



Solarthermal Redox-based Water Splitting Cycles

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Project ID No. PD028



Overview

Timeline

- Start: 6-1-2005
- End: 9-30-2013
- 80% completed

Budget

- Total Project Funding
 - 2005-2011: \$1,210K DOE
 - \$347,500 Cost Share
- Funds received in FY12
 - \$217,000 (subcontract from SNL)
 - \$ 54,250 Cost Share
- Planned FY2013 Funding
 - \$250,000 (subcontract from SNL)

Barriers

U. High-Temperature Thermochemical Technology

V. High-Temperature Robust Materials

W. Concentrated Solar Energy Capital Cost

X. Coupling Concentrated Solar Energy and Thermochemical cycles

Partners

National Renewable Energy Laboratory (NREL)

Sandia National Laboratories (SNL)



Relevance

- Objective - Develop and demonstrate robust materials for a two-step thermochemical redox cycle that will integrate easily into a scalable solar-thermal reactor design and will achieve the DOE cost targets for solar hydrogen:
(\$14.80/kg H₂ in 2015; \$3.70/kg H₂ in 2020; ultimately \$2/kg H₂)

Milestone – “Synthesize a cobalt ferrite/alumina “hercynite” active material by ALD using polymer templates. Demonstrate isothermal redox water-splitting in a stagnation flow reactor at a temperature of 1350°C yielding a H₂ production per gram of total mass of active material > 100 μmoles/g active material.” (> 200 μmoles/g active material achieved in 3/2013)



Approach

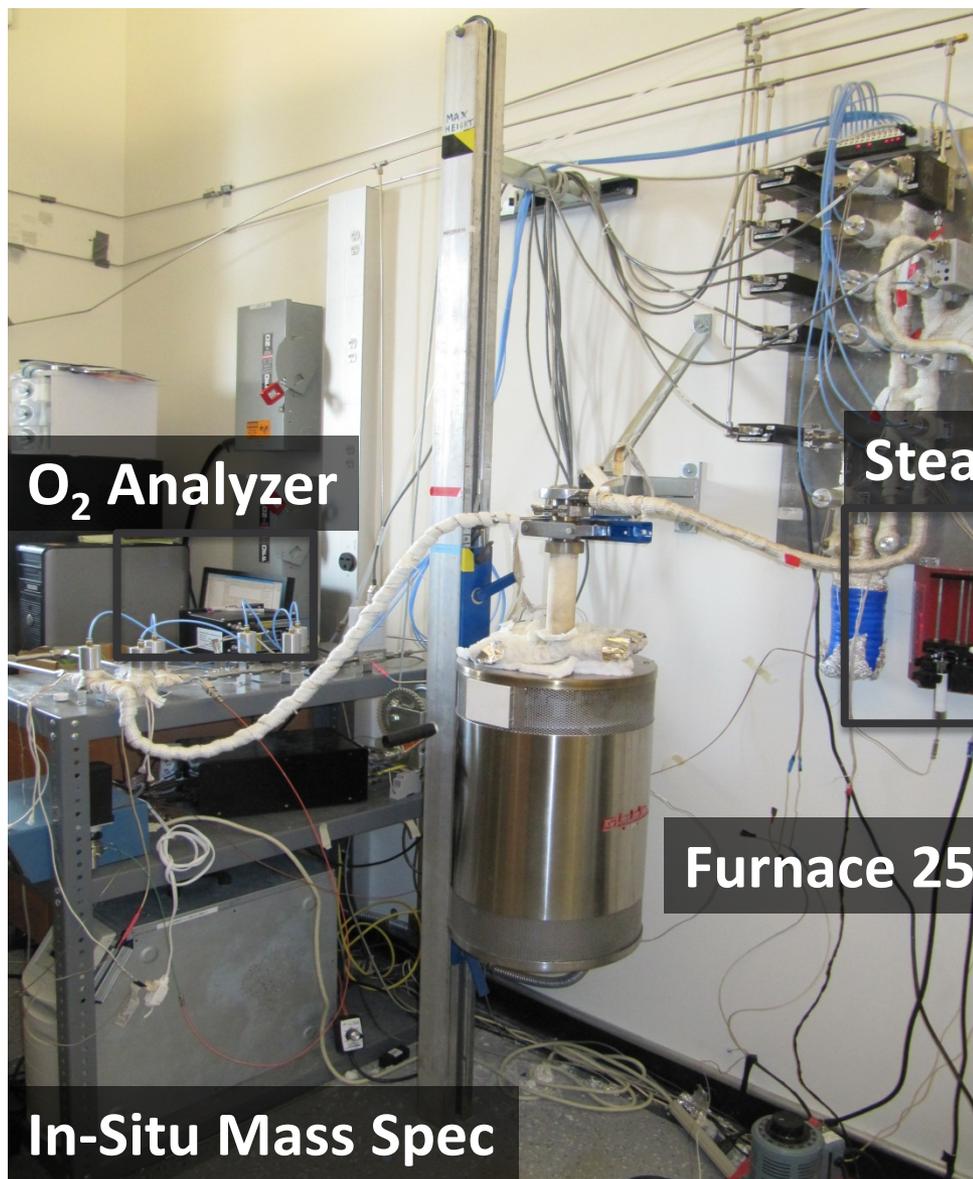
- Ceria redox is considered base material for comparative water splitting (WS) performance – fast kinetics & robust
- Evaluate “doped” CeO_2 , compared to base
- Evaluate “hercynite cycle” materials, i.e. ferrite/alumina reaction
 - Temperature Swing redox (TS)
 - Isothermal redox (IS)
- Model multi-tube fixed reactor configuration for efficiency estimates & “best” design
- Evaluate effect of increased pressure (P) and temperature (T) on increasing the slower oxidation rates measured at Sandia National Labs in 2012
- Validate high productivity “hercynite cycle” data obtained on-sun at NREL in 2012 (145 $\mu\text{mole H}_2/\text{g}$ total)



