Biomass-derived Liquids Distributed (Aqueous Phase) Reforming

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DOE Merit Review
June 8, 2010

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Overview

Timeline
- Project start date: Oct. 1, 2004
- Two projects consolidated in 2007
  - Aqueous phase reforming of sugar and sugar alcohols
  - Vapor phase reforming of ethanol
- Percent complete: 80%

Barriers
A: Reformer Capital Cost
C: Operation & Maintenance
D: Feedstock Issues
E. Greenhouse Gas Emissions

Budget
- Funding received in FY04: $100K
- Funding received in FY05: $500K
- Funding received in FY06: $0K
- Funding for FY07: $550K
- Funding for FY08: $600K
- Funding for FY09: $600K
- Funding for FY10: $450K

Collaborations
- ORNL—high resolution TEM studies
Project Objective

- Develop bio-derived liquids aqueous phase reforming technology for hydrogen production that can meet the DOE efficiency and cost targets
  - Enhance catalyst performance by increasing catalyst activity and hydrogen selectivity
  - Develop mechanistic understanding of reaction pathways and means to control product distributions consistent with application end-use

DOE 2017 Target: <$3/gge
<table>
<thead>
<tr>
<th><strong>Aqueous Phase Reforming</strong></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>Summarize effect of catalyst and support pretreatment and preparation methods on performance of Pt/C and Pt-Re/C catalysts</td>
<td>9/30/09 milestone met</td>
</tr>
<tr>
<td>Provide a report summarizing kinetic data, catalytic and non-catalytic reaction pathways, and pH effects with glycerol and sorbitol feedstock</td>
<td>9/30/09 milestone met (glycerol only)</td>
</tr>
<tr>
<td>Preliminary process economic analysis for CH₄ co-production for solid oxide fuel cell application</td>
<td>1/31/10 (complete)</td>
</tr>
<tr>
<td>Complete process and catalyst optimization to maximize H₂ and C₁ with glycerol feed</td>
<td>4/30/2010 milestone met</td>
</tr>
<tr>
<td>Demonstrate full conversion of glucose/sorbitol with &lt;5% carbon retained as C₂⁺ oxygenated product</td>
<td>9/30/2010 in progress</td>
</tr>
</tbody>
</table>
Technical Approach

- Detailed study of Pt-Re/C catalyst
  - Compare catalytic performance with Pt/C with glycerol
  - Quantify the effect of Re addition on Pt/C performance
    - Activity
    - Product selectivity—modification of reaction pathways
  - Develop advanced catalyst characterization methods to understand interactions between the components
    - XPS analysis of metal oxidation state changes (PNNL-EMSL)
    - XANES analysis of Pt-Re interaction (BNL)
    - In situ TEM for changes in metal dispersion (Ariz State, ORNL)
- Examine and quantify effect of base addition on catalyst performance
- Evaluate options for co-production of hydrogen with CH₄ for compatibility with SOFC for power generation
- Extend knowledge of glycerol APR to sorbitol APR
Recent Progress on APR

- Found evidence for dual-functionality of Pt-Re/C under hydrothermal APR environment:
  - Pt-Re alloy formation provides increased activity toward H₂ production
  - Acidic ReOx present facilitates alternate reaction pathways

- Advanced the understanding of glycerol APR over Pt-Re/C
  - Addition of Re increases conversion of glycerol, but also provides additional reaction pathways competing with H₂-generating C-C cleavage pathway
  - ReOx formed under APR conditions facilitates C-O scission, which consumes H₂ and leads to higher selectivity to alcohols and C₂⁺ alkanes
  - H₂ productivity increases with addition of Re at expense of H₂ selectivity
  - Addition of KOH to glycerol feed over Pt-Re/C neutralizes acidity of ReOx and depresses C-O scission pathways, resulting in increased H₂ yield via C-C cleavage

- Preliminary results from APR of sorbitol have been obtained
Fuel Production From Reforming Of Bio-liquids

Agriculture
- Rotational crops
- Energy crops (switch grass, poplar, etc)
- Oil crops
- Rotational crop residue (stover, wheat & rice straws, etc)

C5, C6 sugars:
Xylose, Arabinose
Glucose
Or sugar alcohols

Hydrolysis:
Acid or Enzymatic

Reforming

Fuel

Aqueous phase reforming

Operates at low temperatures compared with conventional reforming, reducing energy costs and favoring water gas shift reaction

Allows processing of biomass feedstock that are difficult to vaporize without decomposition

Compatible with wet feedstock utilization

Forest residue

Proudly Operated by Battelle Since 1965
Reaction Test on APR of Glycerol

- Isothermal microchannel reactor with oil heating jacket
- Aqueous feed is pumped into the reactor with pre-heating
- Catalyst is reduced in-situ at 280 °C before use.
- Reaction runs typically at 225 °C, 420 psig.

