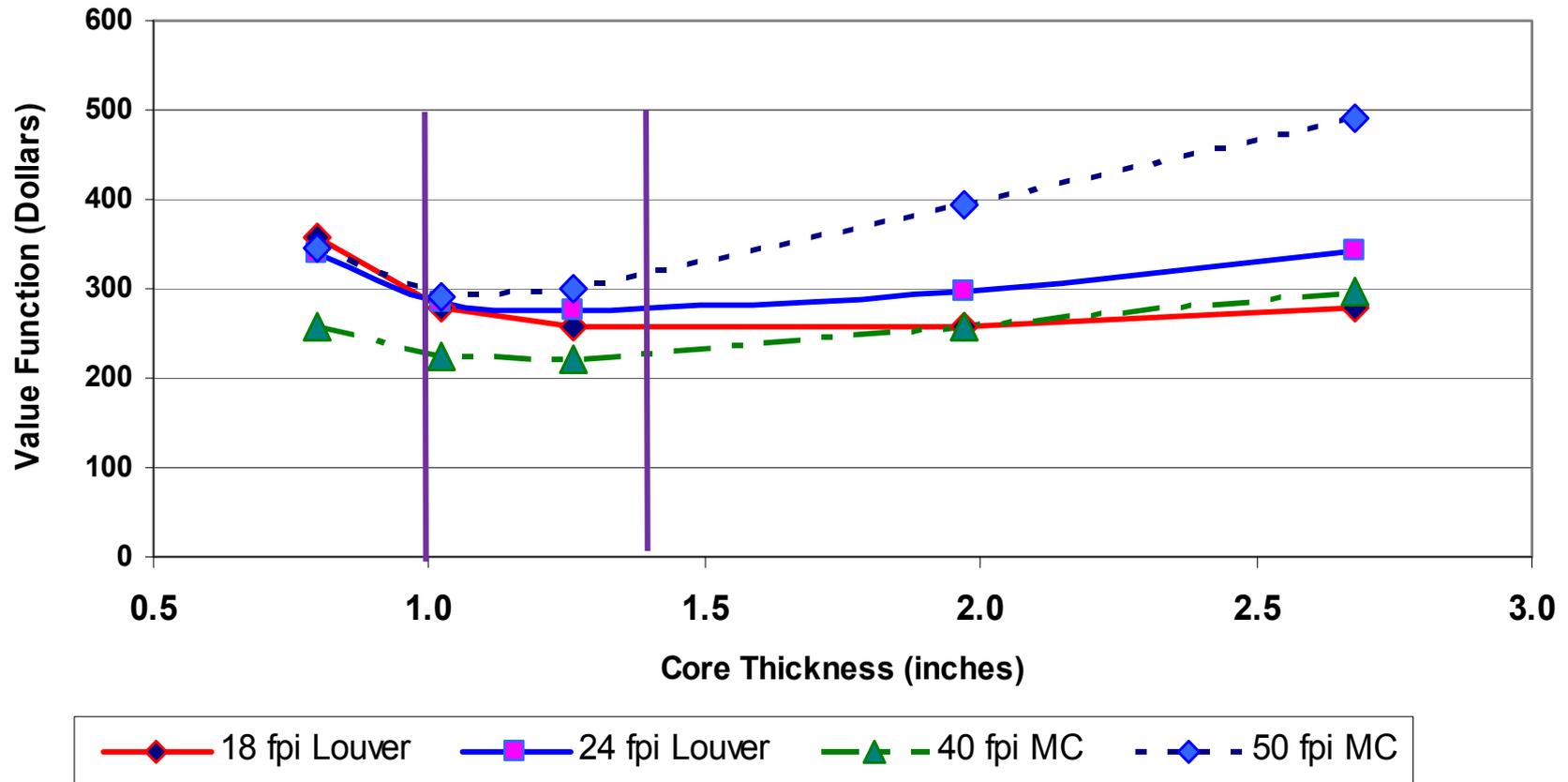
**40 fins/in. Microchannel Fins**



**18 fins/in. Louver Fins**