Accomplishments & Progress

Stagnation Flow Reactor for Materials Characterization

- CeO₂
- “Hercynite”
- T-Swing redox
- Isothermal redox



O₂ Analyzer

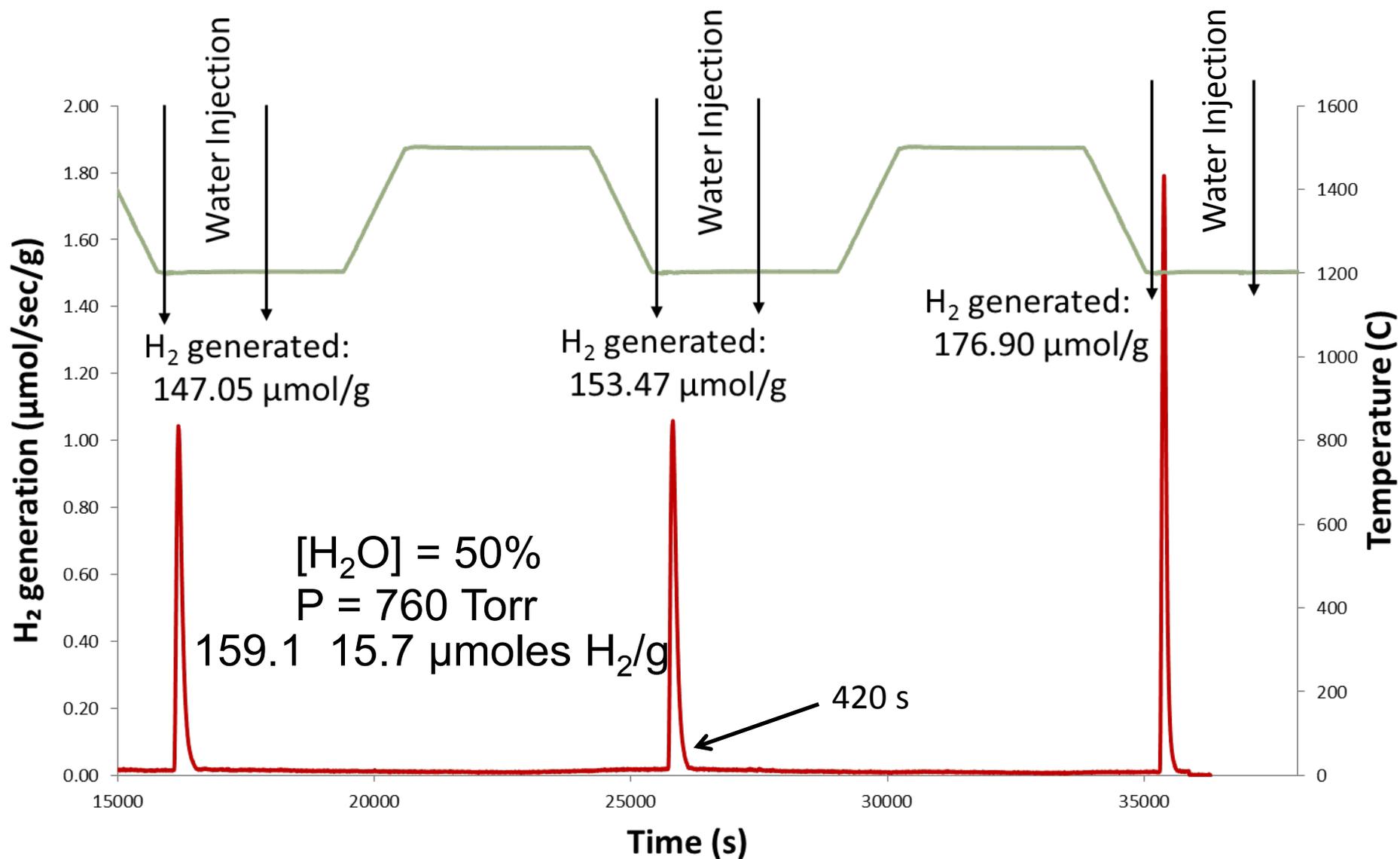
Steam Generator

Furnace 25 – 1700°C

In-Situ Mass Spec

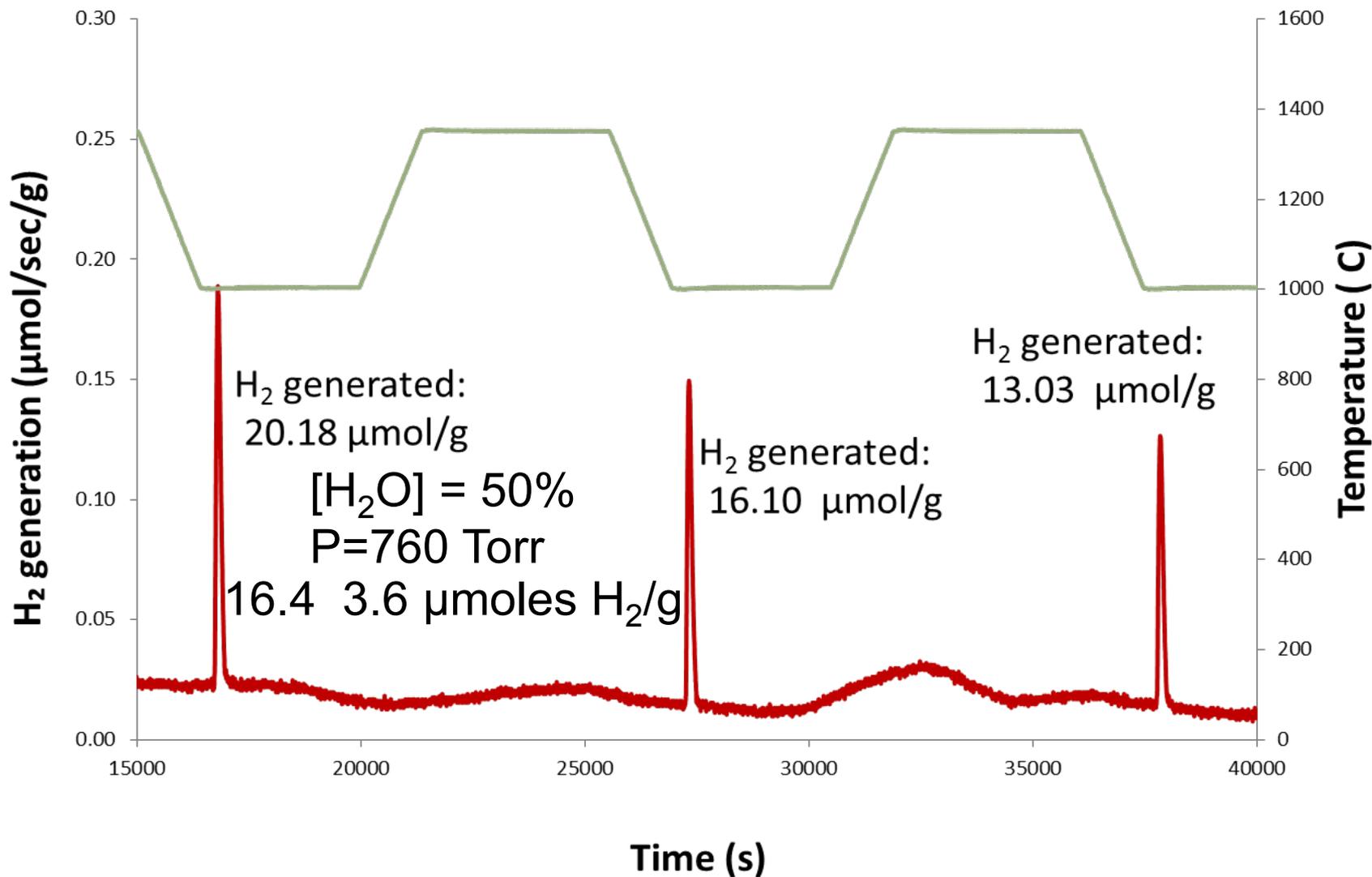


Ceria 1500°C/1200°C (redox)



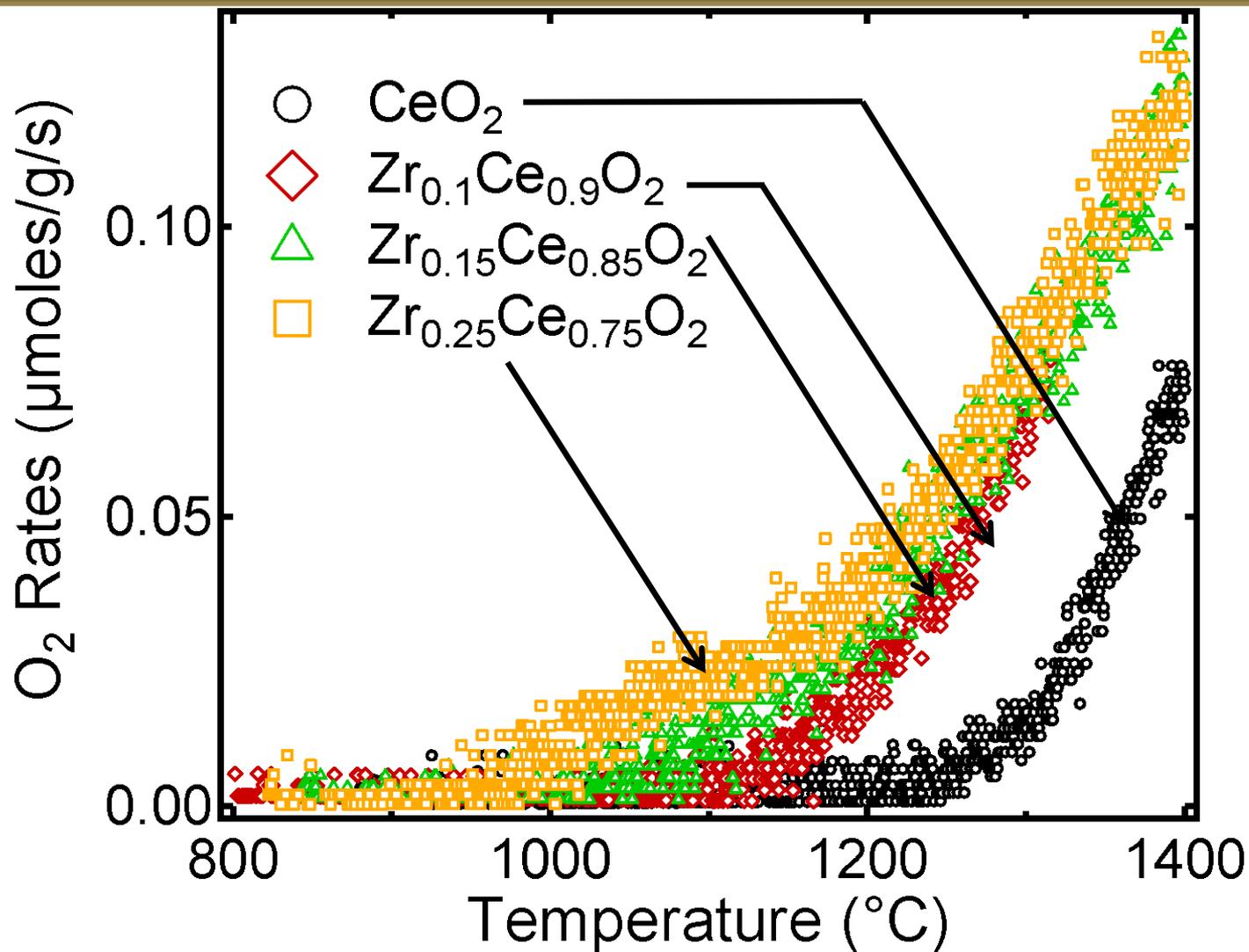


Ceria 1350°C/1000°C (redox)