Pt is chosen based on its good activity for C-C cleavage
Carbon is chosen as the support due to its higher hydrothermal stability than silica and alumina
Catalyst Preparation: Incipient Wetness Impregnation

- **Pt(NH$_3$)$_4$(NO$_3$)$_2$**
- **HReO$_4$**

BET 570 m$^2$/g
P.V. 0.42 cc/g
## Prepared Catalysts—Metal Surface Areas and Dispersion

<table>
<thead>
<tr>
<th>Catalyst</th>
<th>Pt (wt.%)*</th>
<th>Re (wt.%)*</th>
<th>CO uptake (μmol/g)</th>
<th>H uptake (μmol/g)</th>
<th>H/CO</th>
<th>Metal Dispersion (%)**</th>
</tr>
</thead>
<tbody>
<tr>
<td>3%Pt/C</td>
<td>3</td>
<td>0</td>
<td>116.2</td>
<td>147.4</td>
<td>1.27</td>
<td>75.6</td>
</tr>
<tr>
<td>3%Pt1%Re/C</td>
<td>3</td>
<td>1</td>
<td>69.5</td>
<td></td>
<td></td>
<td>45.2</td>
</tr>
<tr>
<td>3%Pt3%Re/C</td>
<td>3</td>
<td>3</td>
<td>67.1</td>
<td>116.5</td>
<td>1.74</td>
<td>43.6</td>
</tr>
<tr>
<td>3%Re/C</td>
<td>0</td>
<td>3</td>
<td>0.9</td>
<td>0.8</td>
<td></td>
<td>N/A</td>
</tr>
</tbody>
</table>

* wt.% -- g metal/100g carbon  ** based on CO chemisorption
Addition of Re to Pt/C Results in ..... 

**Higher Activity**

**Different Selectivity**

![Graph showing TOF (min$^{-1}$) with Addition of Re](image)

![Graph showing Selectivity (carbon based)](image)

$T = 226 \, ^\circ\text{C}, P = 420 \, \text{psig}, \text{feed rate} = 0.06 \, \text{moles glycerol/gcat-h}; \text{TOF is calculated based on CO chemisorption}$

- Addition of Re results in significant enhancement in activity and different selectivity
- What is the role of Re?
Elucidating the Role of Re by Characterization and Testing

Electronic Structure of PtRe/C under H₂ pretreatment

Structure and composition of PtRe/C under hydrothermal conditions

Correlation with activity and selectivity
Modification of Pt Electronic Structure by Addition of Re

► Addition of Re retards reduction of Pt at lower temperature

► Pt appears to facilitate reduction of Re at 80°C

► Binding energies of Pt increase with addition of Re when reduced at 280°C, suggesting charge transfer from Pt to Re
Fully Reduced Pt and Re Results in Higher Activity

- Reduction at 280 °C fully reduces Pt and Re, which may forms Pt-Re alloy particles.
- Fully reduced Pt and Re results in higher activity.

3%Pt-3%Re/C

T = 226 °C, P = 420 psig, feed rate = 0.06 moles glycerol/gcat-h

TOF is calculated based on CO chemisorption
EDS Shows Pt Rich and Re Rich Particles

3Pt3Re/C, reduced

Pt-Re phase diagram also predicts Pt-rich phase and Re-rich phase
Concentration profile

Line scan or spot scans on single particles shows uniform Pt and Re composition in the bulk part of particles, indicating formation of Pt-Re alloy.
Summary on Pt-Re interaction after reduction

- Pt facilitates the reduction of Re

- Reduction at 280°C is required to fully reduce Pt and Re and maximize activity of glycerol APR

- Charge transfer (XPS) and uniform composition (TEM) suggests formation of Pt-Re bimetallic particles

- Modification of Pt electronic structure may account for enhancement of activity.
Pt-Re Interaction under Hydrothermal conditions