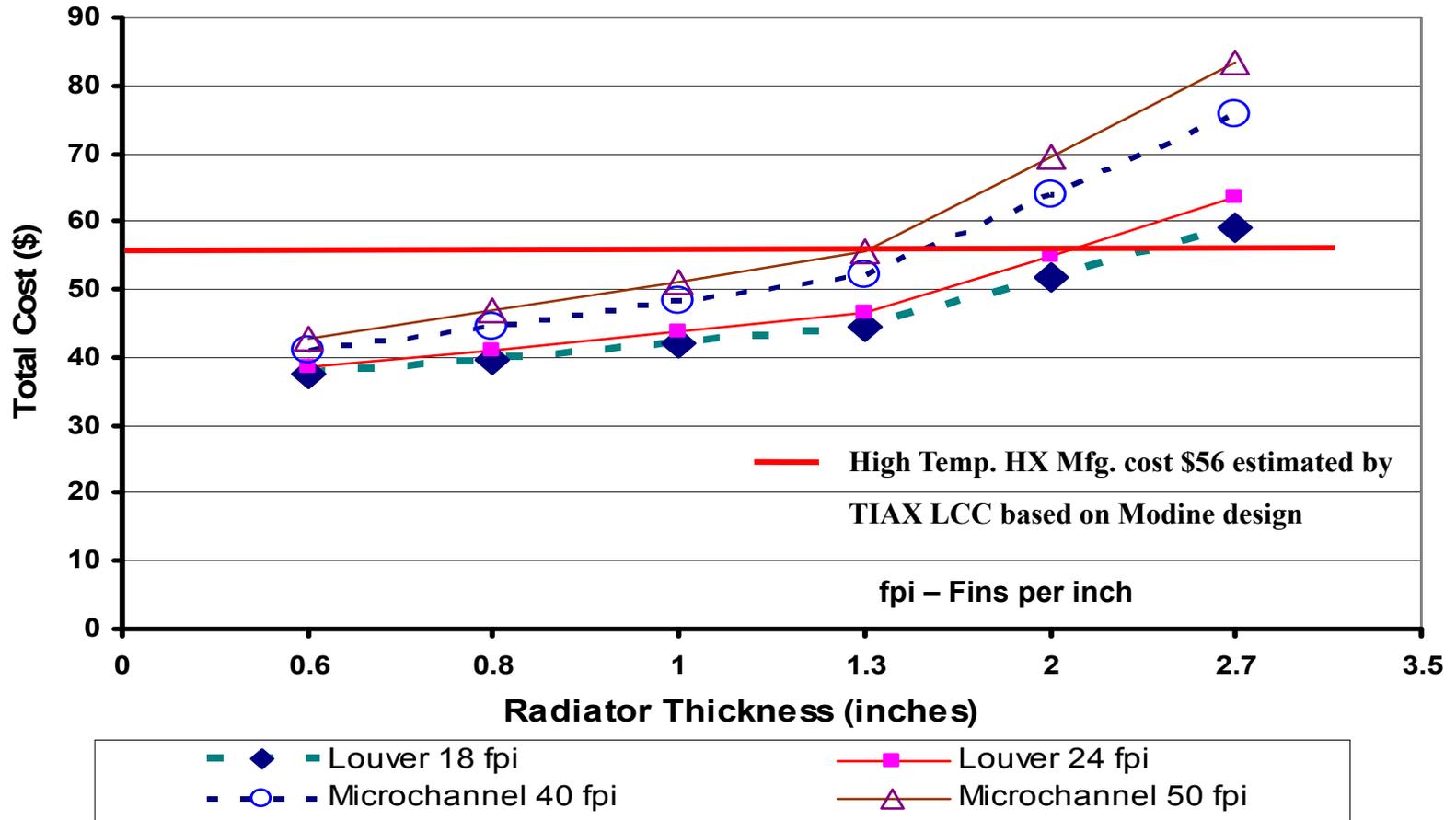
***Full size microchannel radiators built successfully***