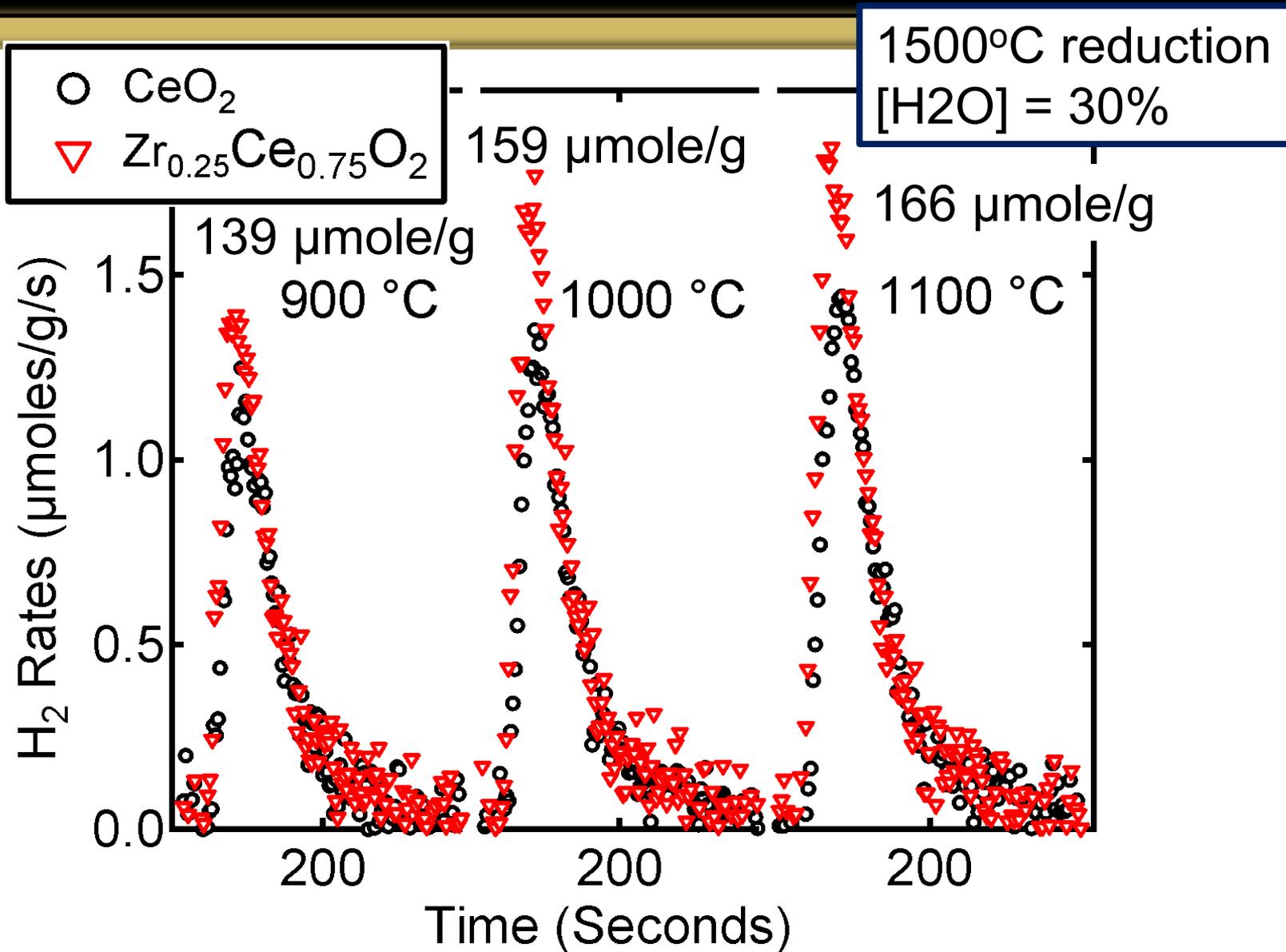
Zr Substitution Beneficial to Reduction



Experiments run at Sandia National Laboratories



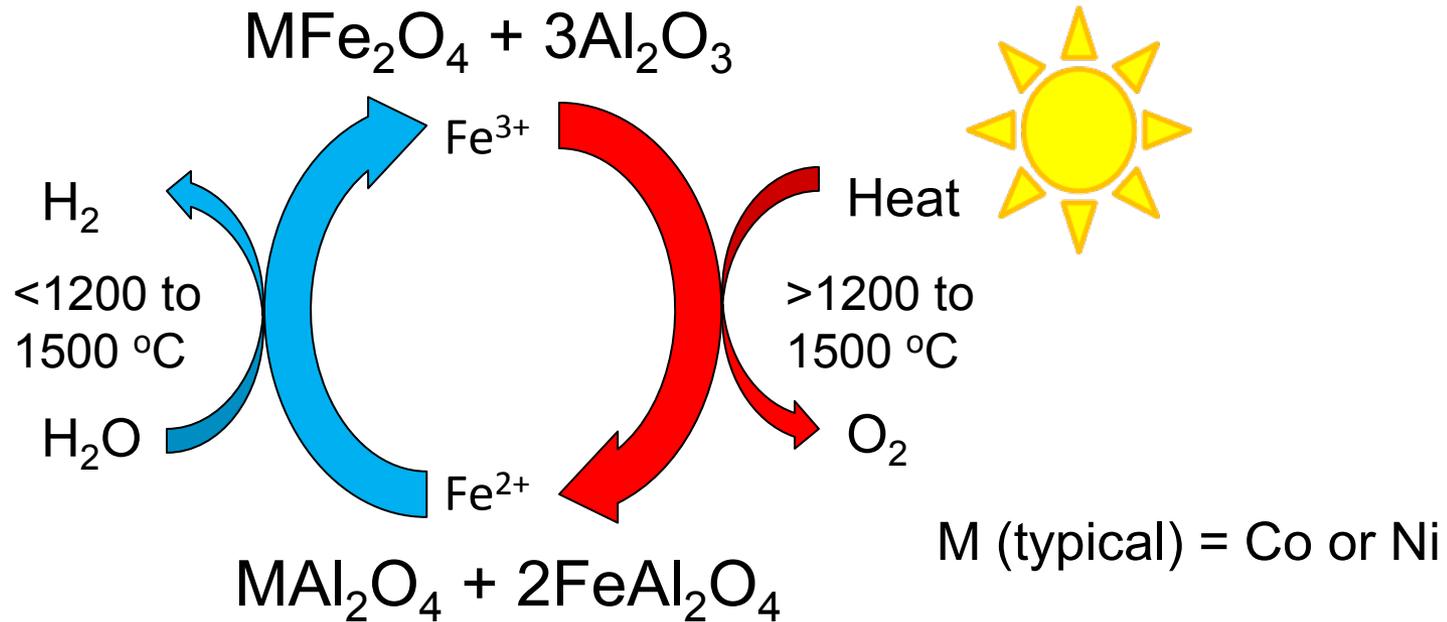
Zr Substitution Beneficial to Oxidation



Experiments run at Sandia National Laboratories



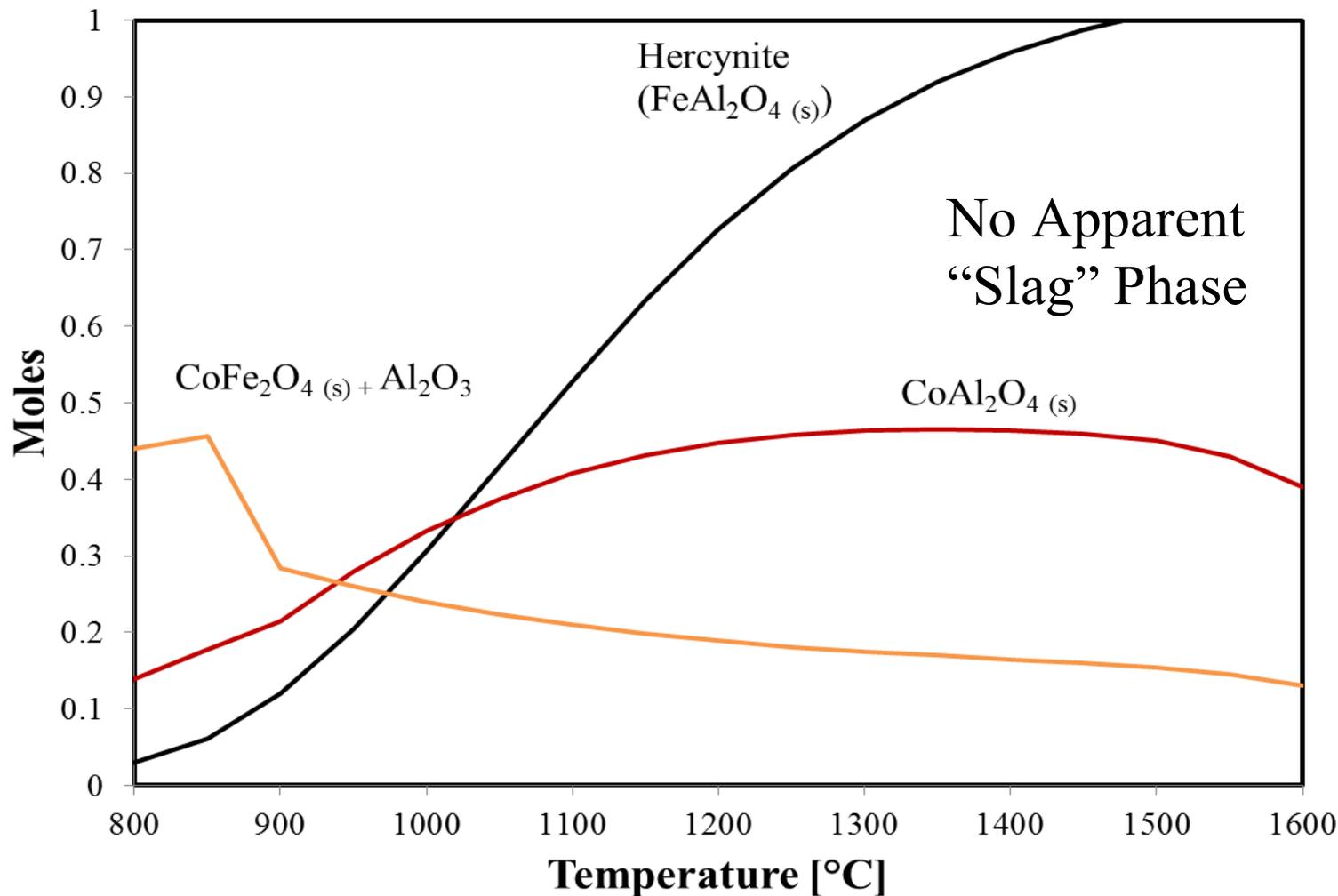
“Hercynite Cycle”



- Reduced and oxidized moieties are stabilized in two different compounds;
- Compound formation is more thermodynamically favorable than solid solution formation
- Higher T and P should increase oxidation rate



“Hercynite Cycle” Robustness



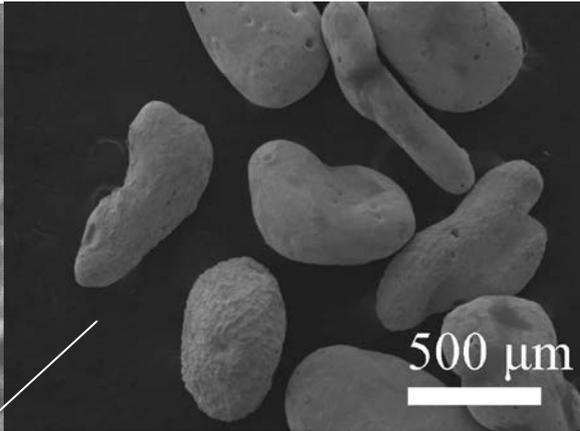
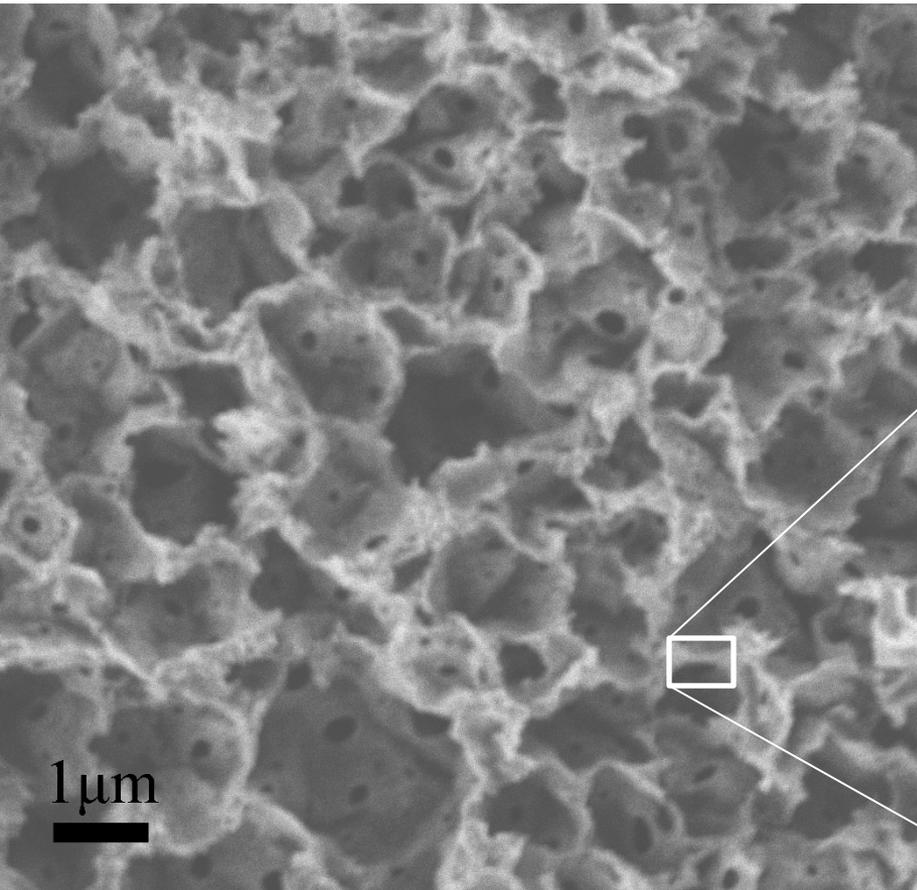
Chemistry Validated via Raman:

Arifin, D. et al. , Energy & Environmental Science **5**, 9438-9443 (2012)

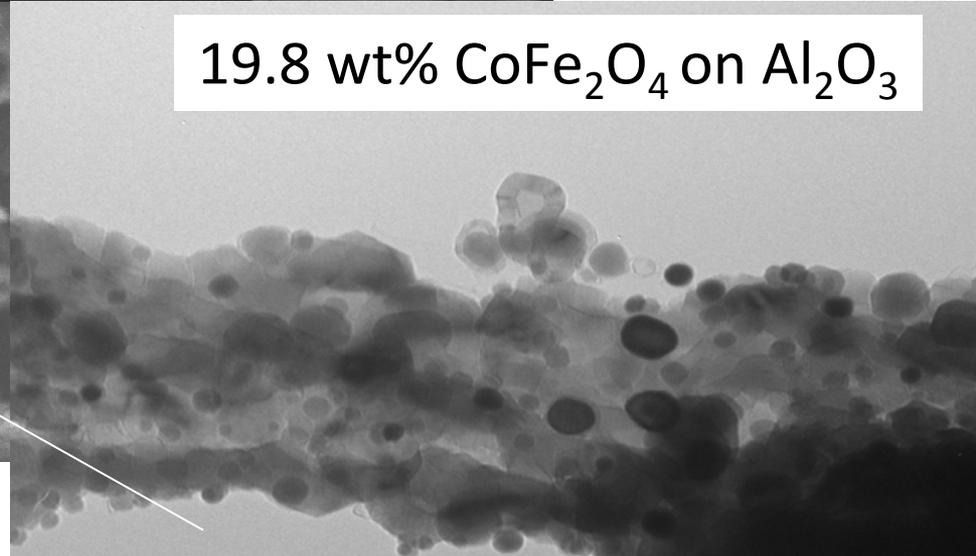


Micrographs of Active Nanostructured “Hercynite” Materials

Liang, X.H. et al., Microporous and Mesoporous Materials, 149, 106-110 (2012)