Exposure to water results in oxidation of Re and Pt (Pt to a much smaller extent)

Surface ReOx may form under hydrothermal conditions
Model Catalyst (Pt:Re=1:1)

- Reduction was carried out in the airlock chamber of TEM. The non-flowing system allows small amount of residual water on the surface, similar to hydrothermal conditions in APR process.
- The Pt-Re/C consists of 2 phases
  - PtRe bimetallic phase rich in Pt
  - Pt embedded in a ReOx rich phase
- Oxygen is detected in Re rich phase.
**Dual-Functionality of Pt-Re**

**TOF (min⁻¹) with Addition of Re**

- Glycerol
- H2
- CO2
- Alkane
- Liquid

- 3%Pt3%Re/C
- 3%Pt1%Re/C
- 3%Pt/C

**Selectivity (carbon based)**

- H2
- CO2
- C2+ Alkane
- Diol
- Alcohol
- Acid

- 3%Pt/C
- 3%Pt3%Re/C

Conversion: 34% for 3%Pt3%Re/C
26% for 3%Pt/C

T = 226 °C, P = 420 psig, feed rate = 0.06 moles glycerol/gcat-h

TOF is calculated based on CO chemisorption

**What is the role of Re?**

Electronic effects from alloying (PtRe)

Separate reaction pathways due to oxidized Re (ReOx)
Definition of Competition Ratio: C-O vs. C-C Scission

C-O Scission = Sum of all dehydrated products for each dehydration step by mole

C-C Scission = Moles of CO₂
Addition of Re Facilitates the Dehydration Reaction (C-O Scission Pathway)

C-O scission/C-C scission (competition ratio) for different PtRe ratio

- Supported ReOx has been reported to be acidic. NH₃ TPD confirmed acidity of ReOx
- Larger amount of Re added to Pt results in higher dehydration selectivity (effect of ReOx)
Addition of Re Affects Hydrogen Selectivity

- H₂ selectivity is defined as measured H₂ yield over theoretical H₂ yield from converted glycerol
- Higher Pt/Re ratio resulted in higher H₂ selectivity
- Lower hydrogen selectivity with addition of Re is due to more consumption of H₂ through C-O cleavage pathway (more ReOx)

Reaction @ 225°C, 420 psig
Addition of Re Affects Reaction Pathways

- Lower hydrogen selectivity with addition of Re indicates more hydrogen consumed by dehydration pathways.
- Dehydration pathways result in less accumulation of diols and more formation of alcohols and C$_2^+$ alkanes.
Effect of Addition of KOH on Glycerol APR over Pt-Re/C

Selectivity to Gas Phase Products on 3%Pt3%Re/C

Selectivity to Liquid Phase Products on 3%Pt3%Re/C

Addition of KOH neutralizes acidity of ReOx and depresses dehydration pathways over Pt-Re/C, resulting in less alkanes and alcohols.

Lower selectivity to dehydration results in higher RHY.

KOH also facilitates the Canizzaro reaction, resulting in more acids and diols in the liquid products.
Conclusions on Pt-Re and the Role of Re

- Pt facilitates the reduction of Re.
- Reduction at 280°C is required to fully reduce Re and maximize the catalyst activity.
- Under reaction conditions, the surface of Pt-Re/C appears to consist of:
  - A PtRe bimetallic phase
  - A ReOx-rich phase
- Re increases the activity of the Pt/C catalyst by:
  - Electronic effect – charge migration in PtRe bimetallic particles
  - Facilitating dehydration pathways → ReOx rich phase (acid sites)
- Addition of base neutralizes the acidity of ReOx and results in lower alkane selectivity and higher H₂/CO₂.
Potential Linkage of APR with Solid Oxide Fuel Cell (SOFC) Operation

- SOFC is more tolerant of impurities and flexible in feedstock than PEMFC, for example CH₄ byproduct has feedstock value with SOFC.

- Orienting the APR product distribution toward a SOFC-compatible feed might provide benefits in catalyst operation and/or process efficiency.