## Value Comparison



**Optimum value with 18 Finslin Louver & 40 fpi microchannel fins with core thickness of 1-1.4 in**

## Cost of Full-Scale Radiators

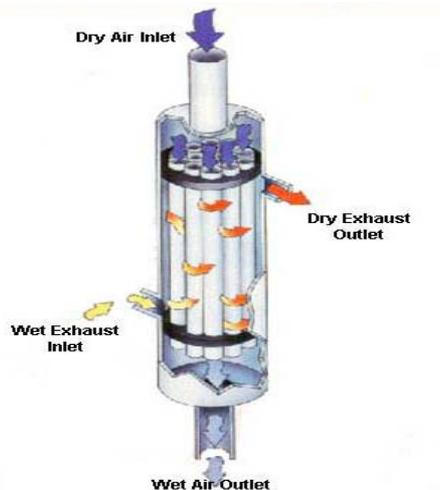


***Louver fins are lower cost and weight***

## Humidification Devices

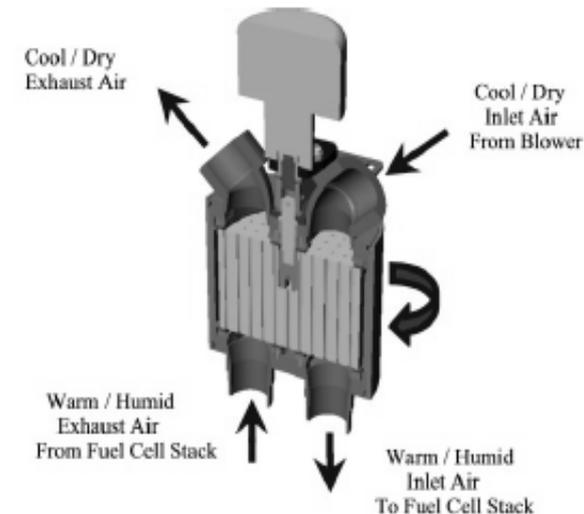
### Membrane Module by Perma Pure

- Membrane selectively allows water to pass through
- Performance sensitive to temp.
- 6" Ø, 10" length cartridge
- 7000 fibers 0.045" OD
- 11.13 in<sup>2</sup> Nafion



### Enthalpy Wheel By Emprise

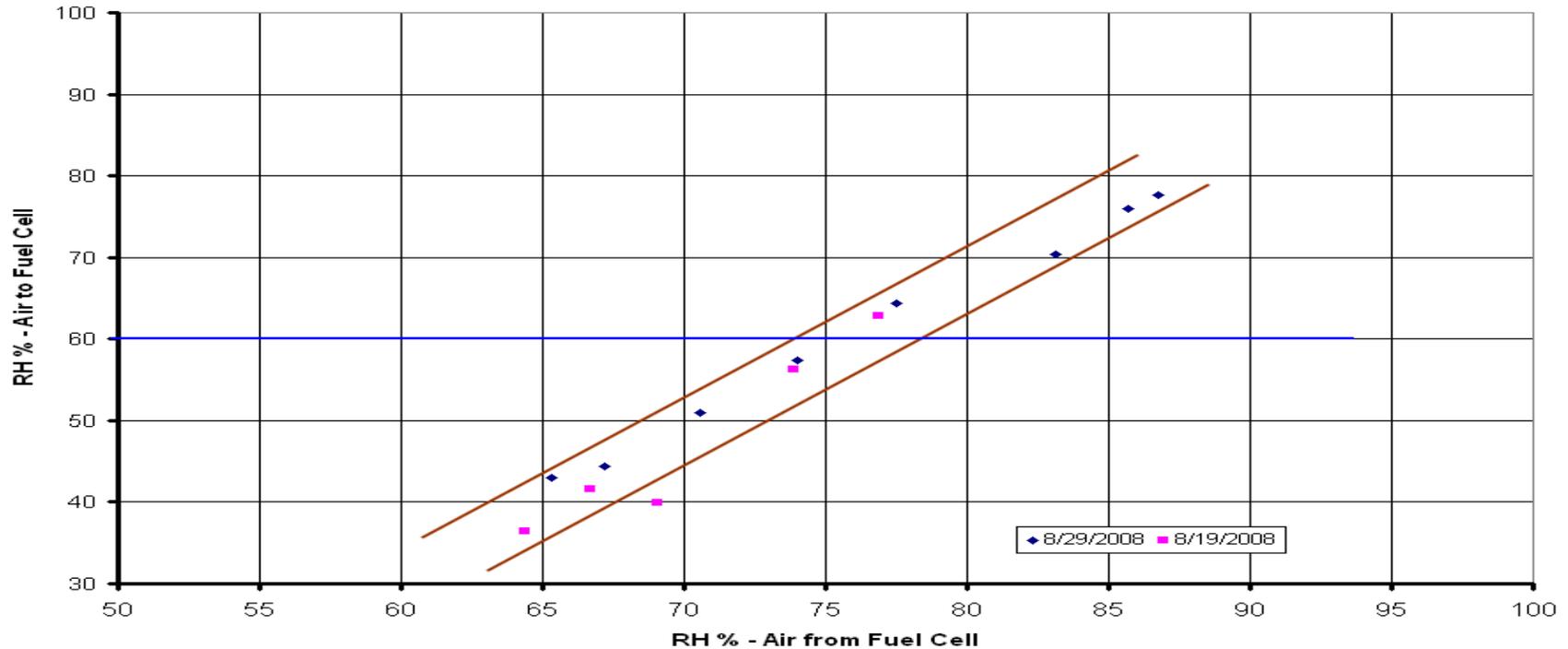
- Water adsorbed and de-sorbed in a rotating wheel
- Power: < 100W
- Leakage < 1% process flow
- 8" Ø, 6" length wheel
- Vol: 17l cu in.; Wt: 17 kg