19.8 wt% CoFe_2O_4 on Al_2O_3



Cross-sectioned Particle

Skeletal $\gamma\text{-Al}_2\text{O}_3$

(80 m^2/g ; 1 cm^3/g pore volume);

Lichty, P., et al. Int. J. of Hydrogen Energy, 37, 16888-16894 (2012)



Isothermal Redox

Reduction temperature is dictated by reduction enthalpy of the active material

However water is not reacting in the gas phase, need to consider three phases:

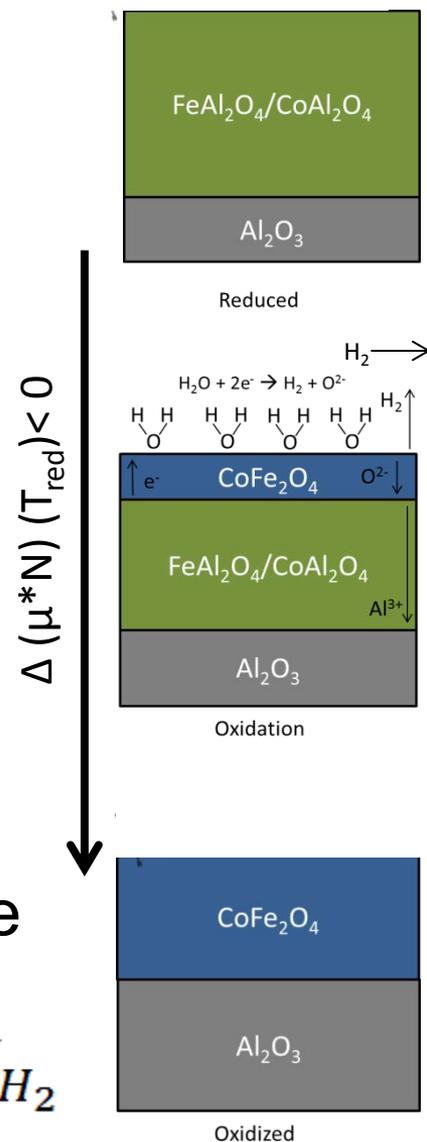
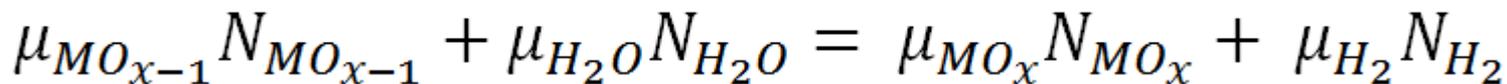
-Gas. Surface and Solid

$$\Delta G = P\Delta V - T\Delta S + \sum_{j=1}^M \mu_j \Delta N_j$$

N_x on the surface is related to P_x :

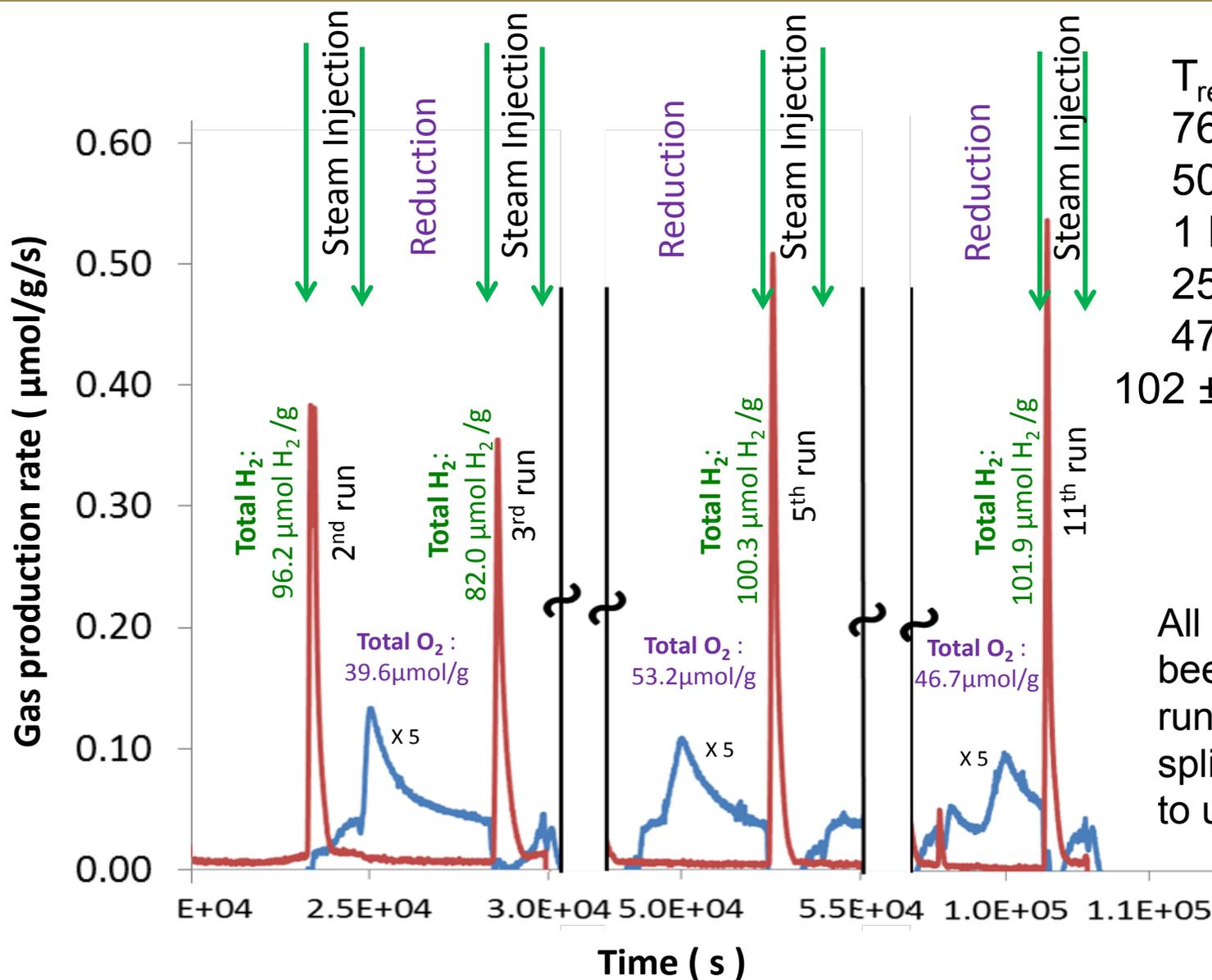
$$N_x = a * P_x$$

By altering pressure, the free energy can become favorable





“Hercynite Cycle” Isothermal Water Splitting



$T_{\text{red}} = T_{\text{ox}} = 1350 \text{ }^\circ\text{C}$
760 Torr
50% [H_2O]
1 hour reduction
25 min oxidation
47% Active
 $102 \pm 18 \mu\text{moles H}_2/\text{g}$

All material has been aged by running > 150 water splitting cycles prior to use.



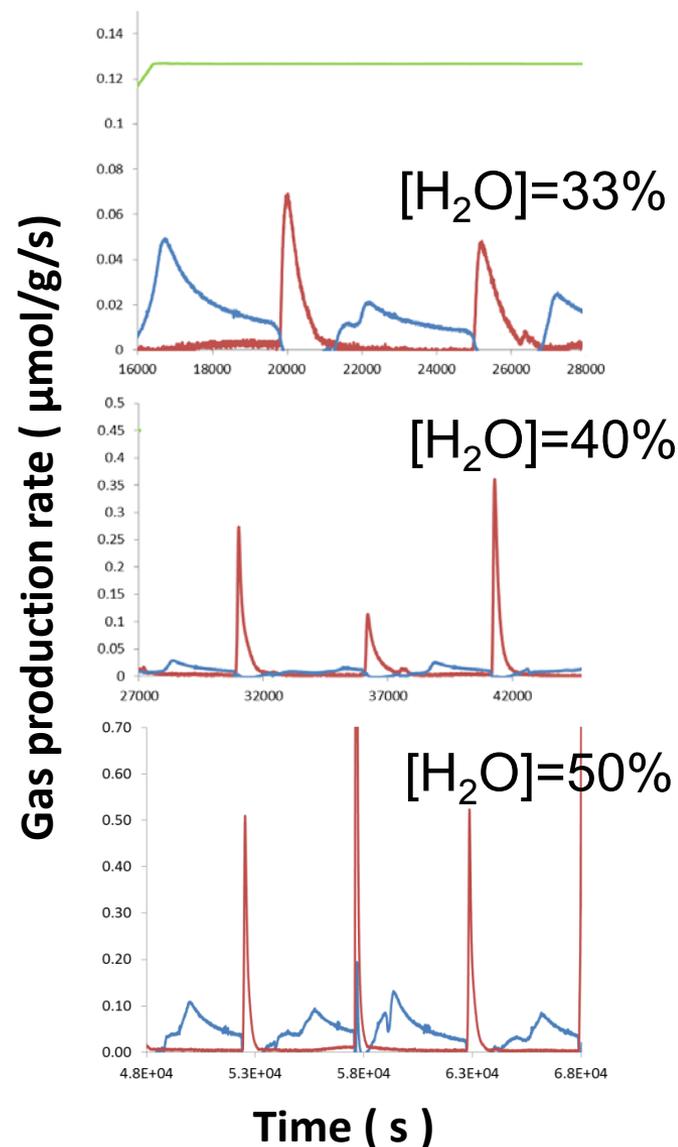
Hercynite Isothermal Summary @1350°C

% [H ₂ O]	P _{H₂O} (Torr)	H ₂ production ^a ($\mu\text{mol/g}$) ^b	Peak rate ^b ($\mu\text{mol/g/s}$)
33	253.3	40 ± 9	0.06 ± 0.02
40	325.7	72 ± 8	0.15 ± 0.07
50	380	102 ± 18	0.35 ± .18

^a Error was calculated at 95% confidence level.

^b Rates represent $\mu\text{mol H}_2/\text{g}$ of total material.
Multiply by 2.13 to get $\mu\text{mol H}_2/\text{g}$ active material.