- Our results have shown that high H₂ selectivity and methane/alkane selectivity can be achieved by adjusting reaction conditions such as flow rate and adding base.
By lowering flow rate and increasing residence time, high $H_2$ and $CH_4$ selectivity can be achieved with minimal liquid phase byproduct.
Study of Glycerol APR for SOFC Application with Base Addition

At 100% conversion, addition of base increases hydrogen selectivity and depresses production of $C_2^+$ alkanes, favoring CH$_4$. 
Extend the Lesson Learned to APR of Sorbitol

Dehydration is more favored on polyols and longer chain polyols which results in lower H$_2$ selectivity.

![Graph showing H$_2$ selectivity for different feeds](image-url)
APR of Sorbitol

- 5%Pt-3%Re/C showed the highest activity and selectivity
- Conditions favoring high H₂ selectivity:
  - 225-230°C and 370-415 psig
  - Longer contact time
  - Addition of base
- Hydrogen selectivity is lower with sorbitol than with glycerol under otherwise similar conditions
Preliminary Economic Analysis on Bio-Liquid Aqueous Phase Reforming for SOFC Feed
Bio-Alcohol Fuel Options

- Ethanol, Glycerol (refined), and Sorbitol (70 wt%) are all currently priced at about $0.30/lb.
- Energy content per gallon much higher for ethanol.
- Current $/MMBtu (based on HHV of fuel)
  - Ethanol - $21/MMBtu
  - Glycerol - $39/MMBtu
  - Sorbitol - $60/MMBtu
Bio-Alcohol Markets

 ► Ethanol already established as significant liquid fuel.

 ► Byproduct production of glycerol from biodiesel production is driving glycerol price down. European requirements for increased biodiesel use is expected to drive glycerol price down further.

 ► Sorbitol price primarily driven by market for high-fructose corn syrup, but can be produced from any source of glucose.
Aqueous Phase Reforming of Sorbitol
Performance

Reformate Fuel Per Mole Sorbitol

- Hydrogen – 6.6 mole
- Methane – 1.0 mole
- Ethane – 0.2 mole
- Propane – 0.1 mole

Conversion Efficiency = 79% if reformate provides reformation energy

Conversion Efficiency = 109% if SOFC provides reformation energy
## APR Direct Capital Costs

(ASPEN Process Economic Evaluator; March 31 2008 dollars)

### Process Sized for 1 MW SOFC First-Cut Design

<table>
<thead>
<tr>
<th>Component</th>
<th>Direct Equipment, Material &amp; Labor</th>
</tr>
</thead>
<tbody>
<tr>
<td>Aqueous Phase Reformer</td>
<td>294,200</td>
</tr>
<tr>
<td>Reformate Cooler</td>
<td>236,700</td>
</tr>
<tr>
<td>APR Feed Mixing Tank</td>
<td>163,100</td>
</tr>
<tr>
<td>Reformate Flash Tank</td>
<td>123,600</td>
</tr>
<tr>
<td>APR Feed Preheater</td>
<td>140,700</td>
</tr>
<tr>
<td>Sorbitol Feed Pump</td>
<td>31,400</td>
</tr>
<tr>
<td>High Pressure Pump</td>
<td>74,300</td>
</tr>
<tr>
<td>Recycle Pump</td>
<td>31,300</td>
</tr>
<tr>
<td>Sorbitol Storage Tank</td>
<td>250,600</td>
</tr>
<tr>
<td><strong>Total</strong></td>
<td><strong>1,345,900</strong></td>
</tr>
</tbody>
</table>

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Levelized Cost of Reformate
$/kg H_2\text{-equivalent}

- Energy content of reformate constituents combined into equivalent quantity of hydrogen
- Cost includes feedstock, capital, and annual O&M costs
- Uses standard H2A assumptions for indirect construction costs, and annual O&M for distributed H_2 production.
- Levelized cost calculated for four scenarios.
  - $0.30/lb and $0.12/lb 70% sorbitol feedstock costs
  - Use of reformate or SOFC waste heat for reforming energy
Levelized Cost Results, $/kg H₂-equivalent
Sorbitol feedstock represents 95+% of hydrogen cost

<table>
<thead>
<tr>
<th>Reforming Energy Source</th>
<th>70% Sorbitol @ $0.12/lb</th>
<th>70% Sorbitol @ $0.30/lb</th>
</tr>
</thead>
<tbody>
<tr>
<td>Fuel Cell Waste Heat</td>
<td>3.06</td>
<td>7.61</td>
</tr>
<tr>
<td>Reformate</td>
<td>4.29</td>
<td>10.65</td>
</tr>
</tbody>
</table>