## Half Scale Membrane Module Test Data

Test operating temperature 70-80 °C  
 Fuel cell stack exit air will be 100% saturated

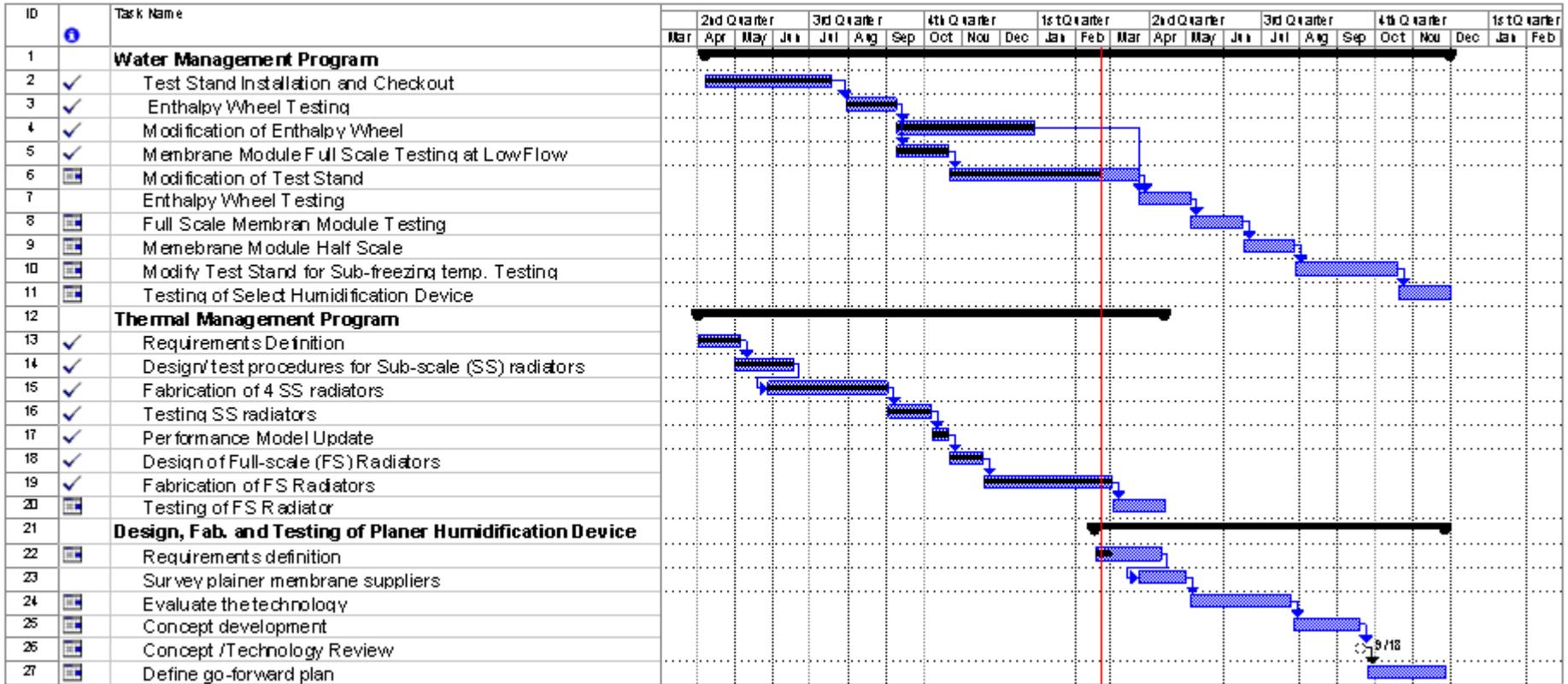
Air flow rate 1 lb/min.  
 Water mass balance within 10%



**Humidity of >75% in fuel exit air satisfies stack requirements**



## FY08/09 Schedule and Major Milestones



- Thermal Management program kickoff** 4/1/08
- Fabrication and testing of Sub-scale radiators** 10/6/08
- Testing of full-scale radiators** 4/13/09
- Complete testing of humidification devices** 7/27/09
- Planer Membrane system evaluation complete** 9/18/09

## Proposed Future Work

- Complete test stand modifications for higher air flow rate and improved humidity measurement accuracy
- Test modified Enthalpy wheel
- Test full and half scale Membrane Module
- Test full-scale radiators
- Evaluate planer membrane-based humidification devices for fuel cell application
- Test selected full-scale planer device to validate performance
- Test the selected humidification device at sub-ambient operating conditions