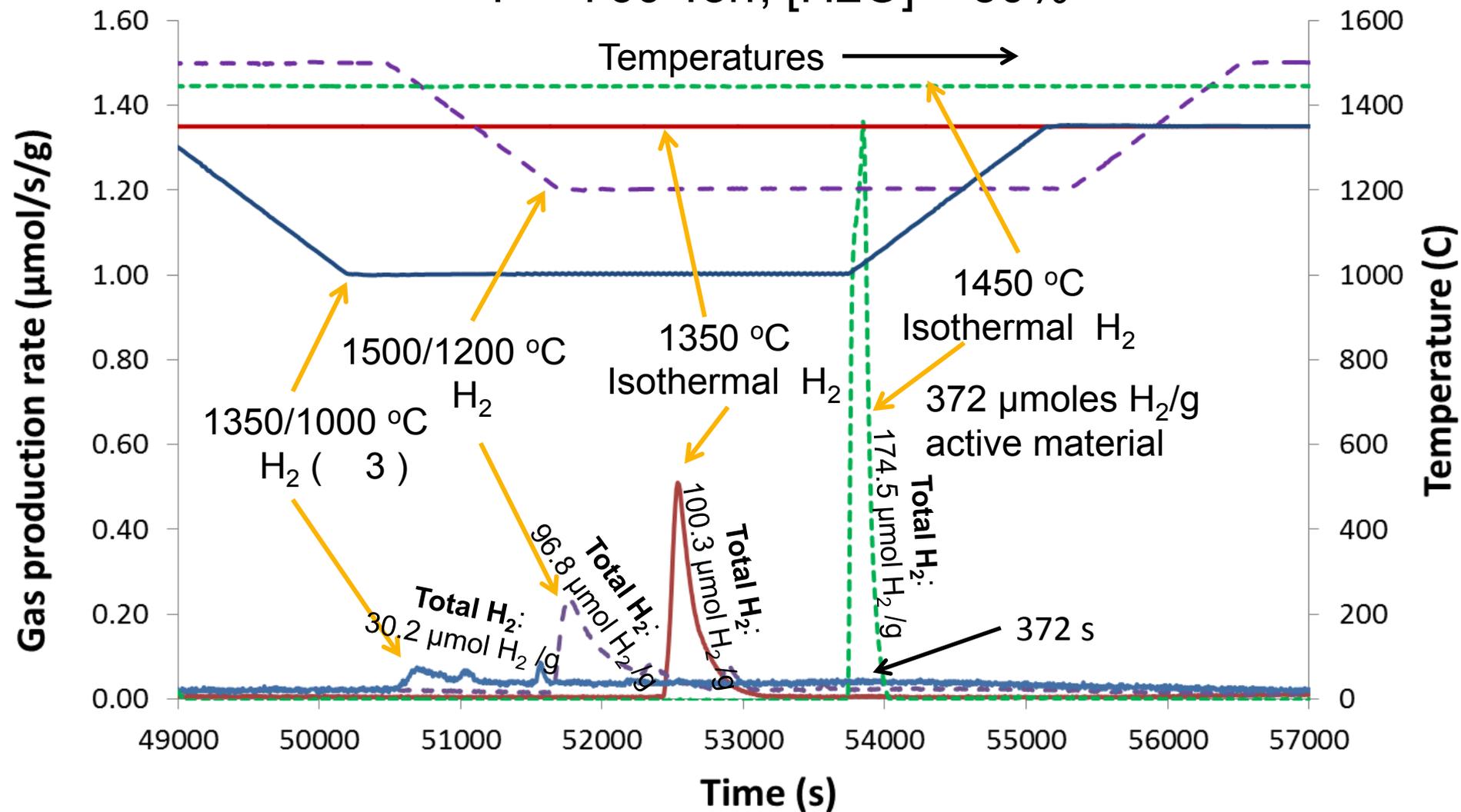
- Increased H₂O pressure increases total H₂ produced
- Increased H₂O pressure increases peak rates of H₂ production
- Increased H₂O pressure decreases time for complete re-oxidation.





Temperature Swing vs. Isothermal Water Splitting

$P = 760 \text{ Torr}, [\text{H}_2\text{O}] = 50\%$





Water Splitting Comparisons

Temp Swing (TS) & Isothermal (IT) (Red/Ox); Temperature (°C)	CeO ₂ (μmole/g)	Nanostructured “Hercynite” (μmole/g); x 2.13 / g active	CeO ₂ Peak Rate (μmole/g/s)	Nanostructured “Hercynite” Peak Rate (μmole/g/s); x 2.13 / g active
1500/1200	159.1 ± 15.7	93.7 ± 19.2	1.28 (avg)	0.32 (avg)
1350/1000	16.4 ± 3.6	31.4 ± 2.3	0.15 (avg)	0.03 (avg)
1350/1350		102 ± 18		0.55 ± 0.16
1450/1450		167.4 (avg)		1.34 (avg)

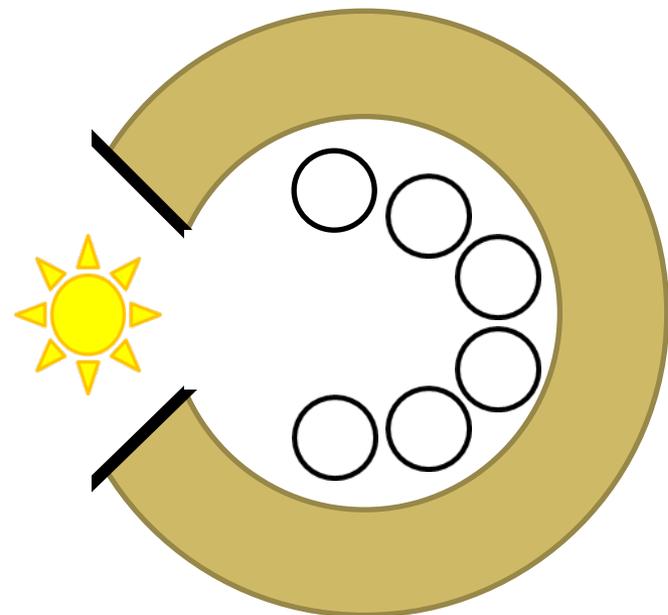
P = 760 Torr; [H₂O] = 50%

- At high reduction T, TS CeO₂ produces ~ equal H₂ as IT “hercynite cycle” per total g of material (“hercynite cycle” produces about 2X more on active material basis).
- At low reduction T, IT “hercynite cycle” produces ~ 5X more H₂ compared to CeO₂ and ~10X more on basis of active material
- IT “hercynite cycle” produces substantially more H₂ than TS “hercynite cycle”.

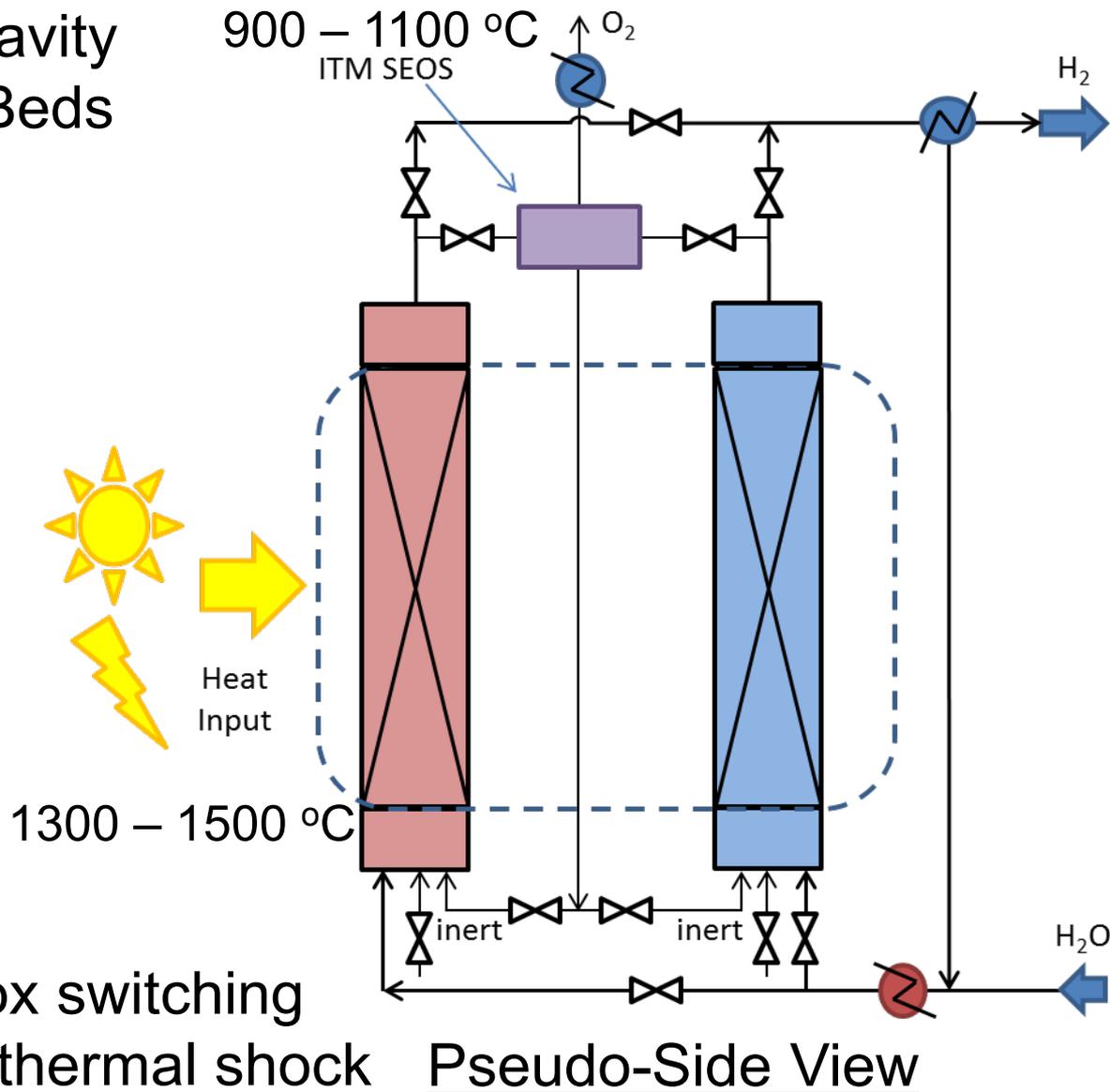


Isothermal Redox Similar to PSA

Insulated, Absorbing Cavity
w/ Multi-tubular Fixed Beds



Top-Down View



Pseudo-Side View

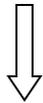
- Potentially faster redox switching
- Fewer concerns with thermal shock



Receiver Model Concept/Overview

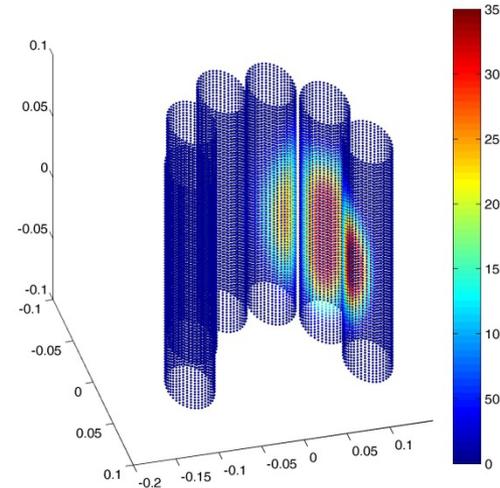
3D Monte Carlo ray-tracing model:

- Provides profiles of absorbed solar energy on all surfaces from defined solar profile at aperture



3D transient CFD model:

- Fluid flow through packed bed
- Convective / conductive / radiative heat transfer in packed bed and cavity
- Natural convection in cavity space
- Kinetic reaction rates = $f(T, \text{local fluid composition, reaction extent})$
- Equilibrium limitations via kinetic rates of reverse reactions



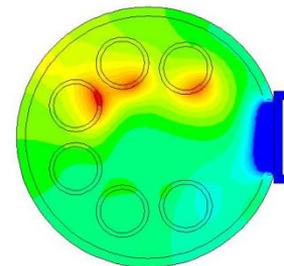
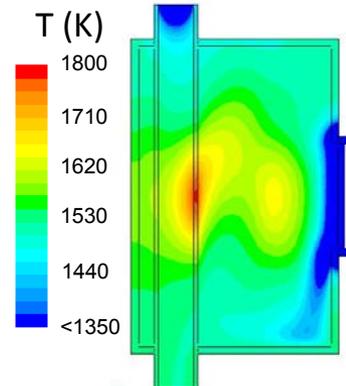
Solar energy flux absorbed on tube array

Time – dependent receiver temperature profiles



Objectives

- Develop steady state & dynamic models of a multi-tube solar receiver
- Identify parameters controlling receiver efficiency
- Identify optimal tube/cavity configurations & solar flux input
- Quantify impacts of isothermal operation on receiver efficiency





Isothermal redox Efficiency Calculations

Time-averaged receiver efficiency based on transient H₂ production

Battery Limits

- 4 kW solar input
- Adiabatic external boundaries
- 6 cm square aperture
- 6 min cycle time
- Flux - Solar beam width / direction optimized independently for each design

“Hercynite Cycle”

$$\bar{\eta} = \frac{\int_{\text{cycle}} \dot{n}_{\text{H}_2} LHV_{\text{H}_2} dt}{\int_{\text{cycle}} P_{\text{solar}} dt + \int_{\text{cycle}} E_{\text{O}_2} \dot{n}_{\text{O}_2} dt} = \frac{\text{Heating value of H}_2 \text{ produced}}{\text{Solar energy} + \text{Energy to separate O}_2 \text{ from inert}} = \frac{LHV_{\text{H}_2} \bar{n}_{\text{H}_2,i}}{P_{\text{solar}} + E_{\text{O}_2} \bar{n}_{\text{O}_2}}$$

<u>r cavity</u> <u>(cm)</u>	<u>h cavity</u> <u>(cm)</u>	<u>r tube</u> <u>(cm)</u>	<u>mol</u> <u>CoFe₂O₄</u> <u>per tube</u>	<u>sccm</u> <u>H₂O per</u> <u>tube</u>	<u>Maximum</u> <u>T (°C)</u>	<u>Average</u> <u>T (°C)</u>	<u>η_{LHV}</u> <u>H₂</u>
14.6	18	2.3	2.6	1	1620	1532	5.5
20.1	22	3.3	6.3	6	1427	1257	16.7

η_{LHV} H₂ increases with a decreased surface/volume ratio for solar reactor



Collaborations

- High-flux Solar Furnace On-sun Operations at NREL
- Laser-assisted Stagnation Flow Reactor Operations at Sandia – Livermore (one Ph.D. student in-place at all times)



Proposed Future Work

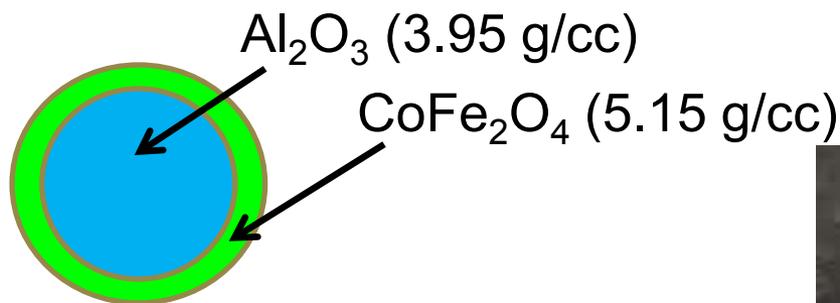
- Evaluate isothermal redox at $T > 1450^{\circ}\text{C}$; $P > 760$ Torr; and $[\text{H}_2\text{O}] = 100\%$
- Evaluate improved compositions approaching stoichiometric $\text{CoFe}_2\text{O}_4/\text{Al}_2\text{O}_3 = 3$
- Develop reaction kinetics rate expressions for “hercynite cycle” active materials
- Incorporate improved reduction and oxidation reaction kinetics into the multi-tubular receiver model; update model
- Demonstrate isothermal redox on-sun
- Evaluate a high-T oxygen transport membrane for O_2 removal during redox cycling (ITM-SEOS)
- Carry out H2A Analysis for Isothermal Redox Processing



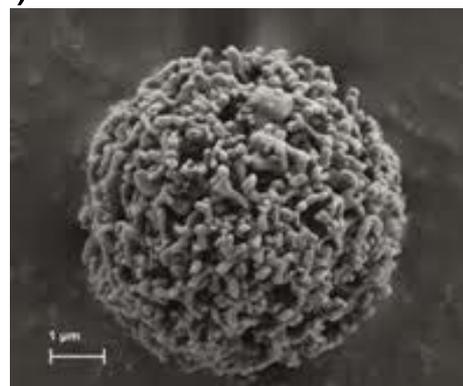
Proposed Future Work

- Synthesize Micro-containers of Nano-sized Active Materials & test in a Particle Flow Reactor
- Particle ALD can be used to produce nano-coated nano-particles that are then spray dried/calcined to 60 microns

$$\frac{\text{CoFe}_2\text{O}_4/\text{Al}_2\text{O}_3}{\text{Al}_2\text{O}_3} = 1/3 \text{ (molar)}$$



$\frac{dp \text{ Al}_2\text{O}_3}{\text{(nm)}}$	$\frac{\text{CoFe}_2\text{O}_4 \text{ Film Thickness (nm)}}{\text{CoFe}_2\text{O}_4}$
20	1.7
40	3.3
150	12.5



Spray Dried



Calcined
(Typical $d_{50} = 60-80 \mu\text{m}$)

Or, directly spray dry nano Al_2O_3 , Fe_2O_3 and CoO



Summary

- Zr-doped CeO_2 increases H_2 productivity by $\sim 20\%$ over undoped CeO_2 ;
- Hercynite cycle nanostructured active materials operating isothermally at 1450°C have comparable peak reaction rates and H_2 production rates/g compared to Zr-doped CeO_2 reduced at 1500°C and oxidized at 1200°C . On the basis of g active materials only, hercynite cycle materials are 2X performance - demonstrated $372 \mu\text{moles H}_2/\text{g}$ active material.
- Hercynite cycle nanostructured active materials operating isothermally at 1350°C have 5X peak reaction rates and H_2 production rates/g compared to CeO_2 reduced at 1350°C and oxidized at 1000°C . On the basis of g active materials only, hercynite cycle materials are 10X H_2 production performance.



Summary Continued

- Active “hercynite cycle” nanostructures maintained their redox activity for over 150 cycles, after 1st cycle;
- Increased $[H_2O]$, operating P and operating T increase total H_2 produced, increase the peak rate of H_2 production, and decrease the time for complete re-oxidation for isothermal “hercynite cycle” materials; and
- A small adiabatic $4\text{-kW}_{\text{thermal}}$ solarthermal multi-tube fixed bed reactor operating isothermally with “hercynite cycle” materials is predicted to have a $\eta_{\text{LHV } H_2} > 15\%$.



Acknowledgements:



- 16 Peer-reviewed scientific papers published in 2012;
- 7 already published in 2013 (+ 3 in press)
- 4 U.S. Patents issued in 2012; 1 Issued thus far in 2013
- Three Ph.D. students won 1st, 2nd, and 3rd Place Posters and an U/G student took 1st Place at 2012 Annual AIChE Meeting (Pittsburgh)

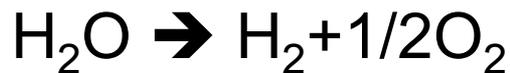




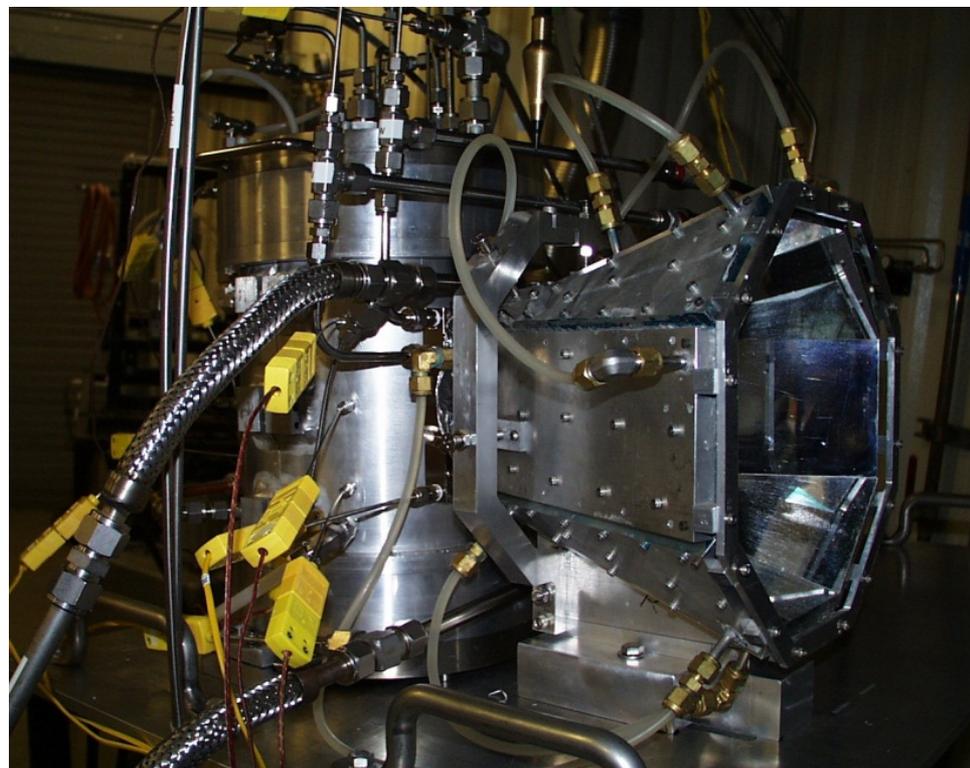
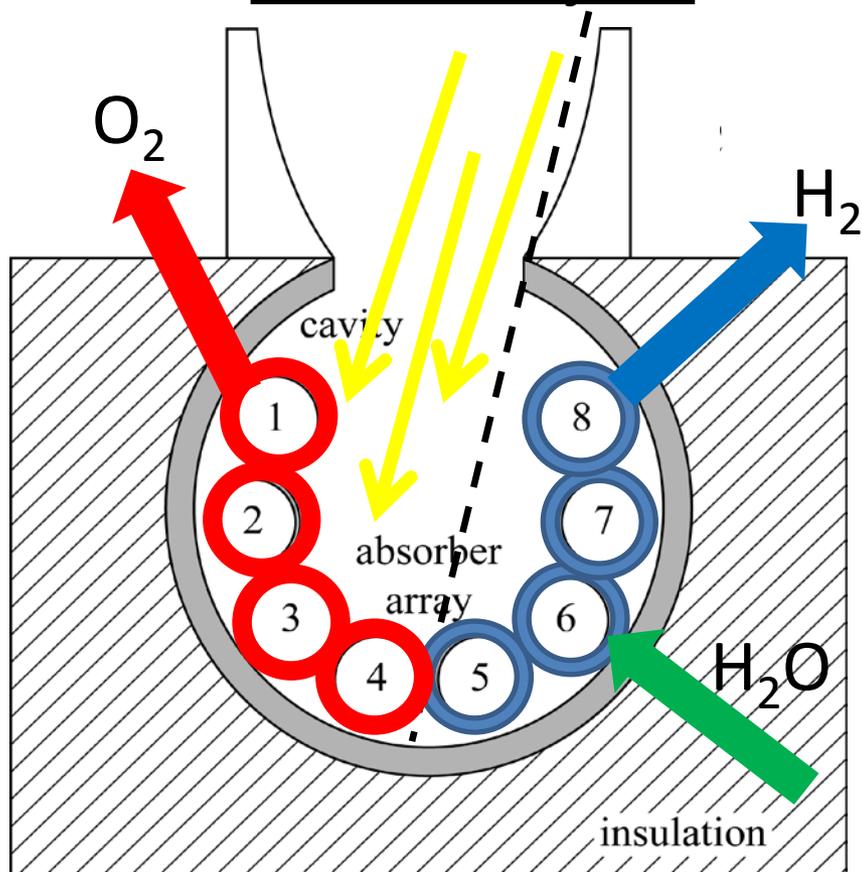
Technical Backup Slides



SurroundSun™ Multi-tubular Switching Redox Reactor/Receiver



1st Half Cycle



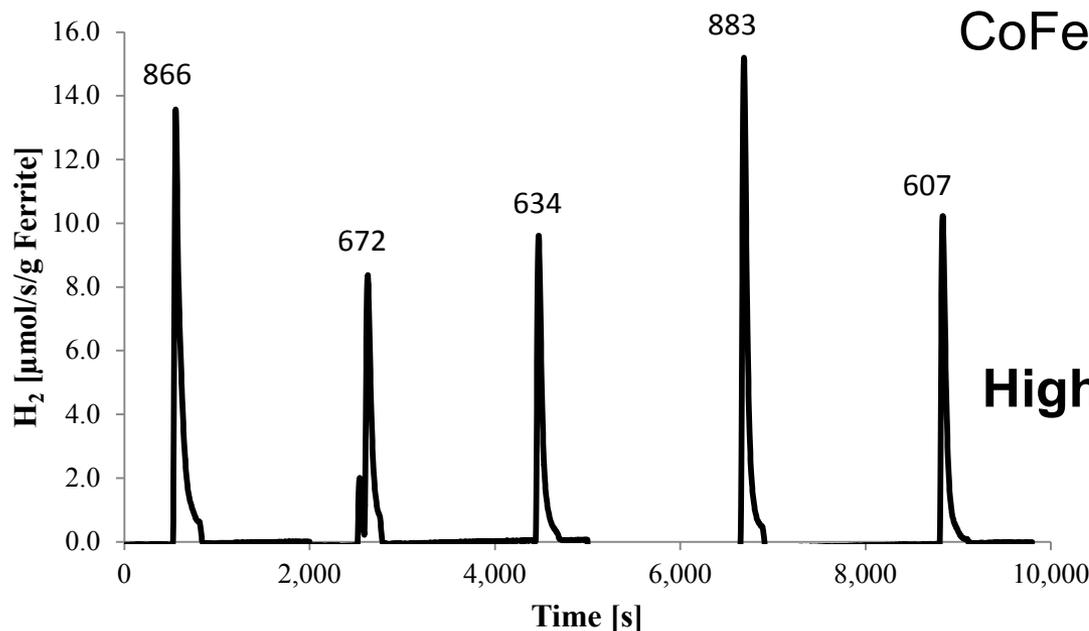
University of Colorado
Multi-tube Solar Receiver/Reactor



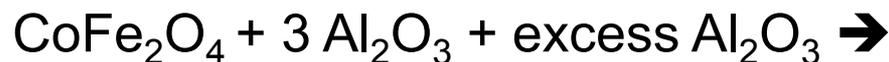
On-sun Experiments at NREL (2012)

1350°C/1000°C Redox (P=1120 Torr; 50% [H₂O])

**Nanostructured ALD “Hercynite”
Materials**



Averaged H₂ Production Rate



145 μmole/g total

309 μmole/g active material

732 μmole/g ferrite

47 % active material

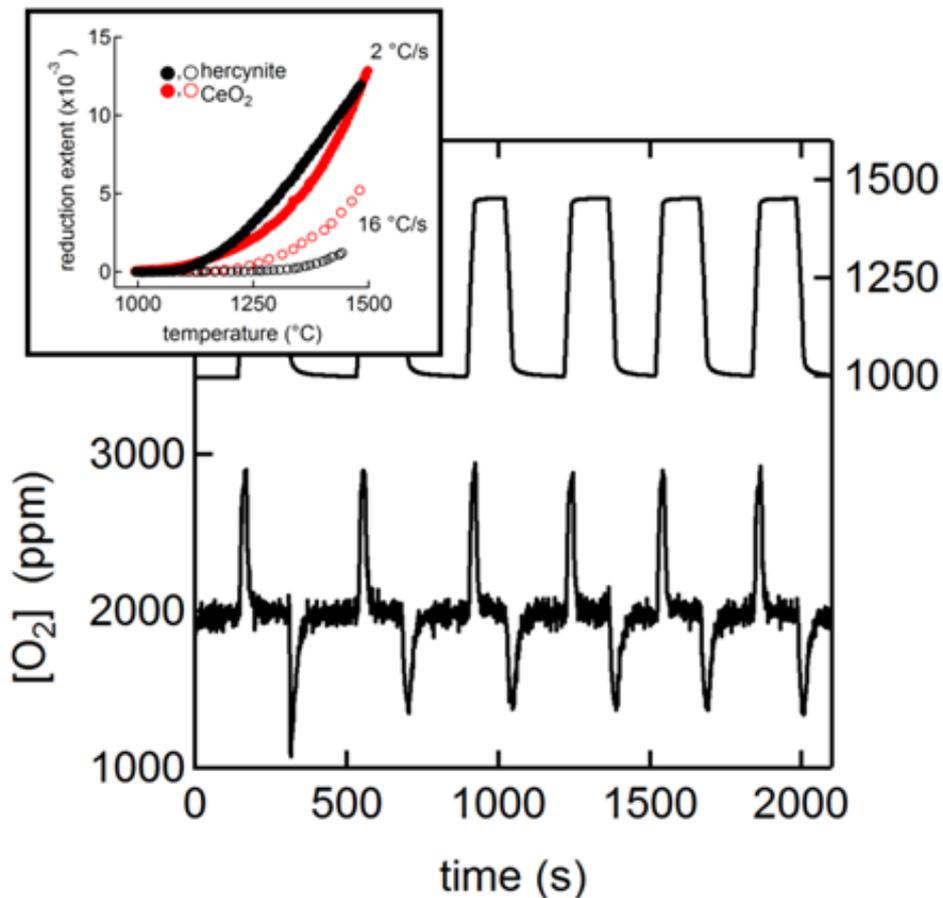
**Higher P favors higher productivity
(need to validate)**

Integrated H₂ production in μmole/g ferrite



Laser-Assisted redox at SNL (2012)

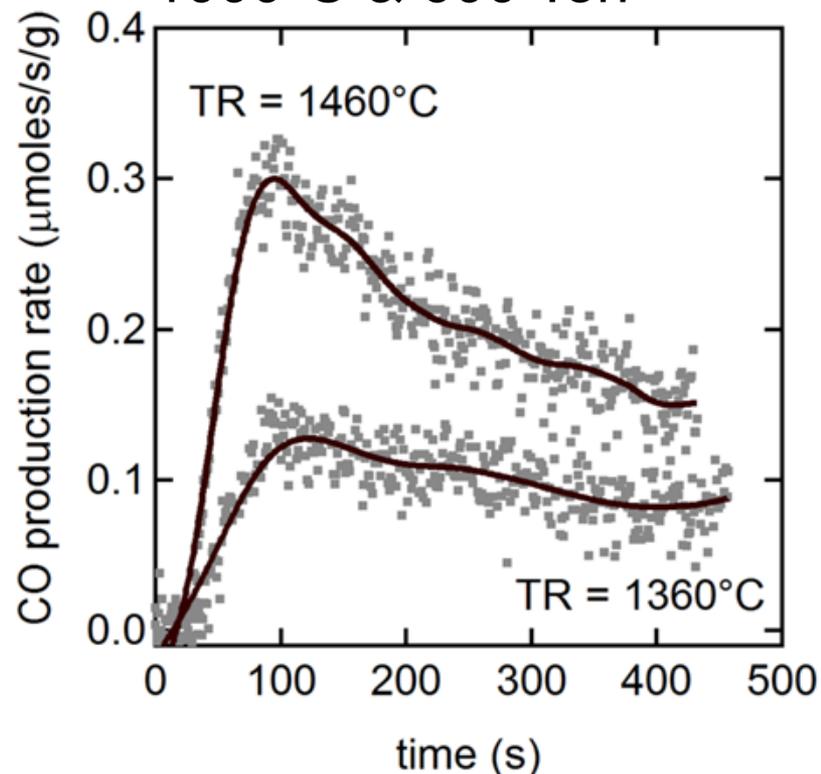
Nanostructured “hercynite cycle” active materials



Fast Reduction Kinetics
& Oxygen Exchange

Arifin, D. et al., *Energy & Environmental Science* **5**, 9438-9443 (2012)

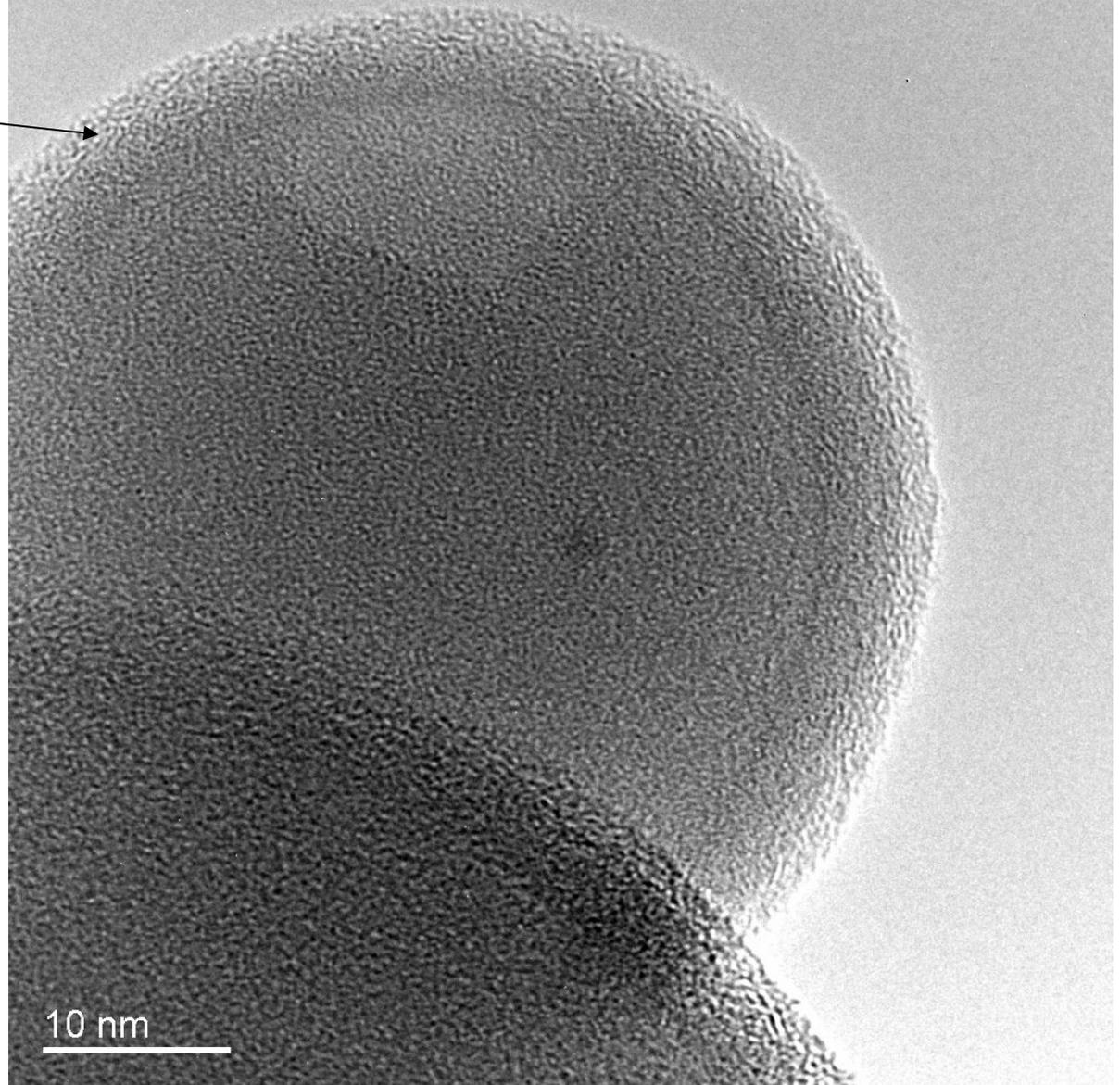
Slow CO_2 oxidation @
 1000°C & 600 Torr



**Need to determine impact of
higher T & P on oxidation rate**

TEM Alumina Coated Silica (40 nm)

5.2 nm film
(1.2 Å/cycle)

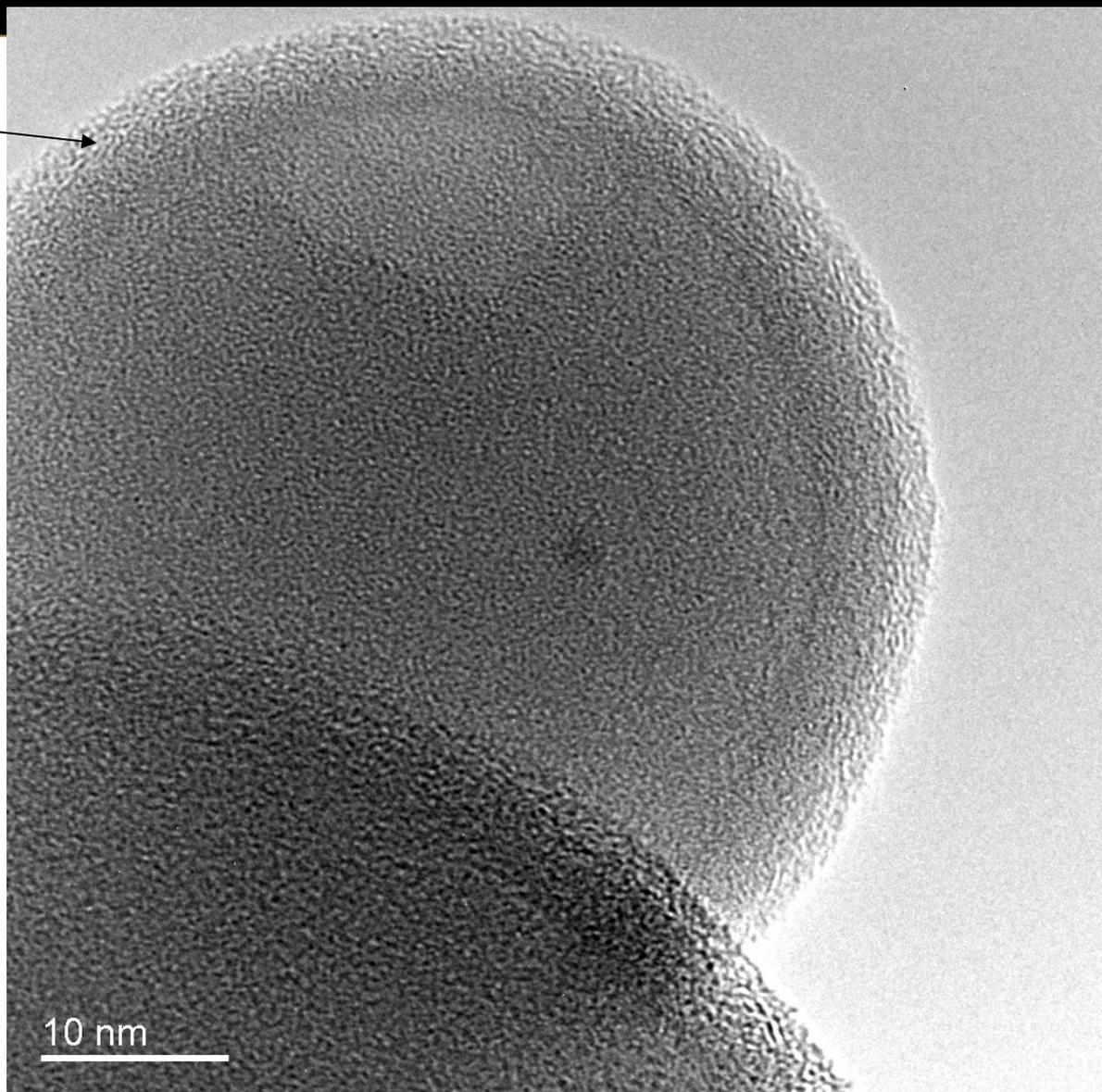


Film thickness is
uniform throughout
the entire sample



HRTEM Alumina Coated Silica (40 nm)

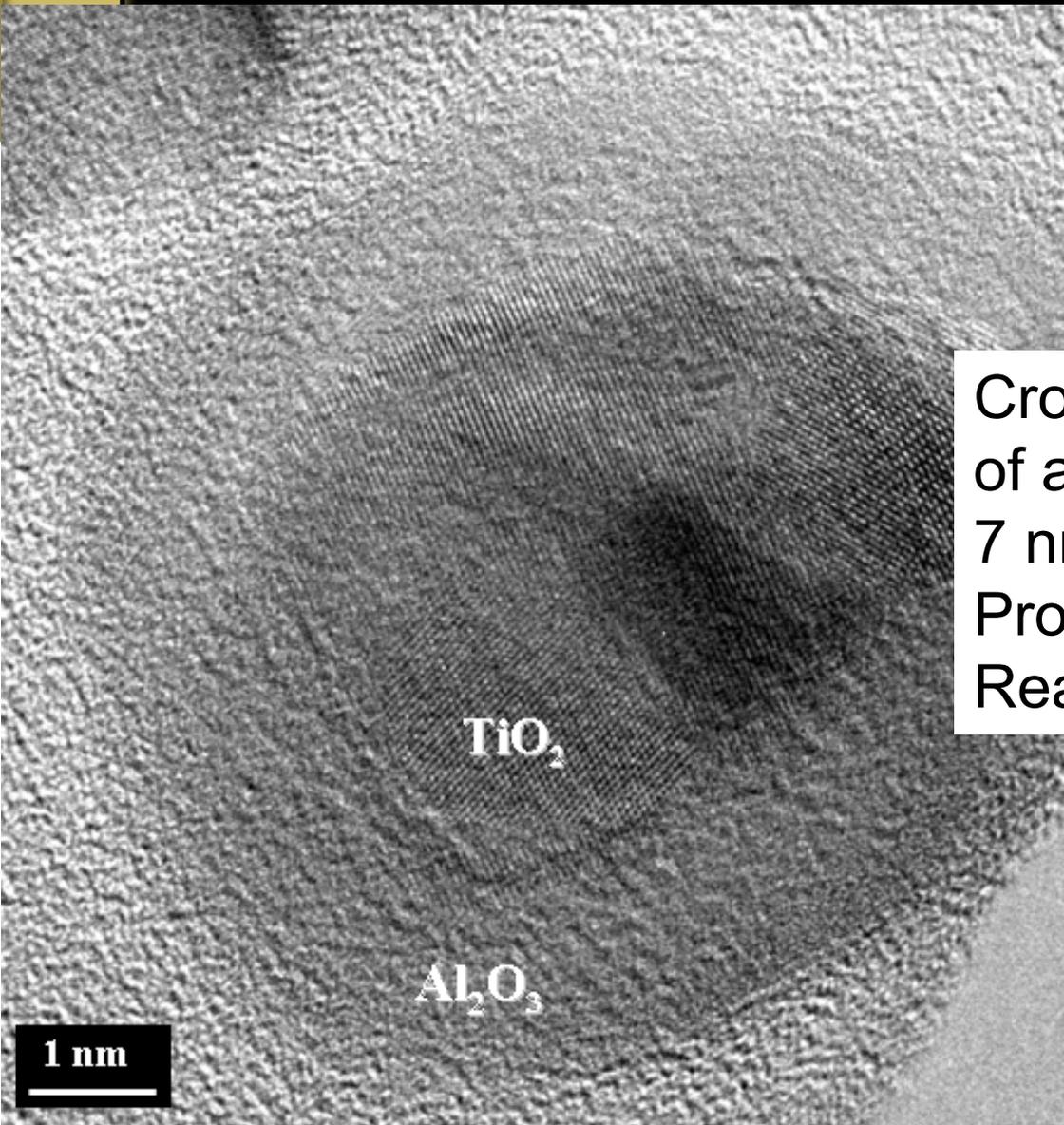
5.2 nm film
(1.2 Å/cycle)



Film thickness is uniform throughout the entire sample of primary particles; coated in a fluidized bed



7 nm Primary TiO_2 Particle Nanocoated



Cross-section HRTEM Image of an Al_2O_3 (15 Å) ALD Coated 7 nm TiO_2 Nanoparticle Processed in a Fluidized Bed Reactor